

Experiment I-b Test Report
"Space Environment Simulator Test Program"
Contract NAS 9-3414

PERFORMANCE & THERMAL RESPONSE
OF THE GEMINI EXTRAVEHICULAR
SPACE SUIT - EXPERIMENT I-b

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FOREWORD

This report describes the results of a Space Environment Simulator test of a prototype Gemini extravehicular space suit (Model GH-2C-18) conducted by LTV Astronautics for the NASA Manned Spacecraft Center. This test (Experiment I-b) was conducted November 5, 9 and 12, 1964 at the LTV Astronautics facility in Dallas, Texas. Experiment I-b is one of 12 space suit thermal evaluation tests being conducted in the LTV Astronautics Space Environment Simulator under contract NAS 9-3414. This contract covers a twelve month effort and is scheduled for completion on July 30, 1965. Mr. J. C. Peradek and Mr. R. F. Schwartz of the NASA-MSC, Systems Test Branch are the technical monitors for this contract.

Experiment I-b was conducted in accordance with LTV report number 00.520 "Gemini Extravehicular Suit Performance and Thermal Response Test" submitted to NASA-MSC for approval on 21 October 1964. This report presents the results of Experiment I-b and is submitted in accordance with contract NAS 9-3414.

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1.0 SUMMARY

Experiment I-b of NASA-MSC Contract NAS9-3414 requires that tests be conducted to evaluate the performance and thermal response of a prototype Gemini extravehicular space suit in a simulated 200 nautical mile earth orbit. A prototype Gemini extravehicular suit assembly (Serial Number GH-2C-18) was instrumented for temperature and pressure measurements and was exposed to the simulated space environment created by the LTV Space Environment Simulator (SES). A thermal dummy capable of providing the sensible heat of a man was placed in the suit assembly to closely simulate manned occupancy of the space suit. Testing was conducted over a three day period under the following conditions: (1) cold soak with -320°F SES walls, (2) conditions simulating a earth orbit, (3) contact with a heated spacecraft surface and (4) high solar heat inputs. The principle objective of the test series was to determine the design adequacy of the prototype suit assembly for operation in the environmental conditions encountered in extravehicular earth orbit operations. The specific test objectives were to determine:

1. Suit temperatures and pressures as functions of time, orbit position and suit rotation position.
2. Suit net heat gain or loss as a function of time, orbit position and suit rotation position.
3. Net heat gain or loss through the suit visor.
4. Evidence of visor frosting.
5. Thermal adequacy of suit.
6. "Hot spots" or "cold spots" on the suit resulting from contact with simulated spacecraft surfaces.
7. Suit leakage under simulated space thermal & vacuum conditions.
8. Effect of compression under the parachute harness on suit thermal performance.

Simulation of the thermal and pressure environments during the tests included the following:

1. Astronaut body temperatures.
2. Deep space heat sink.
3. Solar heat flux.
4. Earth thermal radiation.
5. Earth albedo.
6. Hot spacecraft surface.
7. Vacuum.

Astronaut body temperatures and sensible metabolic heat output were simulated by a fiberglass and copper articulated dummy. The shell type construction of the dummy provides an outer layer of material which approximates the conductance of human skin. An electrical heater network covers the interior of the dummy shell and the dummy surface temperatures are controlled by regulating the power to the heaters.

The radiation heat sink of space was simulated by the liquid nitrogen shroud surrounding the test section of the SES. The simulated solar heat flux was provided by a bank of Mercury-Xenon lamps installed at one surface of the test chamber. A pressure of less than 10^{-4} mm Hg was maintained throughout the tests by the SES vacuum pumping system. Earth thermal radiation and reflected solar radiation (albedo) were simulated by use of a dished aluminum plate located opposite the suit from the solar lamps and coated with a controlled emittance paint. The thermal radiation from the earth simulator was controlled by regulating the simulator surface temperature. This was accomplished by varying the power input to electrical heaters attached to the back of the plate. Incident energy from the SES lamp bank was reflected from the dished plate to simulate the earth albedo radiation. The simulated spacecraft surface was provided by a section of aluminum structure which could be moved into contact with the suited dummy. The surface of the structure was adjustable to simulated spacecraft surface temperatures by electrical resistance heaters.

The prototype Gemini extravehicular space suit consists of a pressure restraint inner assembly and a thermal protective outer assembly fabricated to produce a single piece garment. The thermal protective provisions include seven layers of aluminized mylar covered by a nylon felt layer. The outer wearing surface of the suit is a lightweight nylon cloth. Thermocouples were attached to the outer surface and at various locations on the interior layers to monitor the thermal performance of the insulative layers. Visor and helmet temperature as well as suit pressures were also monitored during the tests.

The results of this experiment indicate that suit outer surface temperatures did not exceed +200°F or fall lower than -200°F during simulated extravehicular operations in an earth orbit. Maximum heat loss during deep space operation should not exceed 250 BTU/hr. The maximum heat leakage into the suit should not exceed 20 BTU/hr under maximum heating conditions. Visor heat loss to deep space was approximately 30 to 40 BTU/hr while visor heat gain under direct solar radiation was approximately 40-50 BTU/hr. The overall conductance of the suit was estimated to be between 0.017 and 0.024 $\frac{\text{BTU}}{\text{hr ft}^2 \text{F}}$. Contact with a 1800°F spacecraft surface or compression points under the parachute harness did not produce any measurable hot spots on the interior surface of the suit.

A positive indication of visor frosting was not obtained in this experiment. Based on visor temperature and the relative humidity measurements, visor frosting very likely did occur. A direct measurement of heat flux through the visor was not obtained due to equipment malfunction.

Suit pressures ranged from 3.8 to 4.4 psia during the test while the pressure differential or loss across the suit varied between 0.08 and 0.12 psi. Suit gas leakage varied between 140 and 190 scc/min during the course of the tests.

The foregoing results indicate that the Gemini prototype suit assembly tested should provide satisfactory thermal protection for manned use during earth orbit extravehicular operations. Additional testing, however, will be required to determine the adequacy of thermal protection about the hands and feet.

2.0 INTRODUCTION

Extravehicular operation in earth orbit requires protection of the astronaut from his environment. An important component of the protective system is the extravehicular space suit. This suit provides both protection from the low pressure of space as well as protection from the extreme heat sources and heat sinks. LTV Astronautics in accordance with Contract NAS9-3414 is engaged in a comprehensive un-manned test program to evaluate the performance of space crew equipment in a simulated space environment. The experimental test results detailed in this report cover the first of twelve space suit thermal evaluation experiments to be conducted in the LTV Space Environment Simulator for the NASA Manned Spacecraft Center. The first experiment (Experiment I-b) subjected the Gemini prototype extravehicular space suit assembly containing a thermal dummy to the low pressures and extreme temperature conditions of a simulated near earth environment. The experiment was performed to permit an evaluation of the thermal performance of this specific suit under space environment conditions similar to those encountered exterior to the Gemini spacecraft while in orbit.

This report presents a description of Experiment I-b, the results obtained, and an extrapolation of the test results to define the actual space conditions anticipated.

3.0 TEST PROGRAM

3.1

TEST OBJECTIVES

The overall objective of Experiment I-b was to evaluate the thermal performance characteristics of the Gemini extravehicular space suit during a simulated near earth orbit. The specific test objectives were as follows:

1. Suit temperatures and pressures as functions of time, orbit position and suit rotation position.
2. Suit net heat gain or loss as a function of time, orbit position and suit rotation position.
3. Net heat gain or loss through the suit visor.
4. Evidence of visor frosting.
5. Thermal adequacy of suit.
6. "Hot spots" or "cold spots" on the suit resulting from contact with simulated spacecraft surfaces.
7. Suit leakage under simulated space thermal & vacuum conditions.
8. Effect of compression under the parachute harness on suit thermal performance.

3.2

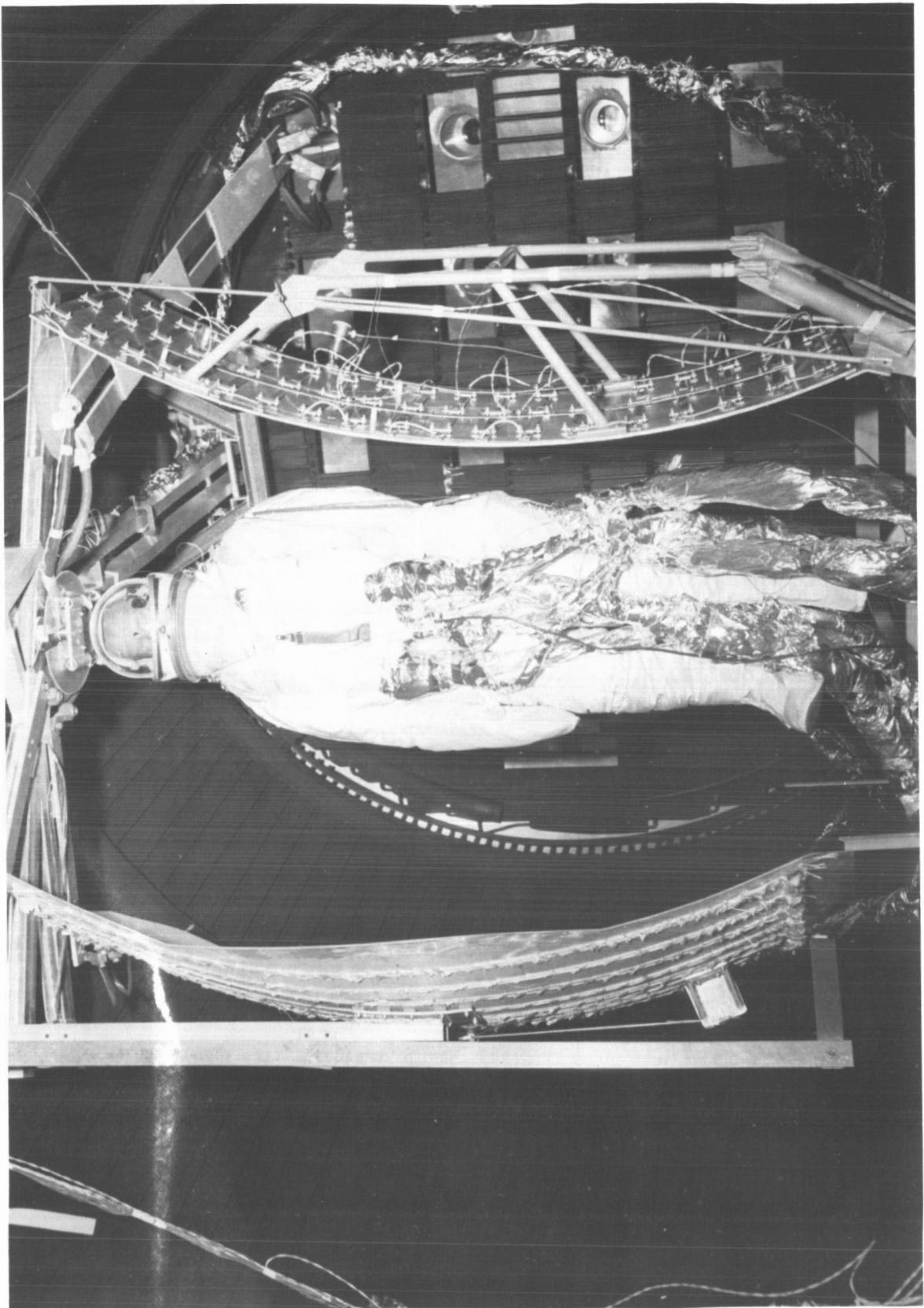
DESCRIPTION OF TEST ARTICLE

The test article was a Gemini space suit (GH-2C-18) which is the prototype of the insulated G-4C Gemini extravehicular suit. During the test, the suit was worn by a thermal dummy (described in paragraph 3.3.2.1) wearing a conventional underwear garment. Figure 1 shows the suit and dummy installed in the Space Environment Simulator for testing.

The test suit consists of a pressure garment with integral thermal insulation (Figure 2). The innermost layer is a lightweight nylon "comfort liner" which is worn next to the astronaut. Outside the comfort liner is the heavier pressure seal which is the airtight layer. Immediately outside the pressure layer is a "restraint net" which provides additional strength for containing the suit burst pressure forces. Following the restraint layer are two layers of light-weight nylon (du Pont HT-1 "Nomex"), seven layers of aluminized mylar superinsulation, the layer of Nomex felt and a Nomex outer layer. The test article included superinsulation gloves and mittens and insulation covers over the inlet and return hose connections to reduce the heat shorts of these areas. An insulation hood to place over the entire helmet was also provided for this test. The hood was provided to allow determination of heat leaks through the helmet and visor.

The left glove of the suit and the left hand of the dummy were removed and a special feed through was fitted to the wrist disconnect for the purpose of withdrawing internal instrumentation leads (Figure 3). The special feed through and leads were protected by a superinsulation cover during the experiment.

FIGURE 1 GEMINI SPACE SUIT ASSEMBLY INSTALLED IN THE LTV SPACE ENVIRONMENT SIMULATOR SHOWING THE EARTH AND SPACECRAFT SIMULATORS (TEST DAY #3)



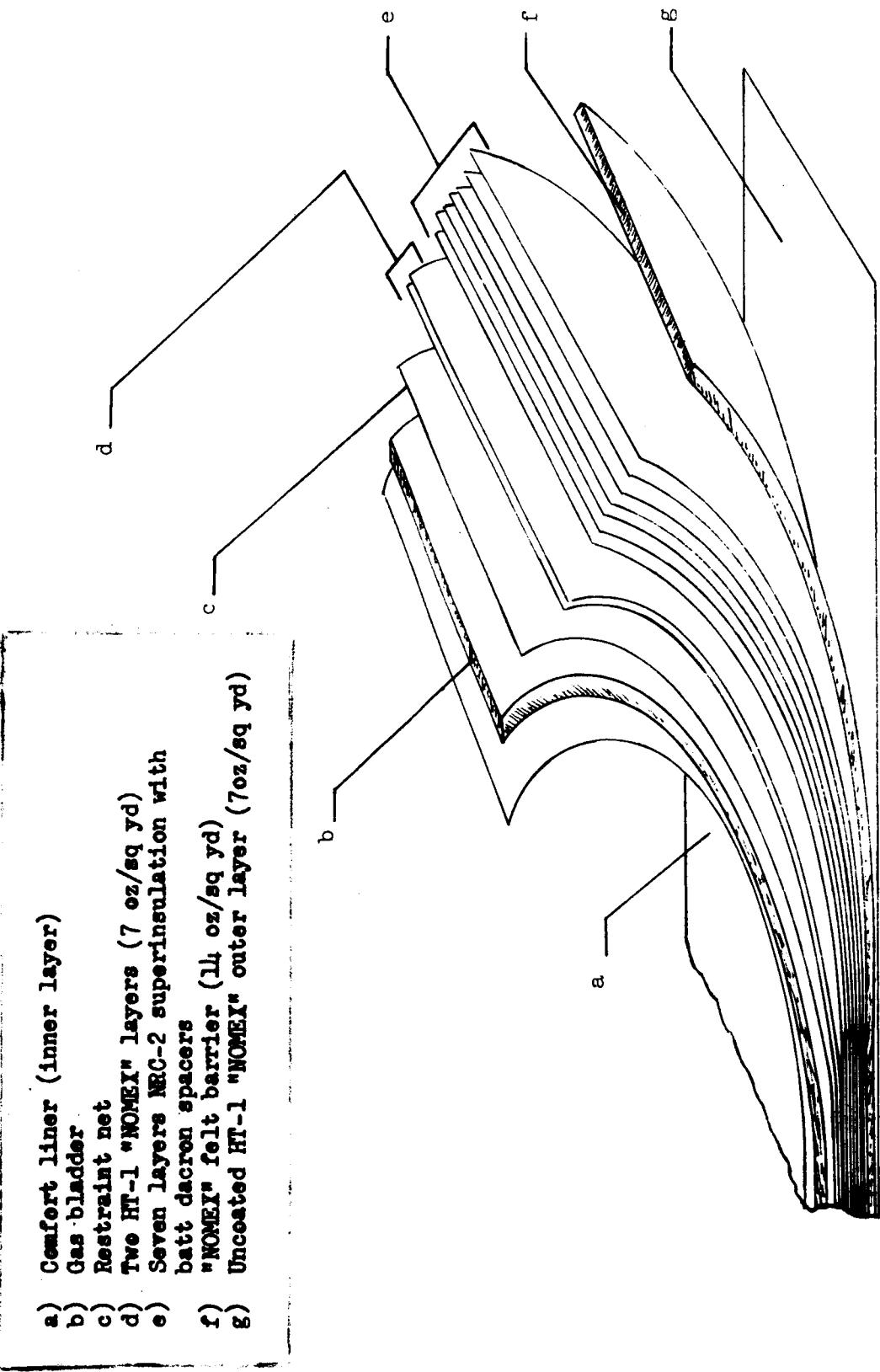


FIGURE 2

DESCRIPTION OF GEMINI EXTRAVEHICULAR SUIT LAYERS

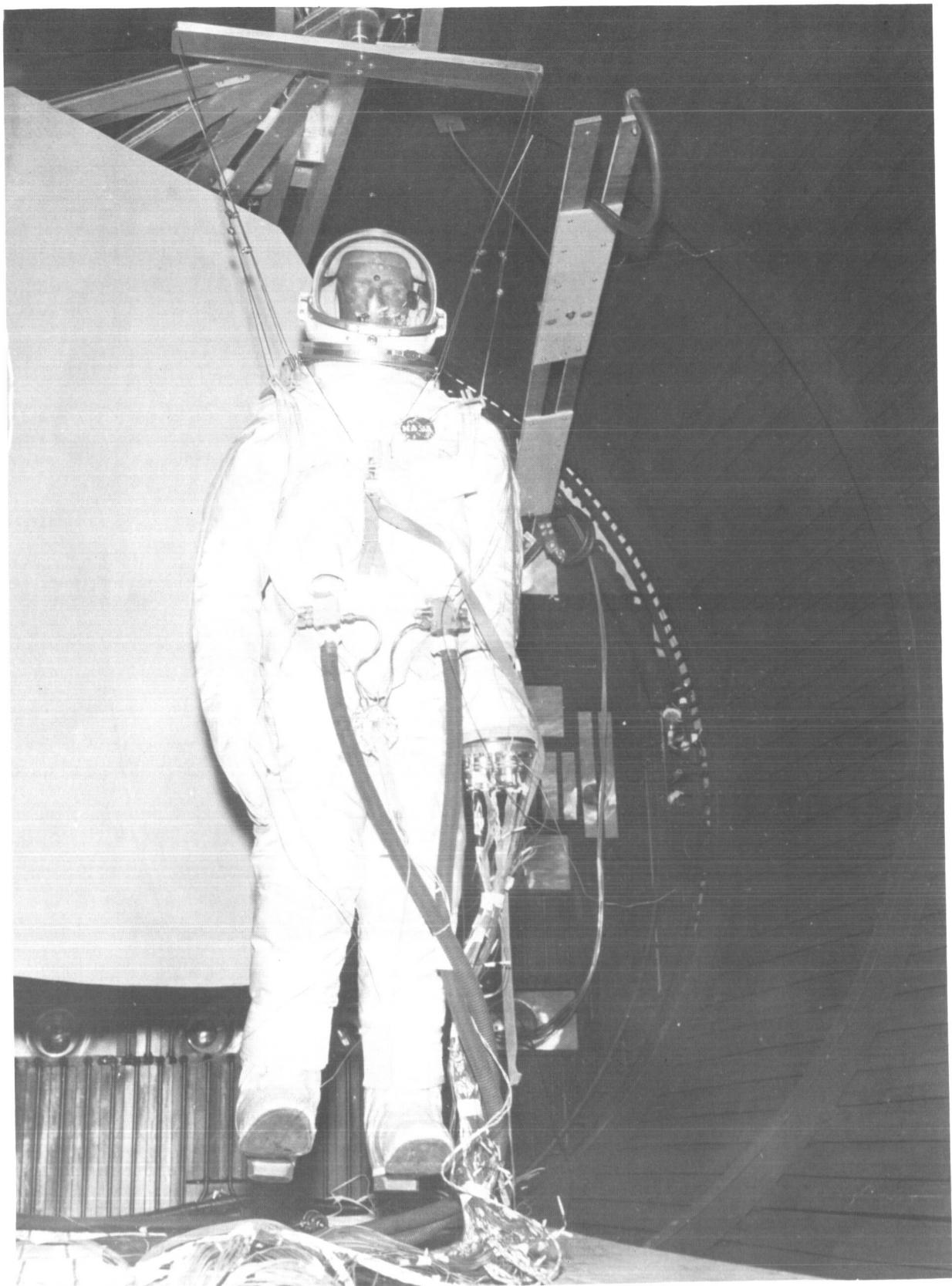


FIGURE 3 GEMINI SPACE SUIT ASSEMBLY INSTRUMENTATION DETAILS (TEST DAY #1)

3.3 TEST EQUIPMENT

3.3.1 TEST FACILITY

Experiment I-b was conducted in the LTV Space Environment Simulator (SES). The SES has a 10 ft. diameter by 10 ft. long test chamber which provides the simulated vacuum heat sink conditions of outer space and radiation of the sun. An overall view of the facility is presented by Figure 4.

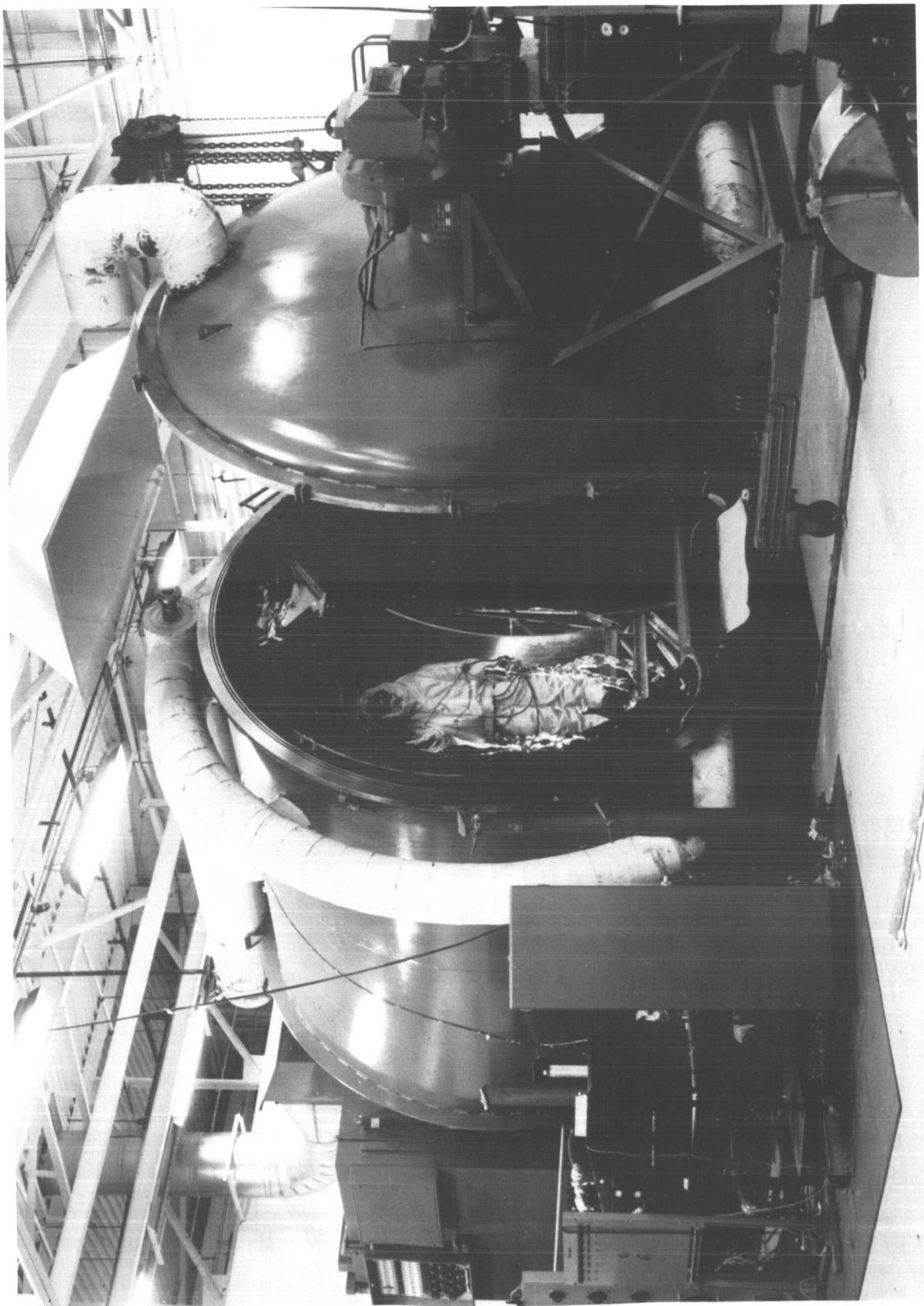
The SES vacuum capability is provided by three, 32-inch oil diffusion pumps with an ejector and mechanical forepumping system. The ultimate vacuum capability of the chamber is approximately 4×10^{-8} mm Hg. During this test, the SES pressure was maintained at approximately 5×10^{-5} mm Hg. This was the minimum pressure attainable with the suit and gas supply system leakage. Figure 5 shows chamber pressure vs time during the second day of testing and is representative of the chamber pressure throughout the entire test. Figure 5 also shows the SES pumpdown time to be approximately 3 hours.

The heat sink conditions of space are simulated by a liquid nitrogen cooled shroud or cryowall which covers the entire inner surface of the SES with the exception of two viewing ports and twenty ports used to allow passage of the solar heat flux. The total uncooled wall area represented by these ports is 3 percent of the total shroud area. The cryowall is a multifinned, aluminum tube bank cooled by liquid nitrogen. The cryowall surface was refinished recently with Minnesota Mining and Manufacturing Company Series 101C-10 Black Velvet coating which has an absorptivity of approximately 0.98 in the solar spectrum.

Simulated solar radiation is supplied by twenty, 2500-watt Mercury-Xenon high pressure arc lamps mounted outside the chamber and focused through quartz ports such that the mean flux over a six-foot plane near the center of the chamber is approximately uniform. The flux at the test plane is controllable over the range of 285 to 445 BTU/hr. ft². Power is supplied to the solar simulator lamps by a regulated power supply capable of limiting power fluctuations to +1% of the operating level.

The spectral distribution of flux from the SES solar simulator lamps is typical of Mercury-Xenon arc lamps. The spectral distribution of the lamps as installed in the SES has been measured and the results are reported in Reference 1. Table 1 is a tabulation of the spectral measurements obtained. The data presented by Table 1 are considered to be valid for Experiment I-b and do not change significantly throughout the life of the lamps. Paragraph 3.6.1 presents a discussion of the methods used during Experiment Ib to compensate for the spectral mismatch of the solar simulator lamps with the sun. Figure 6 presents the measured distribution of simulated solar flux over a plane in the SES at the point where the test specimen was located. The measurements presented by Figure 6 were obtained by scanning the test plane with a certified thermopile (Eppley Serial No. 5380) which was purchased for the solar source calibration. The measurements were made immediately before the conduct of Experiment I-b.

FIGURE 4 LTV SPACE ENVIRONMENT SIMULATOR



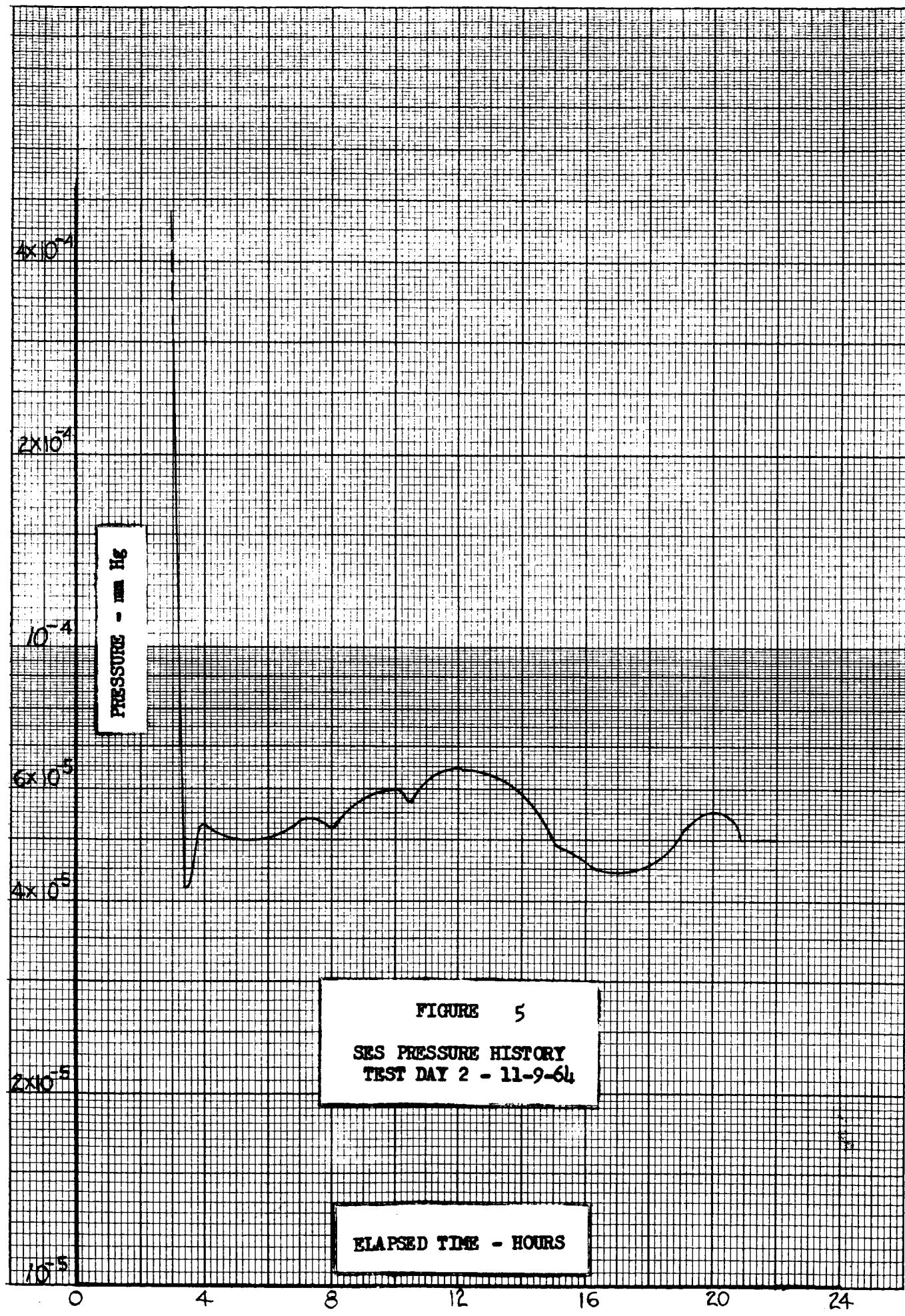


TABLE I
SPECTRAL ENERGY DISTRIBUTION OF 2.5 KVA MERCURY-XENON
(HANOVIA) SOURCES AS INSTALLED IN THE LTV SOLAR
SIMULATOR

Wavelength Band, Millimicrons	Energy in Band, Milliwatts/cm ²	Wavelength Band, Millimicrons	Energy in Band, Milliwatts/cm ²
< 260			
260	(0.5)	560-70	0.2
260-70	1.0	70-80	2.7
70-80	1.5	80-90	2.2
80-90	1.7	590-600	0.2
290-300	2.0	600-10	0.1
300-10	2.5	10-20	0.6
10-20	2.6	20-30	0.1
20-30	0.4	30-40	0.1
30-40	1.2	40-50	0.1
40-50	0.2	50-60	0.1
50-60	0.4	60-70	0.1
60-70	3.6	70-80	1.1
70-80	3.5	80-90	0.4
80-90	0.3	690-700	0.1
390-400	0.2	700-750	0.5
400-10	1.7	750-800	0.4
10-20	0.2	800-850	0.7
20-30	0.3	850-900	1.0
30-40	3.4	900-950	0.9
40-50	0.2	950-1000	1.0
50-60	0.2	1000-1100	2.0
60-70	0.1	1100-1200	1.8
70-80	0.1	1200-1300	0.9
80-90	0.1	1300-1400	1.9
490-500	0.2	1400-1500	0.4
500-10	0.1	1500-1600	0.5
10-20	0.1	1600-1700	0.5
20-30	0.1	1700-1800	0.5
30-40	0.2	1800-1900	0.2
40-50	2.5	1900-2000	0.1
550-60	0.3		
		Total	49.8 %
		UV (380 mu and below)	18.1 36
		VIS (380-750 mu)	18.9 38
		NIR (above 750 mu)	12.8 26

Source: Measurements by Dr. A. J. Drummond, Eppley Laboratories, Newport,
Rhode Island

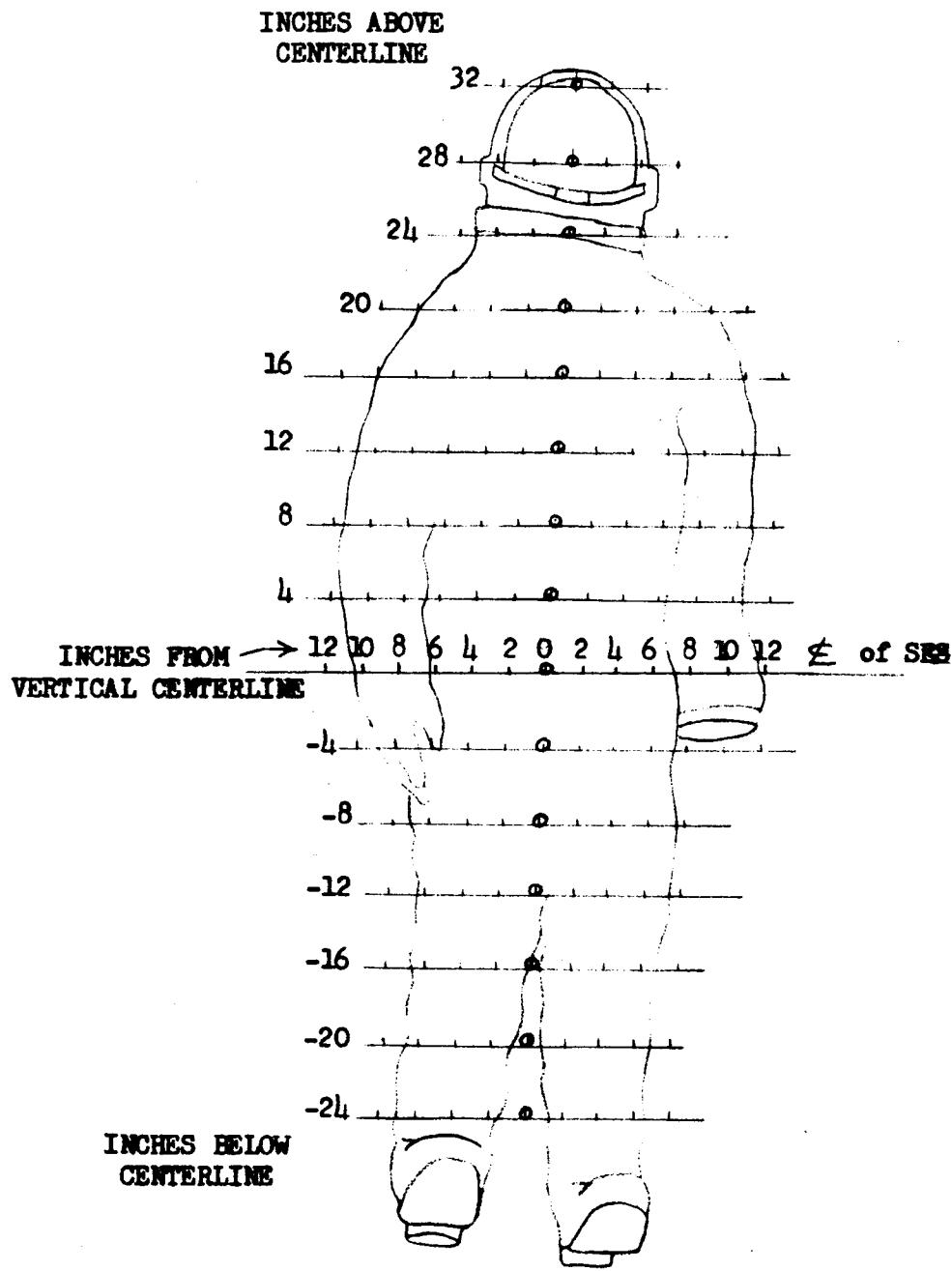


FIGURE 6a

SPECIMEN RELATIONSHIP TO SOLAR SOURCE CALIBRATION

FIGURE 6b

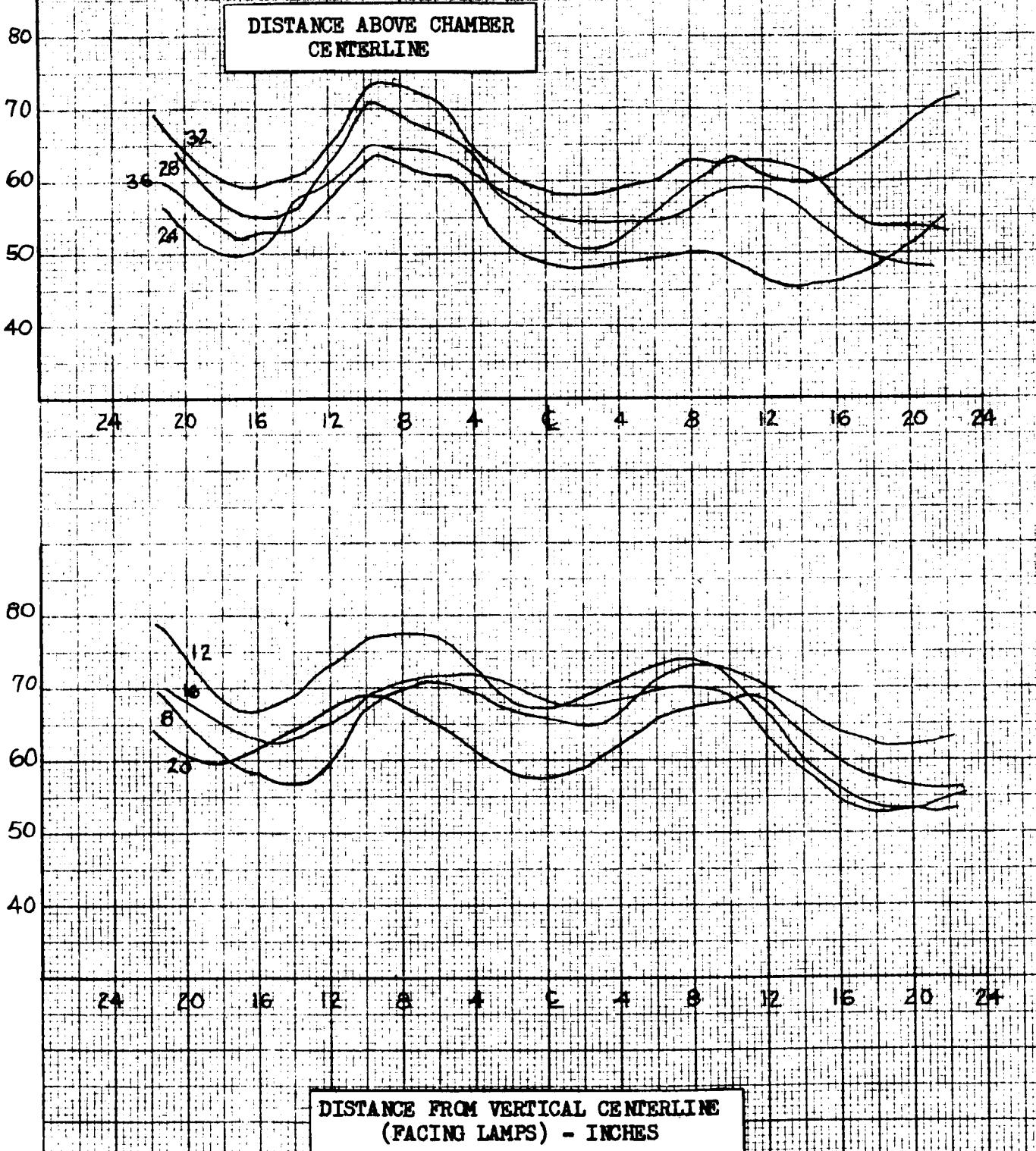
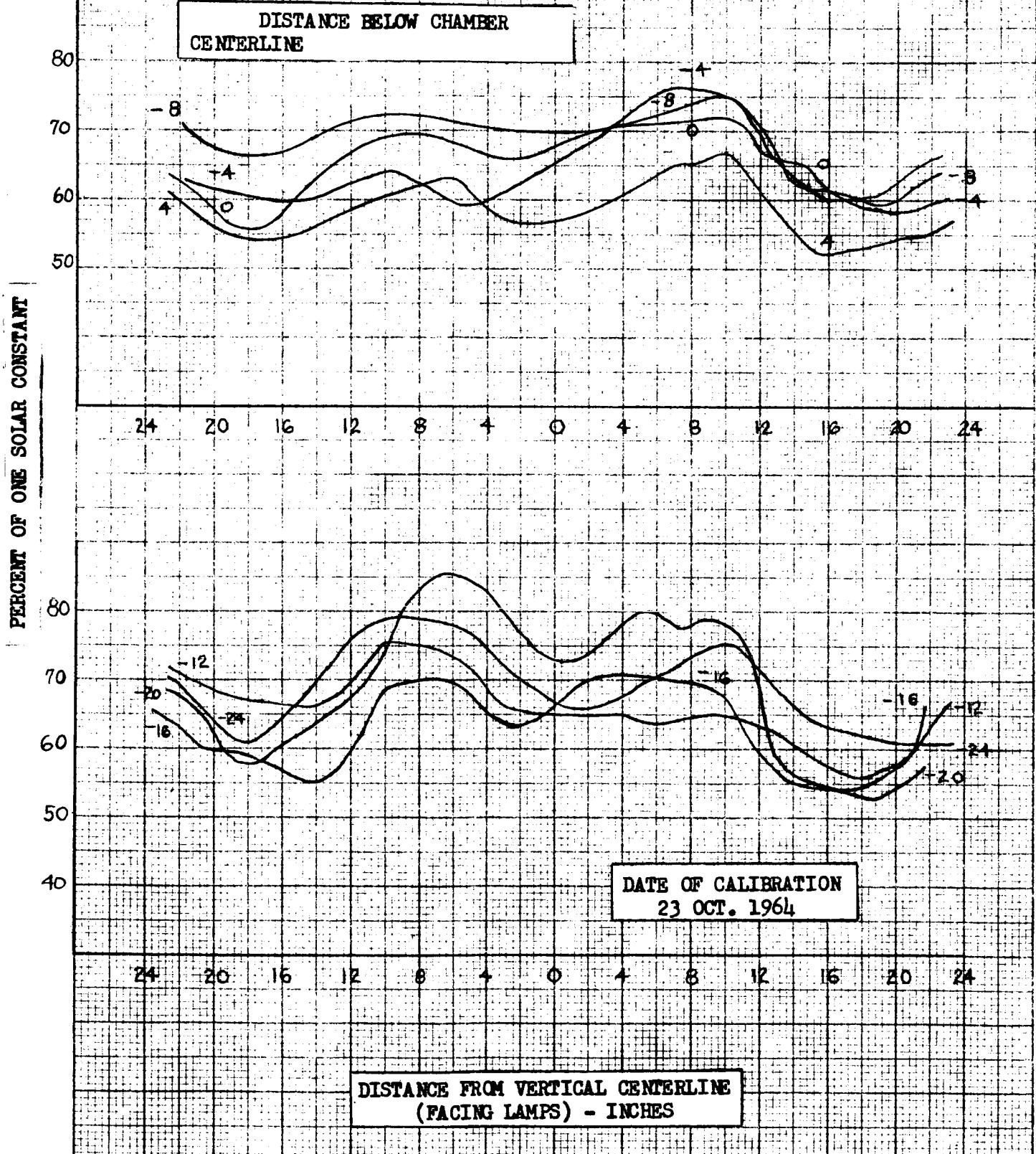
LTV SPACE ENVIRONMENT SIMULATOR
SOLAR FLUX DISTRIBUTION AT TEST
PLANE

FIGURE 6c

LTV SPACE ENVIRONMENT SIMULATOR
SOLAR FLUX DISTRIBUTION AT TEST PLANE
(CONTINUED)



3.3.2 SPECIAL TEST EQUIPMENT

3.3.2.1 Thermal Dummy

The space suit used for Experiment I-b was worn over a thermal dummy throughout the test. Figures 7 and 8 show two views of the dummy. The dummy is heated in order to simulate the sensible metabolic heat of a man and also allows duplication of suit ventilation flow patterns in the suit. The dummy is constructed such that the conductance of the shell approximates the average conductance of human skin (7 BTU/hr ft² °F).

The thermal dummy was manufactured by the Sierra Engineering Company of Sierra Madre, California. It is constructed in a phenolic-fiberglass laminate shell with articulation of the head, shoulders, hips, knees and ankles. Access is provided to the inside of the head and torso. The dummy conforms to a 15th percentile man. Each body segment has an individual electrical resistance heater circuit so that power can be supplied and controlled individually to each of the segments. A thin copper plate is formed into the fiberglass shell to insure an even distribution of heat over the surfaces of the dummy. Unheated hands and feet were used during Experiment I-b.

3.3.2.2 Earth Emission and Albedo Simulator

The earth's albedo and thermal radiation were simulated by a dished aluminum reflector (earth simulator) located opposite the test plane from the solar lamps. Figure 1 is a photograph of the test installation showing the earth simulator on the left. Strip heaters electrically insulated with glass tape were attached to the back as shown in the photograph and were used to control the earth simulator temperature and therefore its thermal radiation. The reflected solar energy from the earth was simulated by painting the side facing the lamps with paint of appropriate reflectance. Figure 9 is a photograph of the back of the suit showing the earth simulator rotated 180° from its normal position so that it is between the suit and solar lamps. In this photograph the painted side faces the front of the suit and its dull gray appearance can be compared with the shiny, bare aluminum, simulated spacecraft surface at the right. The paint used on the earth simulator was Cat-a-Lac Thermoflect 463-3-41 TRS 5569 (manufactured by Finch Paint Company). This paint has a total reflectance of 0.32 in the SES lamp spectrum and a reflectance of 0.45 in the solar spectrum. A reflectance of 0.35 is generally accepted as the average reflectance of the earth (Reference 2).

3.3.2.3 Spacecraft Surface Simulator

The curved surface shown at the right of Figure 9 was used in the evaluation of the effects of direct contact between an extravehicular suit and a spacecraft surface. The surface has the curvature of the Gemini spacecraft adapter section and can be actuated to move against the suit (Figure 10) or be retracted from it. The desired temperature of the simulated spacecraft surface can be obtained by supplying electrical energy to its electrical resistance heaters or by allowing it to cool by radiation to the SES cryowalls.



FIGURE 7 THERMAL DUMMY ASSEMBLED

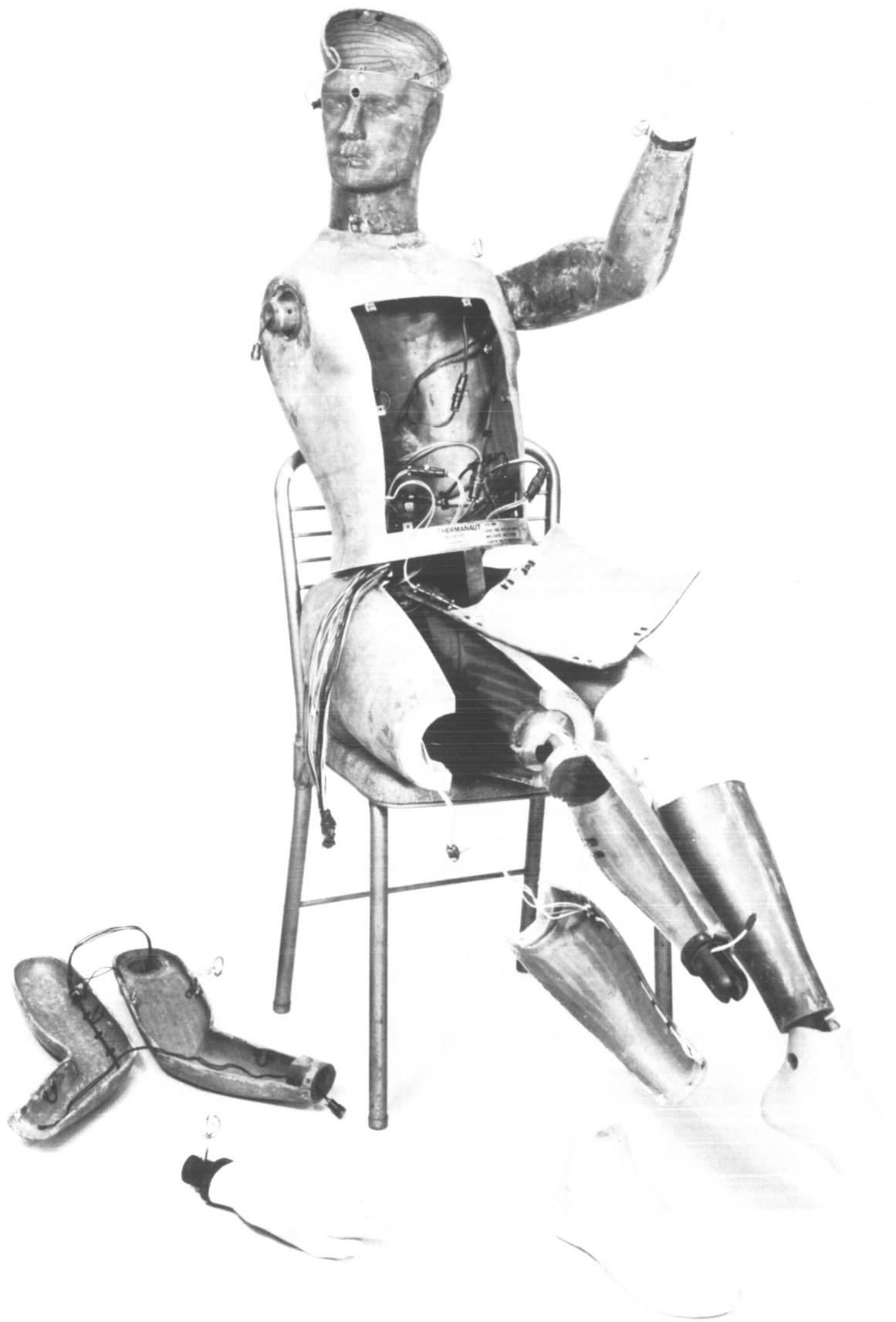


FIGURE 8 THERMAL DUMMY PARTIALLY DISASSEMBLED SHOWING SECTIONS AND HEATERS

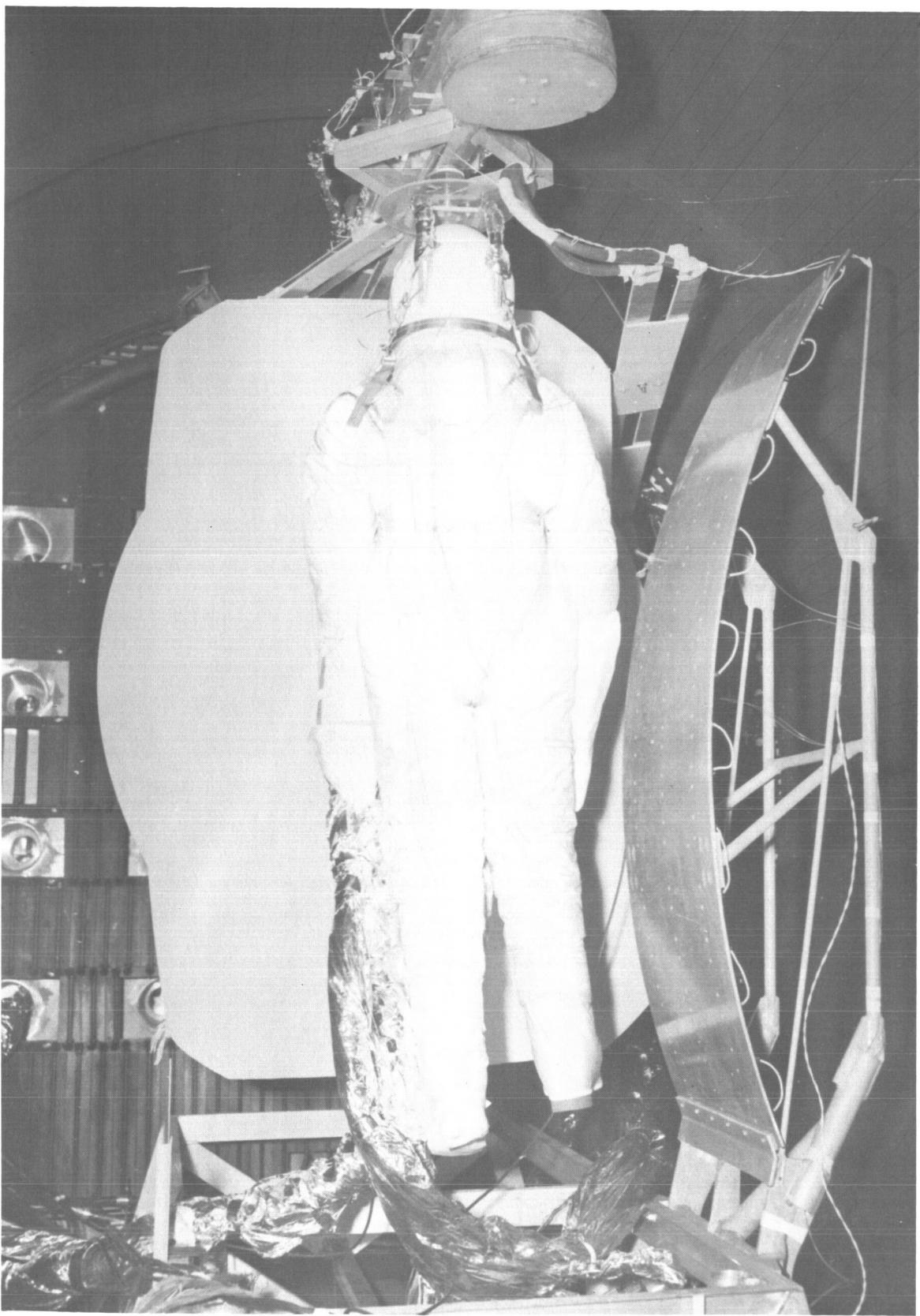


FIGURE 9 GEMINI SPACE SUIT ASSEMBLY INSTALLED IN LTV SPACE ENVIRONMENT SIMULATOR SHOWING EARTH AND SPACECRAFT SIMULATORS (REAR VIEW OF SUIT)

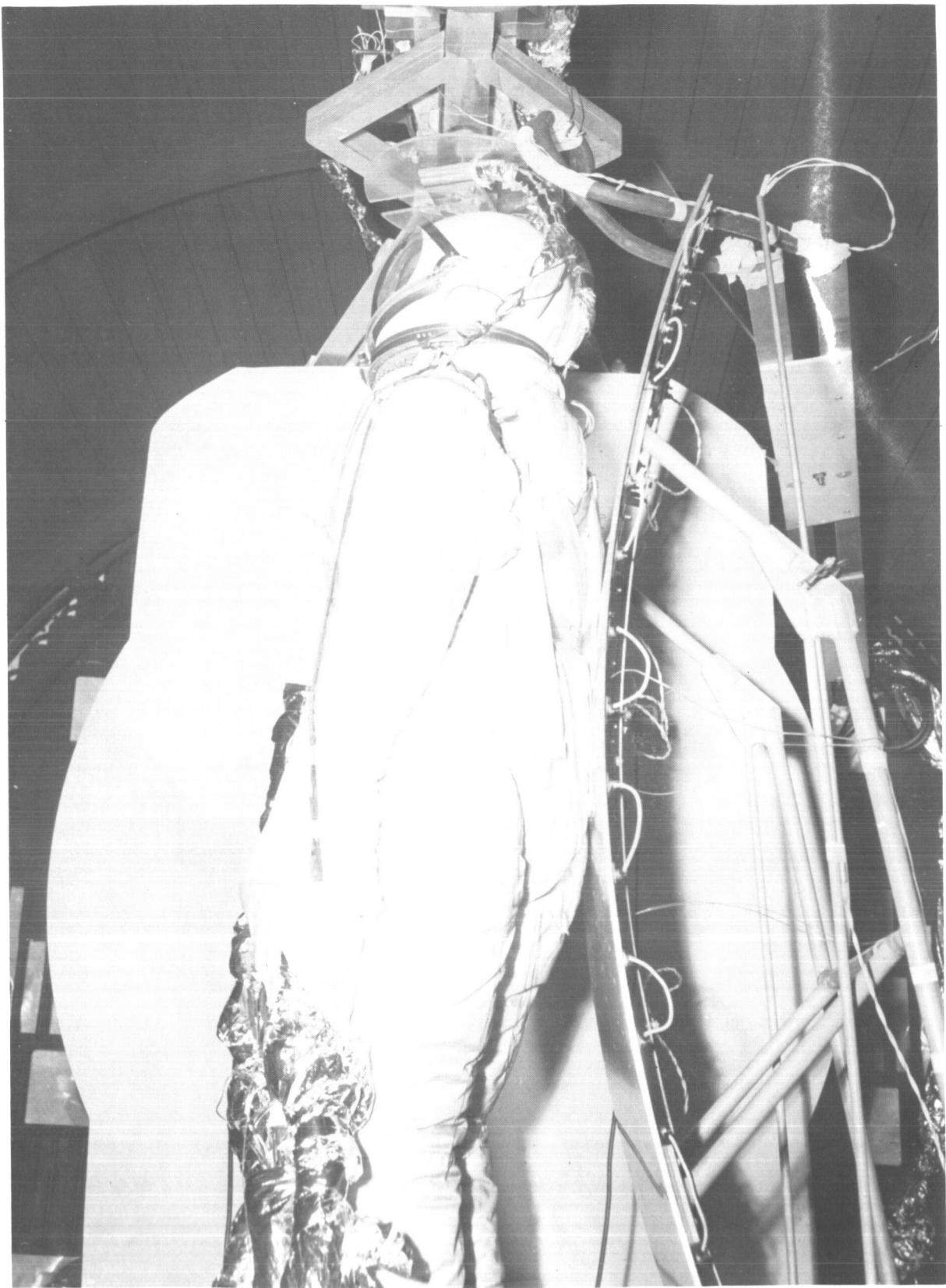


FIGURE 10 SPACECRAFT SIMULATOR IN CONTACT WITH GEMINI SPACE SUIT ASSEMBLY

Movement of the spacecraft surface simulator is accomplished by the pneumatic cylinder mechanism shown on Figure 11. The force exerted against the suit is determined by the amount of compression in a specially designed spring in the actuating mechanism. Prior to the beginning of testing the force required is preset into the actuating mechanism by bringing the spacecraft surface in contact with the suit and adjusting the amount of travel. The mechanism was adjusted prior to Experiment I-b such that the force exerted against the suit by the simulator was approximately fifteen pounds.

3.3.2.4 Specimen Rotation

The gear and rack drive mechanism shown in Figure 12 was operated by air cylinders and allowed rotation of the suit through an angle of approximately $\pm 190^\circ$. The suit rotation mechanism and earth simulator were supported by an overhead beam attached to the top of the chamber as shown in Figure 1. The simulated spacecraft surface was supported by the welded aluminum base shown in Figure 13 which fastened to rails in the bottom of the chamber.

3.3.2.5 Suit Gas Supply System

The open loop gas supply system used in the test is shown schematically in Figure 14. Two nitrogen supplies were provided; one for operation and the other for suit leakage testing. The main supply of nitrogen was regulated to atmospheric pressure then passed through a heat exchanger where its temperature could be raised or lowered as desired before entering the suit. The suit exhaust was dumped to the atmosphere vacuum pump. A suit vent line was provided to prevent suit overpressure during pumpdown. During pumpdown, valve B (Figure 14) is open to allow the suit to vent into the chamber. As operating pressures are approached, valve B is closed, valves A and C are opened, and the suit exhausts completely through the vacuum pump with positive flow through the system. During suit leakage testing valves A, B, and C are closed, valve D is opened, and the flow is measured. Valves E and F are manually controlled to provide the desired suit inlet gas temperature.

FIGURE 11 AIR CYLINDER UTILIZED TO PROVIDE MOVEMENT OF GEMINI SPACECRAFT SIMULATOR

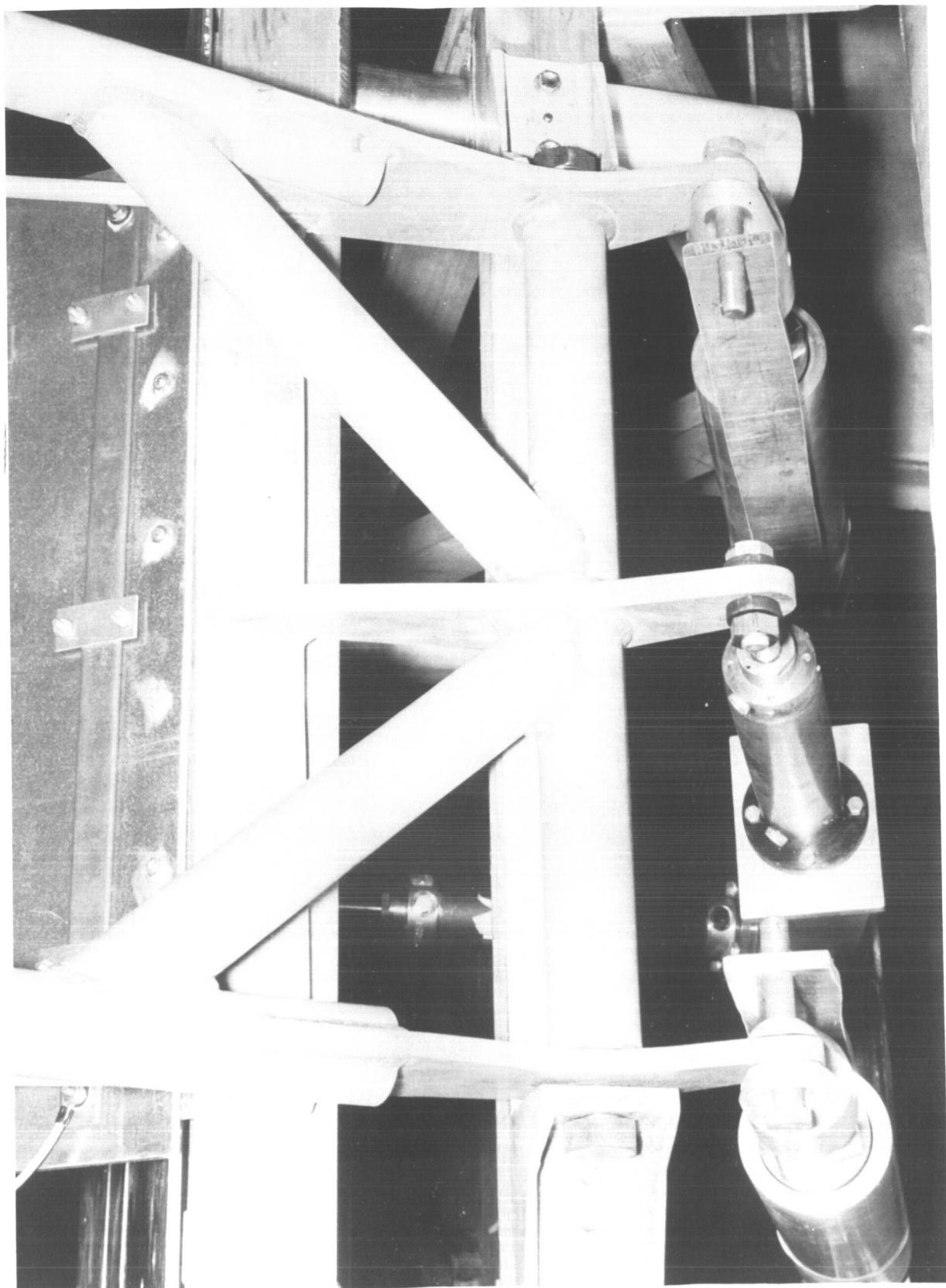


FIGURE 12 SUIT ROTATION MECHANISM

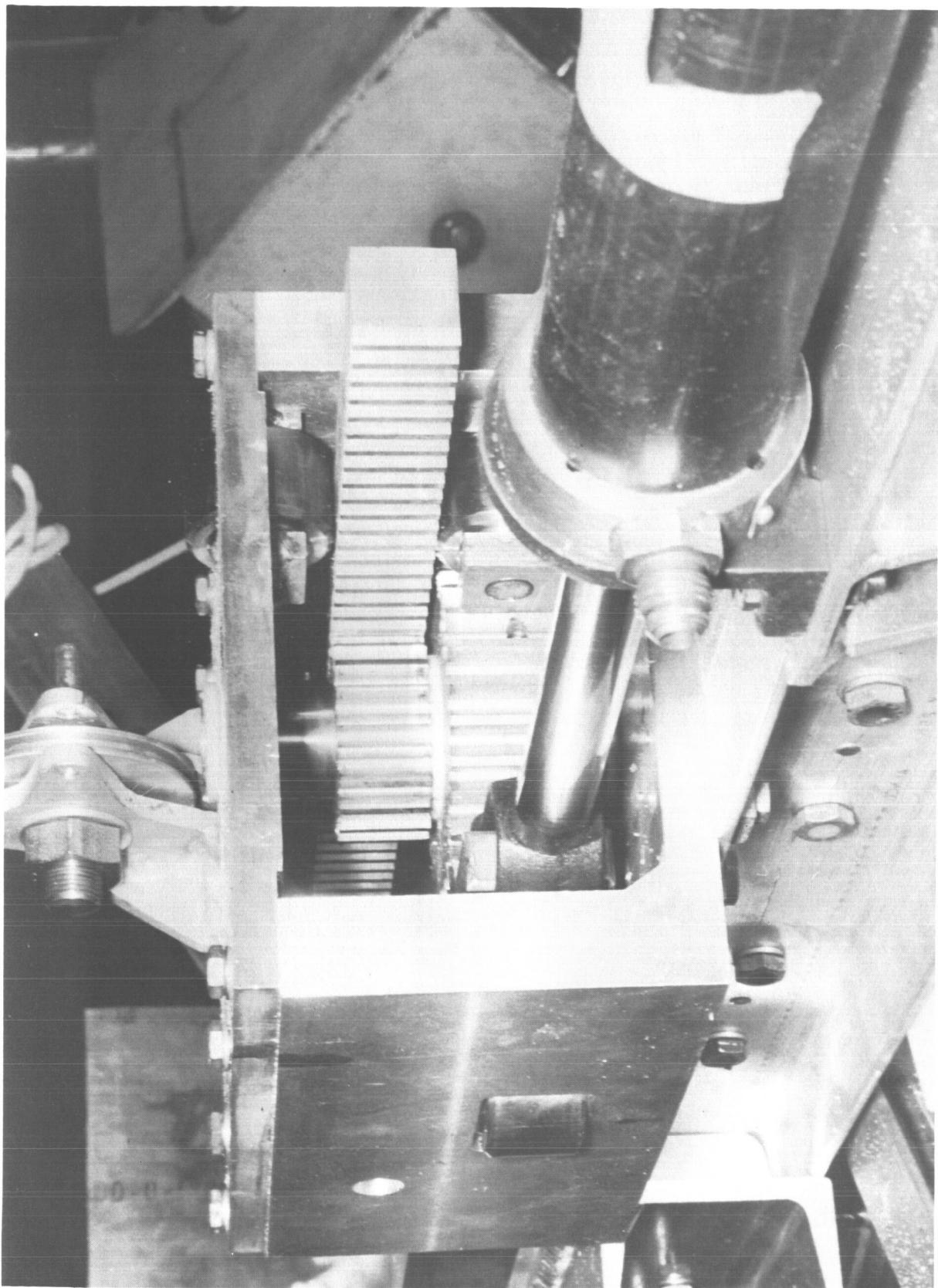
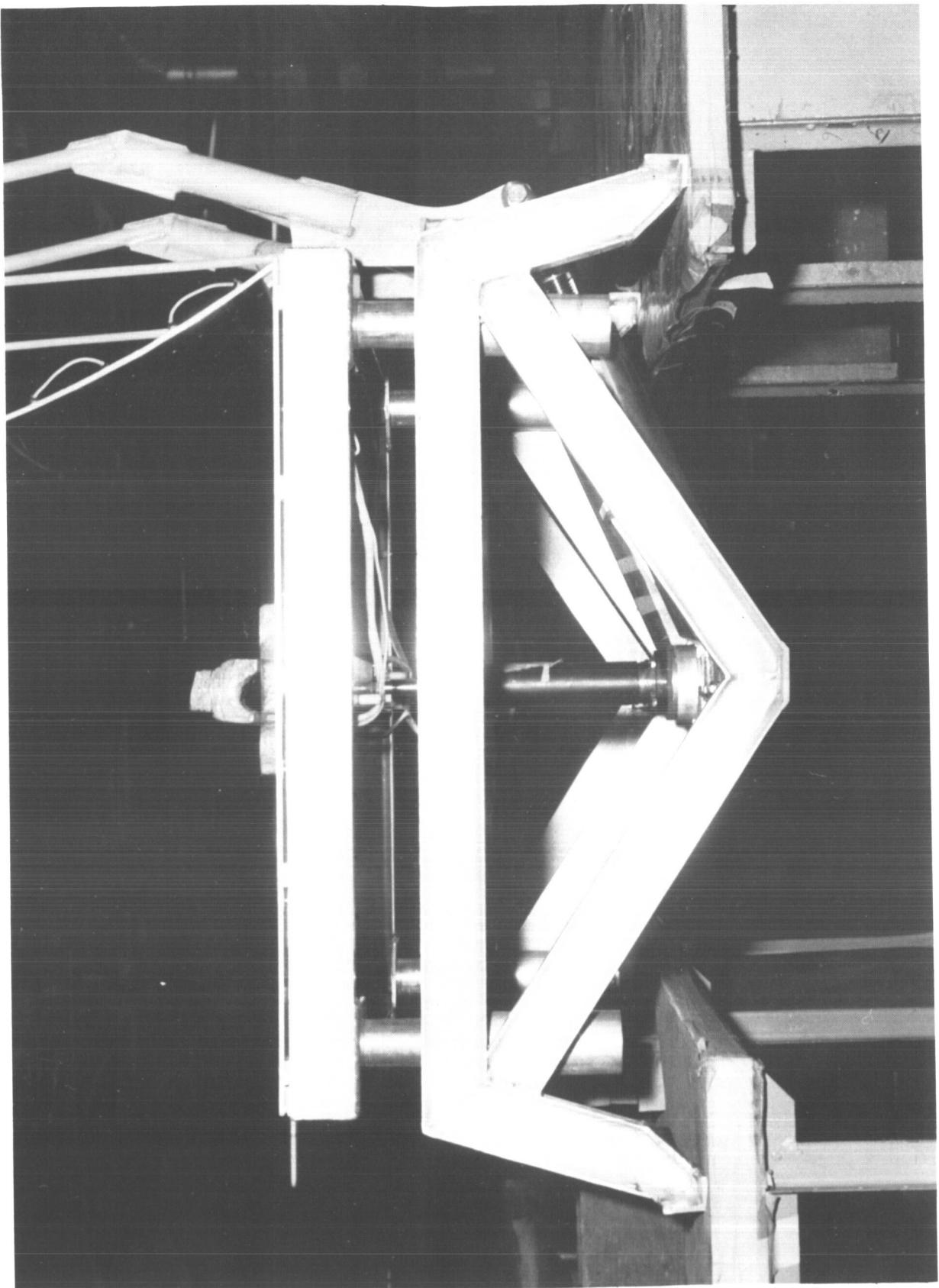


FIGURE 13 SUPPORT FOR GEMINI SPACECRAFT SIMULATOR



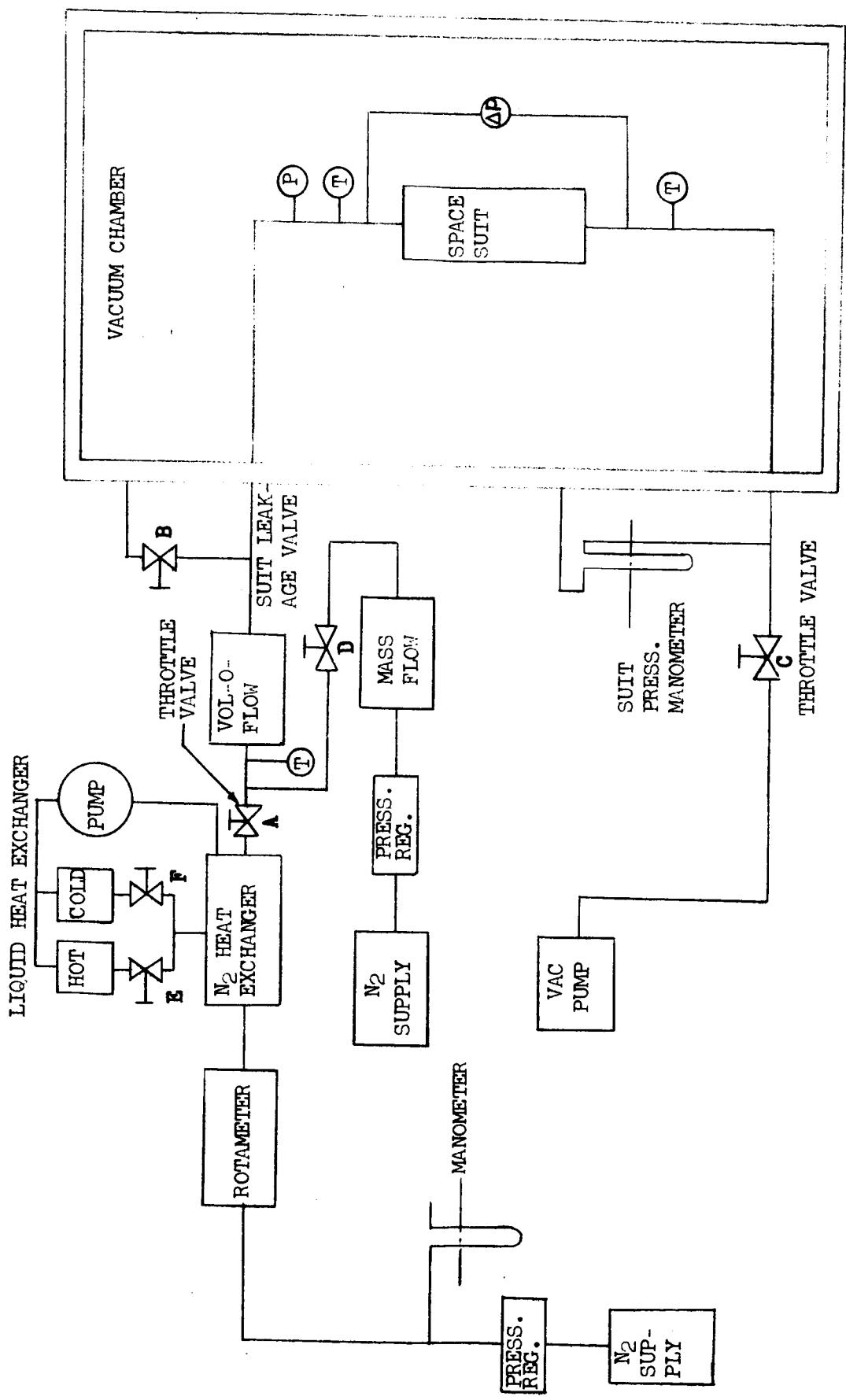


FIGURE 14
SUIT FLOW SYSTEM - EXPERIMENT Tb

3.4

INSTRUMENTATION

Instrumentation was selected for Experiment I-b which would:

- (a) Provide suit test data required to make the evaluations and determinations stated by the test objectives in paragraph 3.1;
- (b) Determine the degree to which the tests simulated the actual orbit conditions represented by the test points;
- (c) Monitor the progress of the test and the facility operation.

This section of the report describes the measurements that were made, data acquisition equipment, measurement and recording techniques, and an error analysis of the data as recorded.

3.4.1 MEASUREMENTS ON SUIT AND THERMAL DUMMY

Temperatures - The suit and dummy were instrumented for temperature measurements on the dummy surfaces, constant wear garment (underwear), inside and outside suit surfaces, selected interlayer locations, and on the helmet. The measurement locations were selected to provide data on suit hot and cold spots, material performance, thermal dummy temperatures and control, suit thermal response, and the effects of mission and configuration variables.

Figures 15 through 18 and Table II present a complete list and description of the temperature measurements with their corresponding recorder channel number. The locations presented by Table II were coordinated with the contract technical monitor.

All temperature measurements on Experiment I-b were made by copper-constantan thermocouples. All thermocouples, except those used for ventilation gas temperature measurements, were constructed of forty-gauge wire (0.003 in. diameter) and beaded by a resistance welder. Forty-gauge wire was utilized for the thermocouples in order to minimize the effects of possible measurement error due to thermal conduction along the lead wire to or from the junction.

Thermocouples located on the outer fabric surfaces of the suit were sewn into the material and secured with the junction in contact with the fabric. The thermocouple junctions were painted with Finch Paint Co. "Cat-A-Lac" white paint previous to installation. This paint has emissive properties comparable to the HT-1 suit cover and was applied in order to reduce possible temperature errors resulting from differences between the emissive properties of the thermocouples and the surrounding fabric to which they were attached.

Thermocouples located on the NRC-2 suit superinsulation were attached by aluminized mylar tape. The thermocouples on metal surfaces were attached by electric welding where possible and Humiseal cement was used for

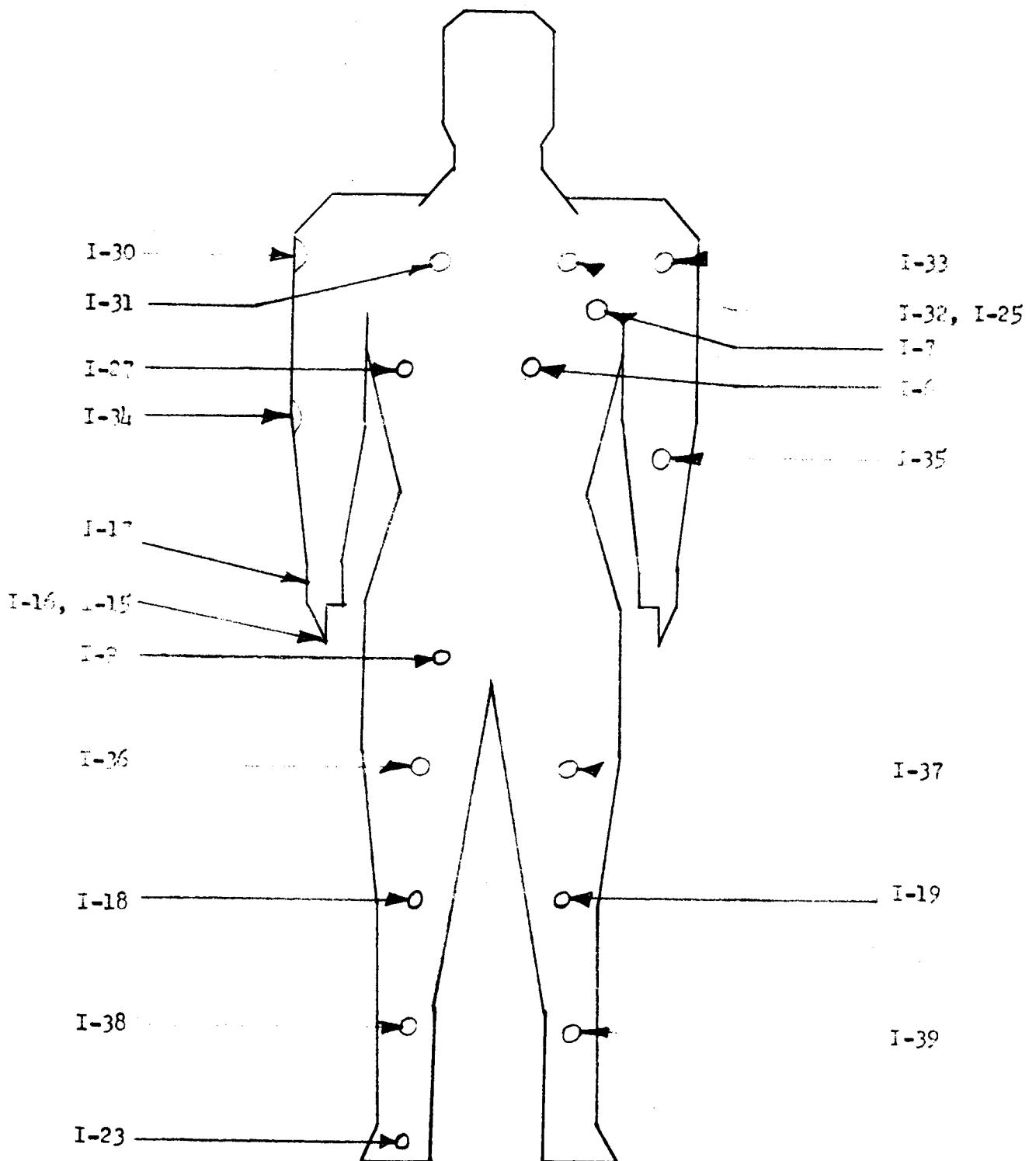


FIGURE 15

THERMOCOUPLE LOCATIONS ON FRONT SURFACE OF
THERMAL DUMMY AND CONSTANT WEAR GARMENT

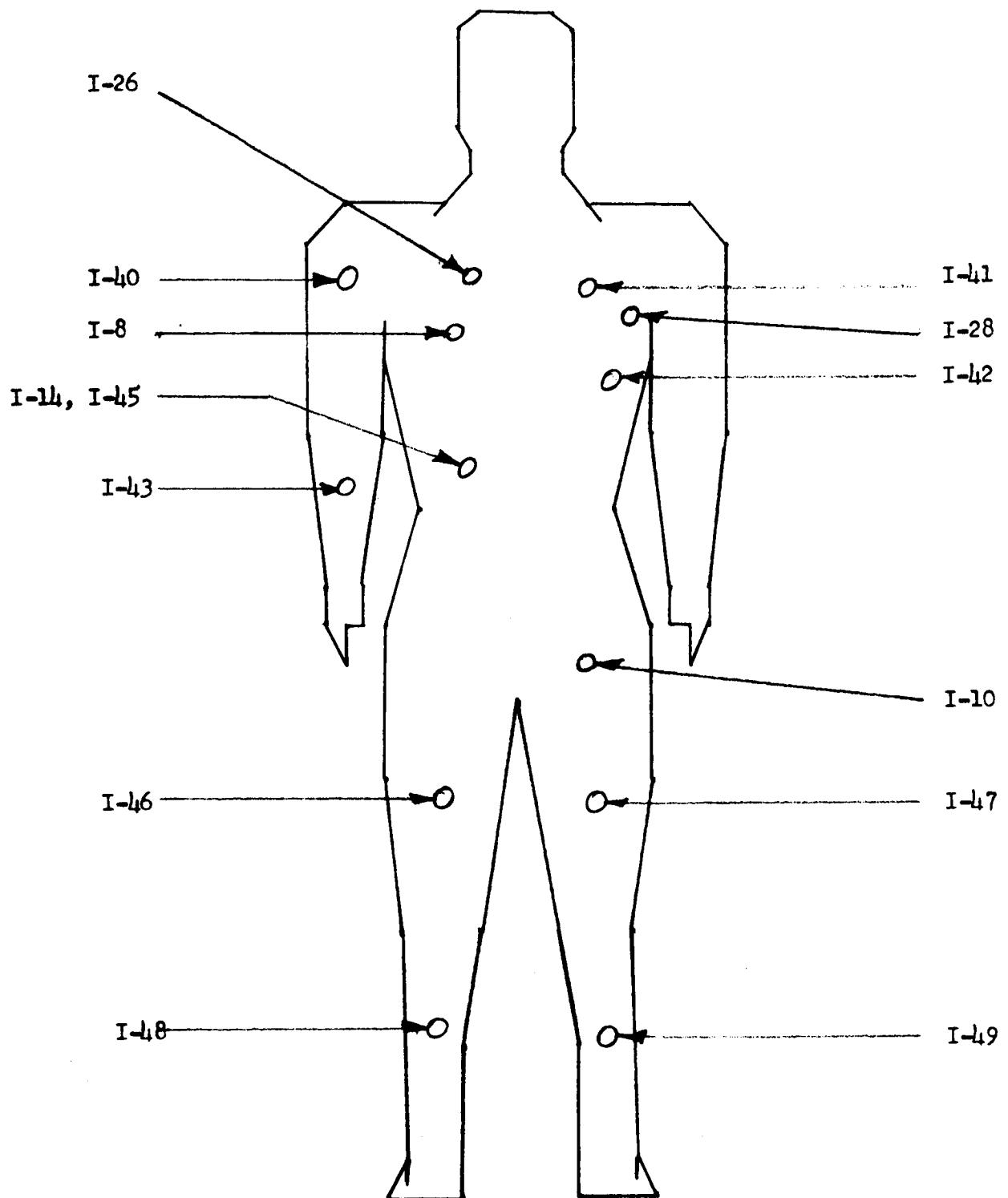


FIGURE 16

THERMOCOUPLE LOCATIONS ON BACK SURFACE OF
THERMAL DUMMY AND CONSTANT WEAR GARMENT

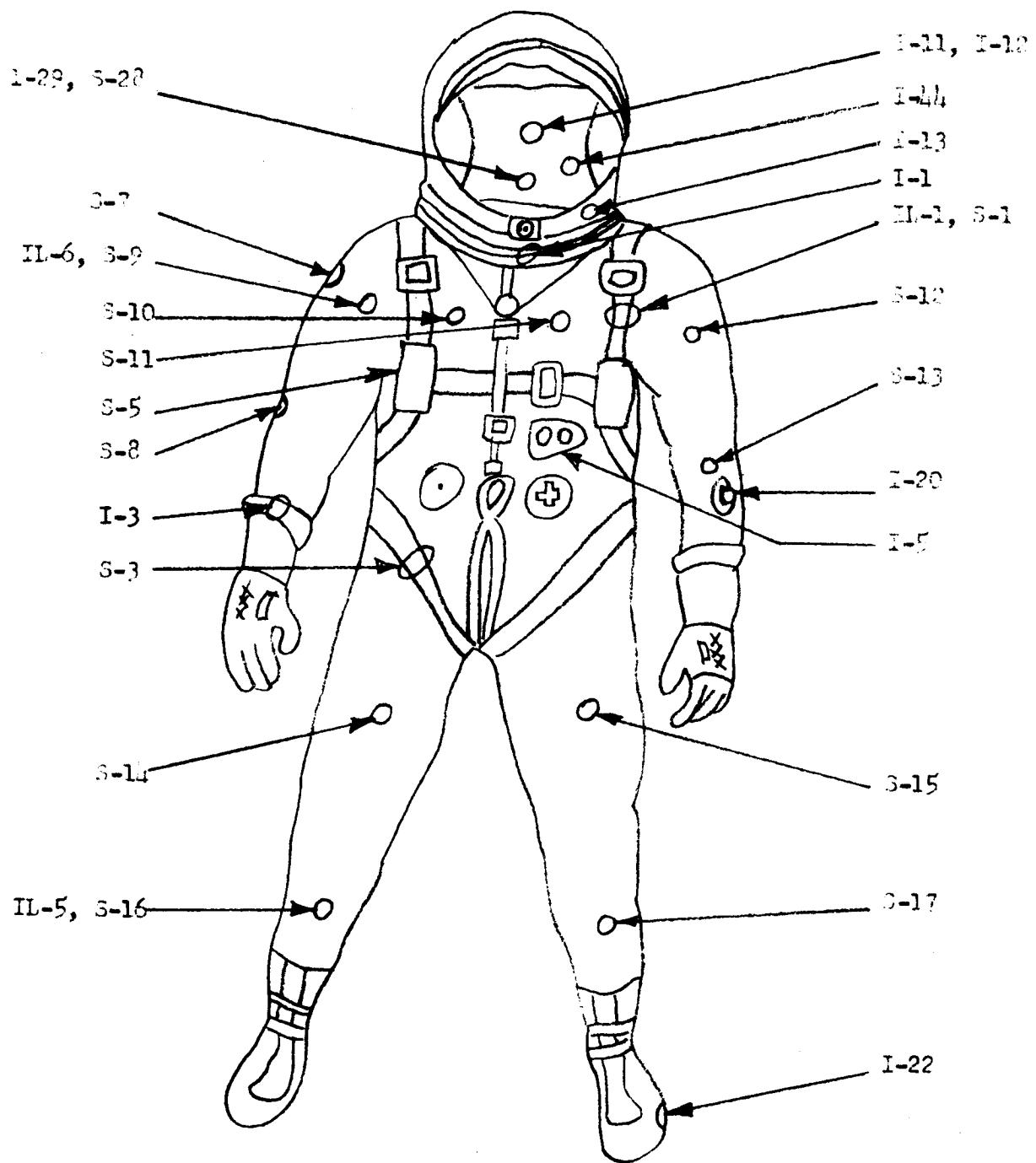


FIGURE 17

THERMOCOUPLE LOCATIONS ON INTERIOR AND EXTERIOR
SURFACES ON FRONT OF GEMINI SPACE SUIT

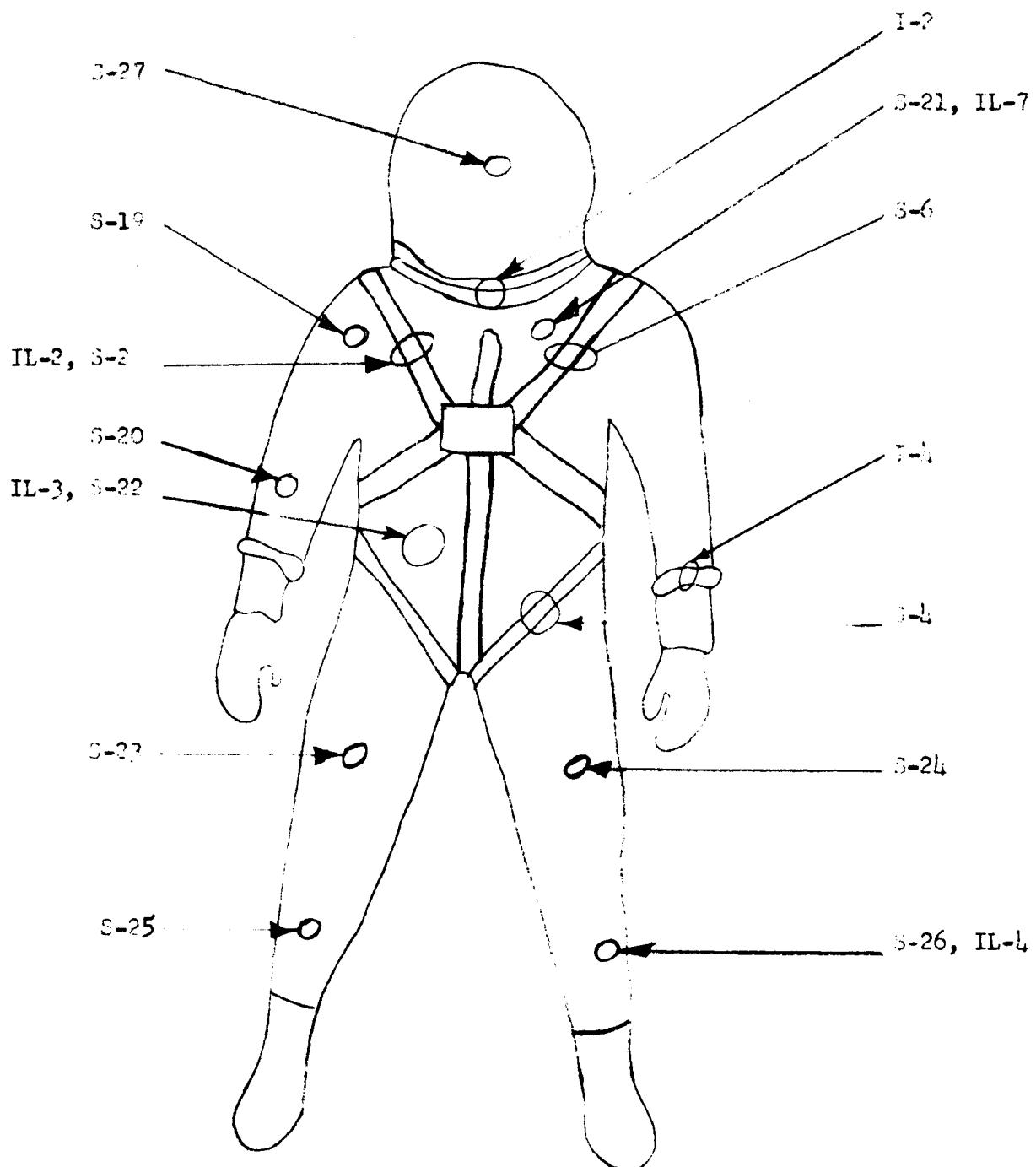


FIGURE 18
THERMOCOUPLE LOCATIONS ON INTERIOR AND EXTERIOR
SURFACES ON BACK OF GEMINI SPACE SUIT

TABLE II
EXPERIMENT I-b THERMOCOUPLE LOCATIONS

LOCATION CODE:

I - Inside Pressure Garment
IL - Thermal Garment
S - Exterior Surface of Thermal Garment and Helmet

CHAN. NO.	CODE	LOCATION AND REMARKS
1	I-1	Front of helmet disconnect bearing
2	I-2	Back of helmet disconnect bearing
3	I-3	Front of right glove disconnect bearing
4	I-4	Back of right glove disconnect bearing
5	I-5	Interior of pressure suit between bio-communications connector and blood pressure fitting
6	I-6	Constant wear garment, under front buckle on horizontal harness strap
7	I-7	Constant wear garment in area of suit interlayer thermocouples on front of suit coded IL-1 - Open during test
8	I-8	Constant wear garment in area of suit interlayer thermocouples on upper back coded IL-2
9	I-9	Constant wear garment at upper, right, front thigh - under harness
10	I-10	Constant wear garment at upper, right, rear thigh - under harness
11	I-11	Helmet at back, between helmet pad and helmet outer shell on days #1 and 2. On day #3, helmet bearing at right side under dummy right ear
12	I-12	Helmet pad between dummy head and pad
13	I-13	Helmet on metal surface at front near microphone
14	I-14	Constant wear garment at back in area of suit interlayer - thermocouples - lower, left, back

TABLE II (Continued)

CHAN. NO.	CODE	LOCATION AND REMARKS
15	I-15	Cotton glove on end of index finger
16	I-16	Cotton glove on end of little finger
17	I-17	Cotton glove on back of right hand
18	I-18	Constant wear garment in right knee cap area
19	I-19	Constant wear garment in left knee cap area
20	I-20	Inside pressure suit on interior side of suit pressure gage
21	I-21	Sock on bottom of right foot
22	I-22	Outer left side of left boot at sole and super insulation interface
23	I-23	Sock on top, front of right foot under boot "lacing" zipper
24	I-24	Sock on bottom of left foot
25	I-25	Constant wear garment on upper left chest
26	I-26	Constant wear garment on upper left back
27	I-27	Constant wear garment in right chest area under harness
28	I-28	Constant wear garment in right back area under harness
29	I-29	Interior, center of helmet visor
NOTE: Thermoouple Numbers 30 - 43 and 45 - 59 were located on the dummy surface in the following locations:		
30	I-30	Outer, upper, right arm (shoulder)
31	I-31	Upper, right chest area
32	I-32	Upper, left chest area
33	I-33	Front, upper, left arm
34	I-34	Outer, lower, right arm (elbow)
35	I-35	Front, lower, left arm

TABLE II (Continued)

CHAN. NO.	CODE	LOCATION AND REMARKS
36	I-36	Front, upper, right thigh
37	I-37	Front, upper, left thigh
38	I-38	*Front, lower, right shin
39	I-39	*Front, lower, left shin
40	I-40	*Back, upper, left arm
41	I-41	*Upper right back
42	I-42	Under right shoulder blade
43	I-43	Back, left, lower arm
44	I-44	Inside helmet on visor near reflector used for visor frosting indication
45	I-45	Lower left back in area of suit interlayer thermocouples coded IL-3
46	I-46	Back, upper, left thigh
47	I-47	Back, upper, right thigh
48	I-48	Back, lower, left leg
49	I-49	Back, lower, right leg
<hr/>		
		IL-1 interlayer temperature measurements in upper, left chest area, under harness
50	IL-1-b-1	Exterior side of nomex felt - open during test
51	IL-1-b-2	Interior side of nomex felt - open during test
52	IL-1-c-2b	Exterior side of second layer of aluminized mylar - open during test
53	IL-1-c-2d	Exterior side of fourth layer of aluminized mylar - open during test
54	IL-1-c-2f	Exterior side of sixth layer of aluminized mylar - open during test
55	IL-1-c-1	*Between interior layers of nylon cloth, open on days #1 and #2. On day #3, this channel was used to monitor a thermocouple on the suit front surface near the helmet hold - down pulley

TABLE II (Continued)

CHAN NO.	CODE	LOCATION AND REMARKS
		IL-2 interlayer temperature measurements in upper, left, back area, under harness
56	IL-2-b-1	Exterior side of nomex felt - open during test
57	IL-2-b-2	Interior side of nomex felt
58	IL-2-c-2b	Exterior side of second layer of aluminized mylar - open during test
59	IL-2-c-2d	Exterior side of second layer of aluminized mylar
60	IL-2-c-2f	Exterior side of sixth layer of aluminized mylar - open during test
61	IL-2-e-1	Between interior layers of nylon cloth - open during test
		IL-3 interlayer temperature measurements in lower, left back area, not under harness
62	IL-3-b-1	Exterior side of nomex felt
63	IL-3-b-2	Interior side of nomex felt
64	IL-3-c-2b	Exterior side of second layer of aluminized mylar
65	IL-3-c-2d	Exterior side of fourth layer of aluminized mylar - open during test
66	IL-3-c-2f	Exterior side of sixth layer of aluminized mylar - open during test
67	IL-3-e-1	Between interior layers of nylon cloth
		Thermocouple No. 68-94 are located on the suit surface as follows:
68	S-1	Front, upper, left chest area under harness - Note: Exposed during test due to harness distortion
69	S-2	Back, upper, left area under harness
70	S-3	Front, upper, right, thigh area, under harness
71	S-4	Back, upper, right, thigh area under harness - Note: Exposed due to harness distortion
72	S-5	Front, right, chest area under harness

TABLE II (Continued)

CHAN. NO.	CODE	LOCATION AND REMARKS
73	S-6	Upper, right, back area under harness
74	S-7	Upper, outer, right arm (shoulder)
75	S-8	Lower, outer, right arm (elbow)
76	S-9	Front, upper, right arm
77	S-10	Upper, right chest
78	S-11	NASA insignia patch, upper, left chest
79	S-12	Front, upper, left arm
80	S-13	Front, lower, left arm
81	S-14	Front, right, thigh
82	S-15	Front, left, thigh
83	S-16	Front, left shin
84	S-17	Front, right, shin
85	S-18	Back, under right shoulder blade. Note: This thermo-couple was no good. It indicates as increasing temperature when temperature is decreasing and vice-versa. The Cu-Cu leads were reversed at a junction.
86	S-19	Back, upper, left arm
87	S-20	Back, lower, left arm
88	S-21	Upper, right, back
89	S-22	Lower, left, back
90	S-23	Back, left, thigh
91	S-24	Back, right, thigh
92	S-25	Back, lower, left leg
93	S-26	Back, lower, right leg
94	S-27	Back, exterior helmet shell
95	G-1	Suit "nitrogen out" temperature #1, 24 gage thermocouple connected in parallel with thermocouple #128 on day #1 only.

TABLE II (Continued)

CHAN. NO.	CODE	LOCATION AND REMARKS
96	G-2	Suit "nitrogen in" temperature #1, 24 gage thermocouple on days #1 and #2. 36 gage thermocouple on day #3. Connected in parallel with thermocouple #127 on day #1 only.
97	A-1	Top, right albedo simulator back.
98	A-2	Top, left albedo simulator back
99	A-3	Left, center albedo simulator back
100	A-4	Bottom, left albedo simulator back
101	A-5	Bottom, right albedo simulator back
102	A-6	Right, center albedo simulator back
103	SPC-1	*Near top of spacecraft simulator, used on day #3 only
104	SPC-1	*Near center of spacecraft simulator, used on day #3 only
NOTE: Channels 105 - 108 were not used during this test		
109	W-1	*SES Chamber Walls
110	W-2	*SES Chamber Walls
111	W-3	*SES Chamber Walls
112	W-4	*SES Chamber Walls
113	W-5	*SES Chamber Walls
114	W-6	*SES Chamber Walls
115		Mounted near I-31 with fiberglass tape
116		Mounted near I-45 with fiberglass tape
117		Thermopile inlet water
118		Thermopile outlet water

TABLE II (Continued)

CHAN. NO.	CODE	LOCATION AND REMARKS
119		Open - Not used
120	S-28	Outside surface of pressure visor
121		Outside surface of gas inlet thermocouple manifold
122		Outside surface of gas outlet thermocouple manifold
123	IL-4	Nomex felt at back of right leg
124	IL-5	Nomex felt at front of right leg
125	IL-6	Nomex felt at front of right arm
126	IL-7	Nomex felt at back of right shoulder
127		*Suit "nitrogen in" temperature #2 24 gage thermocouple. Connected in parallel with thermocouple #96 on day #1 only (Downstream from thermocouple #96)
128		*Suit "nitrogen out" temperature #2 connected in parallel with thermocouple #95 on day #1 only. 24 gage thermocouple days #1 and #2. Changed to 36 gage thermocouple on day #3 (upstream from thermocouple 95)
		*On 32° F reference junction, all others on 150° F reference junction.

attachment on the thermal dummy and fabrics inside the suit. Visor and helmet thermocouples were secured by transparent Scotch tape.

The thermocouple recording system is shown in diagram form in Figure 19.

Pressures - Suit pressures were measured during this test to provide both suit gas flows and a history of pressure within the suit. Pressures were measured at the suit inlet and in the visor area while a differential pressure across the inlet and exit were measured.

The suit inlet pressure transducer (Dynisco Model APT 25-10) was mounted on a manifold in the nitrogen inlet hose at a point near the entrance to the suit. The temperature of the inlet nitrogen was sufficiently high to keep the transducer temperature within its specified temperature range of -65°F to $+300^{\circ}\text{F}$. The helmet pressure transducer, also Dynisco APT 25-10, was cemented under the chin of the dummy with Densifoam cement. The temperature inside the helmet was within the specified operating temperature range of the transducer. The suit pressure drop transducer (Dynisco Model PT 14-05) was connected between the inlet gas manifold and the outlet gas manifold. A strip heater was installed on this transducer to maintain the temperature of the transducer within its specified operating temperature range of -65°F to $+300^{\circ}\text{F}$. Each of the exposed pressure transducers was wrapped with superinsulation to reduce radiant heat loss to the chamber walls.

The pressure transducers incorporate a miniature unbonded strain gauge in the configuration of a four active-arm resistive wheatstone bridge. The output voltages of the three gauges were connected to a bridge balance box which served to zero the gauges at some reference pressure. The signals from the bridge balance box were recorded by a CEC Model 5-123 recording oscillograph which provided a continuous record of suit pressures throughout the test. Figure 20 shows a block diagram of the suit pressure instrumentation.

Suit Leakage - The suit leakage to low vacuum environment of orbit must be determined to ascertain the endurance capability in orbit. This test arrangement utilized a Hastings-Radist LF-1000, 0 to 1000 sccm mass flowmeter installed in a suit feed line (Figure 14) to determine the suit leakage. An additional indication of leakage which might develop during the course of a test was provided by six Phillips cold cathode ionization gages (CEC Model PHG-026) mechanically positioned around the exterior of the suit. These gauges were ceded and positioned as follows:

- P-1 - Zipper in crotch area.
- P-2 - Biomedical connector.
- P-3 - Right wrist disconnect bearing.
- P-4 - Left wrist disconnect bearing.
- P-5 - Helmet disconnect bearing.
- P-6 - Zipper area on back.

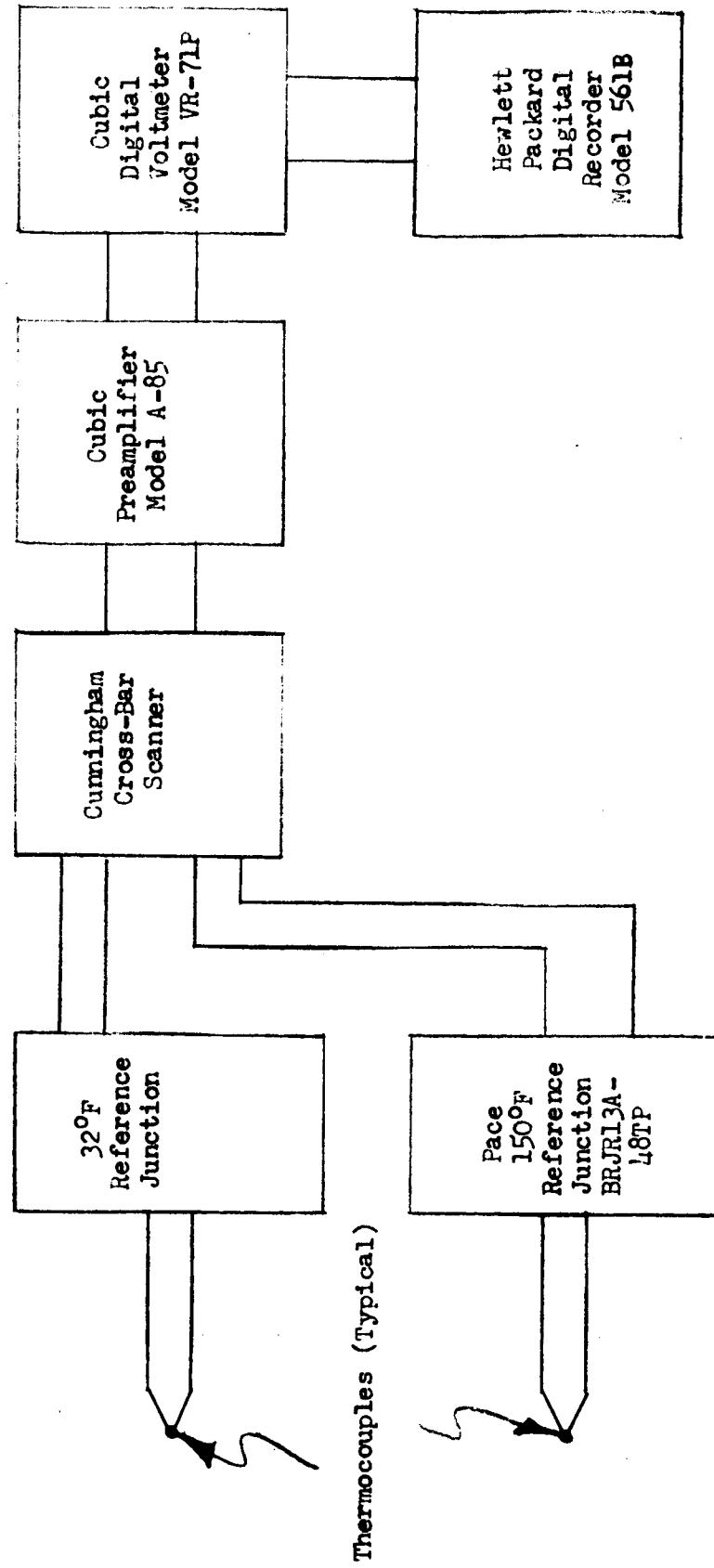


FIGURE 19
BLOCK DIAGRAM OF THERMOCOUPLE RECORDING SYSTEM

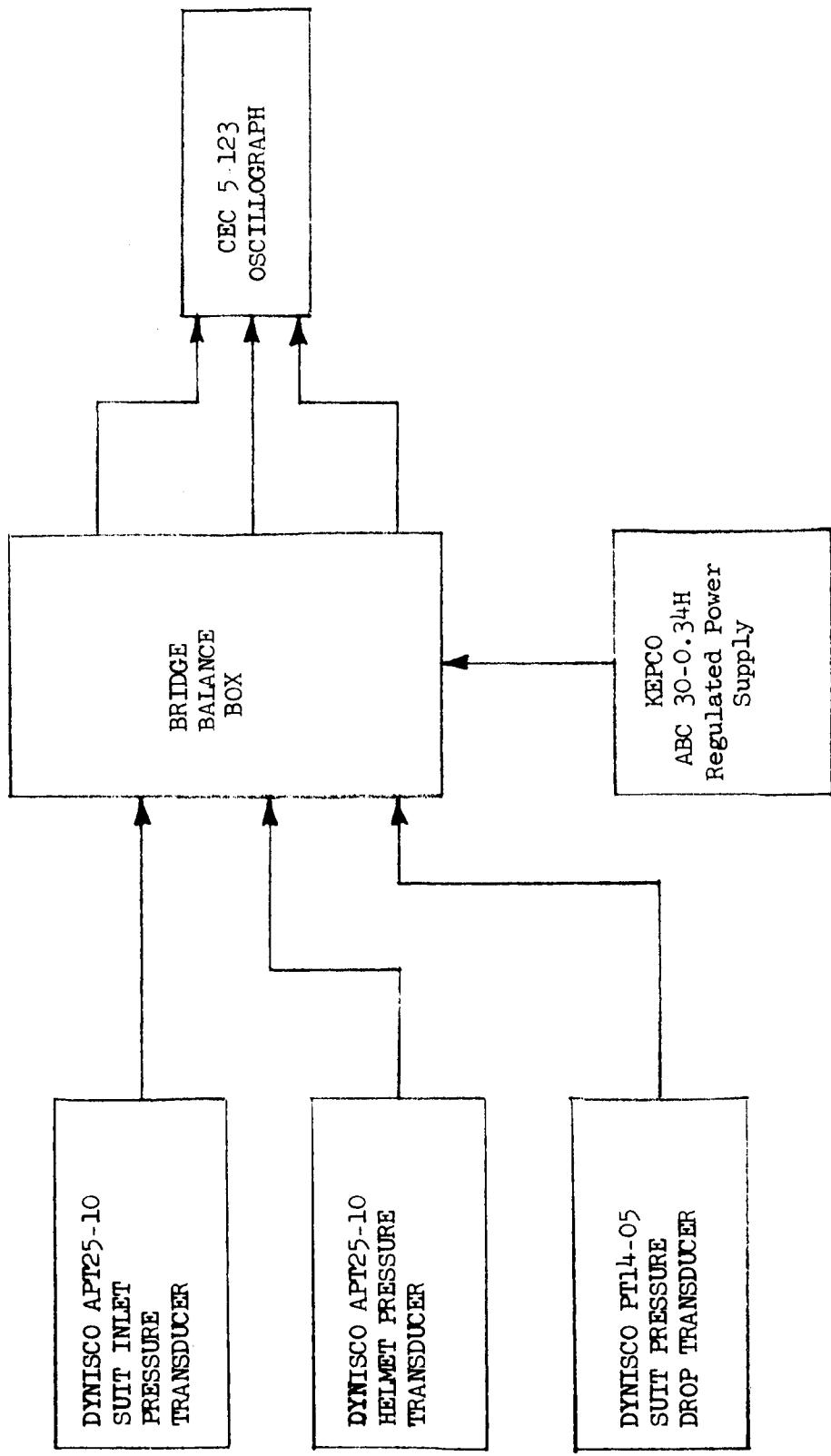


FIGURE 20
BLOCK DIAGRAM OF SUIT PRESSURE INSTRUMENTATION

These gauges were positioned to indicate the general area of leakage about the suit rather than indicate an exact leakage value.

Suit Gas Flow - The suit flow was continuously monitored and controlled by the suit flow system (Figure 14). The measurement of the flow of conditioned nitrogen to the suit was accomplished by using two flowmeters in series. A Fischer-Porter 36" laboratory type rotameter was utilized as the basis of flow control. In addition a National Instrument Laboratory Vol-O-Flow Model 10-1-15 flowmeter with a digital voltmeter readout was utilized to measure suit flow rate in actual cubic feet per minute based on the suit inlet pressure and temperature.

Relative Humidity and Visor Frosting - Relative humidity and visor frosting indications were included in this experiment to determine both the extent and possible effect of visor frosting during the various orbit conditions. A relative humidity sensor (Johnson Service Company Model WQ 9140 A) was installed in the water vapor inlet line to detect the relative humidity of the water vapor injected into the helmet. Water vapor (steam) was produced in a small container outside the SES and fed through copper tubing to finally impinge on the helmet visor. The relative humidity detector measured the relative humidity of the water vapor present while a light-photocell and mirror arrangement was used to detect any change in the reflection of light from the visor. The presence of such a change was an indication of visor frosting.

Energy Input to Visor - The measurement of energy passing into or out of the helmet visor is most essential to the thermal evaluation of the space suit assembly. To assist with this evaluation, an Eppley thermopile was mounted in the head of thermal dummy facing the visor. Cooling water for the thermopile was supplied by circulating water lines from outside of the chamber.

3.4.2 FACILITY INSTRUMENTATION

The SES instrumentation acquisition and recording system is designed to control system operation, collect data pertinent to the test, and supply recorded data suitable for reduction and analysis.

The recording devices utilized for acquisition of data during the test included:

1. Oscillograph: 50 channel direct writing CEC Model 5-123.
2. Recorders: Brown multipoint, 24 channel.
3. Digital Voltmeter: Cubic 300 channel with automatic print out.

Instrumentation feed-throughs in the chamber walls accomodate the following numbers and types of thermocouples.

1. 198 copper-constantan.
2. 108 iron-constantan.
3. 72 chromel-alumel.

Feed-throughs are also provided for cooling water, gas flow and power into the chamber. Vacuum measurements are continuously monitored and for such measurements the following instruments are available.

1. CVC GMA-140 Magnevac. (Range 760 mm to 10^{-3} mm Hg).
2. CVC GIC-100 Ionization gauge. (Range 10^{-3} to 10^{-10} mm Hg).
3. CVC PHG-9 Phillips gauge. (Range 0.5 to 10^{-3} mm Hg).
4. CVC GM 110 McLeod gauge. (For vacuum calibration).

A CEC Model 24-120 mass spectrometer is used for vacuum leak detection.

3.4.3 DATA RECORDING

The data collected during this test included:

- a. Manual hand written data.
- b. Digital voltmeter automatic print-out data.
- c. Brown recorder data.
- d. Oscillograph data.
- e. Pressure recorder data.
- f. Log book data.

Correlation on these various items included test point designations and time and date. The raw data has been reduced and assembled in Appendix A of this report.

3.4.4 DATA ACCURACY

The following is a summary of the accuracy of the data measurements made during this test.

- Temperatures (inside suit): $\pm 1.7^{\circ}\text{F}$.
- Temperatures (outside of suit): $\pm 3.1^{\circ}\text{F}$. RMS recording error plus thermocouple installation error.
- Suit ventilation gas temperatures: $\pm 3^{\circ}\text{F}$.
- Suit Pressures: ± 0.15 psi.
- Suit ventilation gas flow rate: $\pm 3\%$ of indication.
- Suit leakage rate: $\pm 2.1\%$.
- Local SES pressures (ionization gauges): $\pm 15\%$ of indication (estimated).
- Relative humidity in helmet area: $\pm 10\%$.
- Visor frosting indicator: qualitative measurement.
- Energy in visor: instrument accuracy estimated at $\pm 1.5\%$.

A derivation of the accuracies presented above and a discussion of thermocouple attachment errors are presented in Appendix B of this report.

3.5 DESCRIPTION OF TESTS

Experiment I-b was conducted in three parts (three days of tests) on November 5, 9 and 12, 1964. The test was conducted according to the test plan (Reference 3) and was completed approximately as planned. During each of the three days of tests, the suit configuration was changed in order to evaluate the effects of:

- (a) Clear versus tinted helmet visor.
- (b) Compression of parachute harness.
- (c) Exposed and uninsulated helmet versus a completely covered helmet.
- (d) Insulated boots.
- (e) Insulated versus uninsulated suit gloves.

(f) Proximity of and contact with a spacecraft surface.

(g) Heated versus unheated dummy surfaces.

The test points conducted included a variety of suit/environmental conditions with the three test configurations including minimum temperature cold soaks, maximum combined orbital heat fluxes and a simulated moving orbital condition.

Table III summarizes the tests performed and a description of the specimen during each of the three test days. Figures 3, 21, 22 and 1 show the specimen in the test position for the first, second and third days of test, respectively. Figure 23 relates position and time of the suit and flux sources during the simulated orbit tests performed on November 12, 1964, (test points 5 and 6).

3.5.1 TEST PROCEDURE

Reference 3 (Test Plan for Experiment I-b) outlined the test procedure that was followed throughout the testing. Table III presents the sequence of test points that were performed.

3.6 VARIANCES

3.6.1 SOLAR SOURCE

The solar simulation provided by the SES lamps differs from the true solar in three respects: (1) spectral energy distribution, (2) energy flux distribution and (3) collimation. The spectral distribution of these lamps is typical of Xenon or Mercury-Xenon lamps in that a large percentage of the energy is at shorter wavelengths than solar energy. The spectral distribution of the solar lamps as installed in the SES has been measured by Eppley Laboratories. The results of these measurements are presented in Table I and in Reference 1.

The effects of a spectral mismatch between the SES solar source and the sun is a function of the spectral characteristics of the surfaces being irradiated. For example, if the reflectance of the surface is relatively constant over the range of about 0.26 to 1.5 microns, the absorptance of the surface to SES solar radiation will be the same as for the true solar. However, if the reflectance of the surface changes significantly in this band (especially near the center of the solar spectrum), the SES absorptance can be significantly different from true solar absorptance. This latter case applies to the HT-1 nylon outer cover of the Gemini extravehicular suit. Figure 24 shows reflectance versus wavelength for HT-1 nylon. The absorptance of the nylon to the SES or solar spectrum was determined by first computing the reflectance and then solving for the absorptance from the equation

$$\alpha = 1 - \rho$$

TABLE II
SUMMARY OF TEST I_b TEST

DATE	SUIT CONFIGURATION	TEST POINT	SOLAR SOURCE	SUIT ORIENTATION	EARTH AND ALBEDO SIMULATOR
1st Day (11-5-64)	<ul style="list-style-type: none"> • Suit hung by parachute harness and tie-down cable • Suit glove on right hand • Insulated hood not on helmet • Clear helmet visor <p>(Ref. Figure 3)</p>	1	Off		Unheated
		2	Off	Back to Earth Simulator	Heated; facing solar source
		3	On	Facing solar lamps	Heating; facing solar source
		4	On	Right side to sun, left side to earth simu.	Heated; facing sun
		5	Off		Unheated
2nd Day (11-9-64)	<ul style="list-style-type: none"> • Suit hung by parachute harness and tie-down cable • Helmet not covered by insulated hood • Right hand suit glove exposed • Tinted visors on helmet • Left leg fixed in 90° bend position <p>(Ref. Figures 21 & 22)</p>	1	Off		Unheated
		2	Off		Unheated
		3	On	Facing solar source	Heated; facing solar source
		4	On	Back to sun	Heated; facing solar source
		5	Off	Front to earth simulator	Heated; facing suit
3rd Day (11-12-64)	<ul style="list-style-type: none"> • Suit suspended from helmet • Clear helmet visor installed • Helmet not covered by insulated hood • Insulated mitten on right hand • Left foot insulated <p>(Ref. Figure 1)</p> <p>#Dummy hands and feet were not heated at any time during the tests.</p>	1	On	See Description	Heated; facing solar source
		2	On	Facing solar source	Heated; facing solar source
		3	On	Facing solar source	Heated; facing solar source
		4	On	Facing solar source	Heated; facing solar source
		5		Simulated moving orbital condition w/ (solar on 60 min., off 30 min.) (See Fig. 1)	
		6		Simulated orbital condition with rotation 60 min., off 30 min.,) (See Fig. 2)	

I

CONDITIONS

DO	DESCRIPTION	DUMMY # SKIN HEATERS	DURATION
	Steady state, suit cold soak test (no incident radiation)	On	2 hours (1200-1400)
	Steady state, simulated orbit in earth's shadow, suit back to earth	On	2 hours (1720-1920)
ig	Steady state, simulated orbit over earth subsolar point, suit facing sun	On	3 hours (1920-2220)
	Steady state, simulated orbit over earth subsolar point, suit right side to sun	On	0.50 hours (0015-0045)
	Steady state, cold soak test. (No incident radiation)	On	4 hours (0100-0500)
	Steady state cold soak test	On	3.5 hours (0630-1000)
	Steady state cold soak test	Off	2.25 hours (1000-1215)
	Steady state, simulated orbit over earth subsolar point, suit facing sun	Off	3 hours (1545-1845)
	Steady state, simulated orbit over earth subsolar point, suit back to sun	Off	1.25 hours (1845-2000)
	Steady state, simulated orbit in earth's shadow, front of suit to earth	Off	3.1 hours (2000-2310)
	Suit rotated continuously until average surface temperature of $75+5^{\circ}\text{F}$ achieved (1 hour)	Off	1.4 hours (0800-0925)
	Steady state, simulated maximum heat flux condition (over earth subsolar point), suit facing sun	Off	1.4 hours (0935-1100)
	Steady state, simulated close proximity of hot spacecraft surface (not touching)	Off	2.5 hours (1100-1330)
	Steady state, simulated hot spacecraft surface pressed against right side of suit, maximum incident space fluxes	Off	2 hours (1330-1530)
th	rotation of suit and earth simulator Figure 23)	Off	1.5 hours (1545-1715)
ition	of suit and earth simulator (solar • 23)	Off	1.5 hours (1715-1845)



FIGURE 21 GEMINI SPACE SUIT ASSEMBLY INSTALLED IN LTV SPACE ENVIRONMENT SIMULATOR (TEST DAY #2)

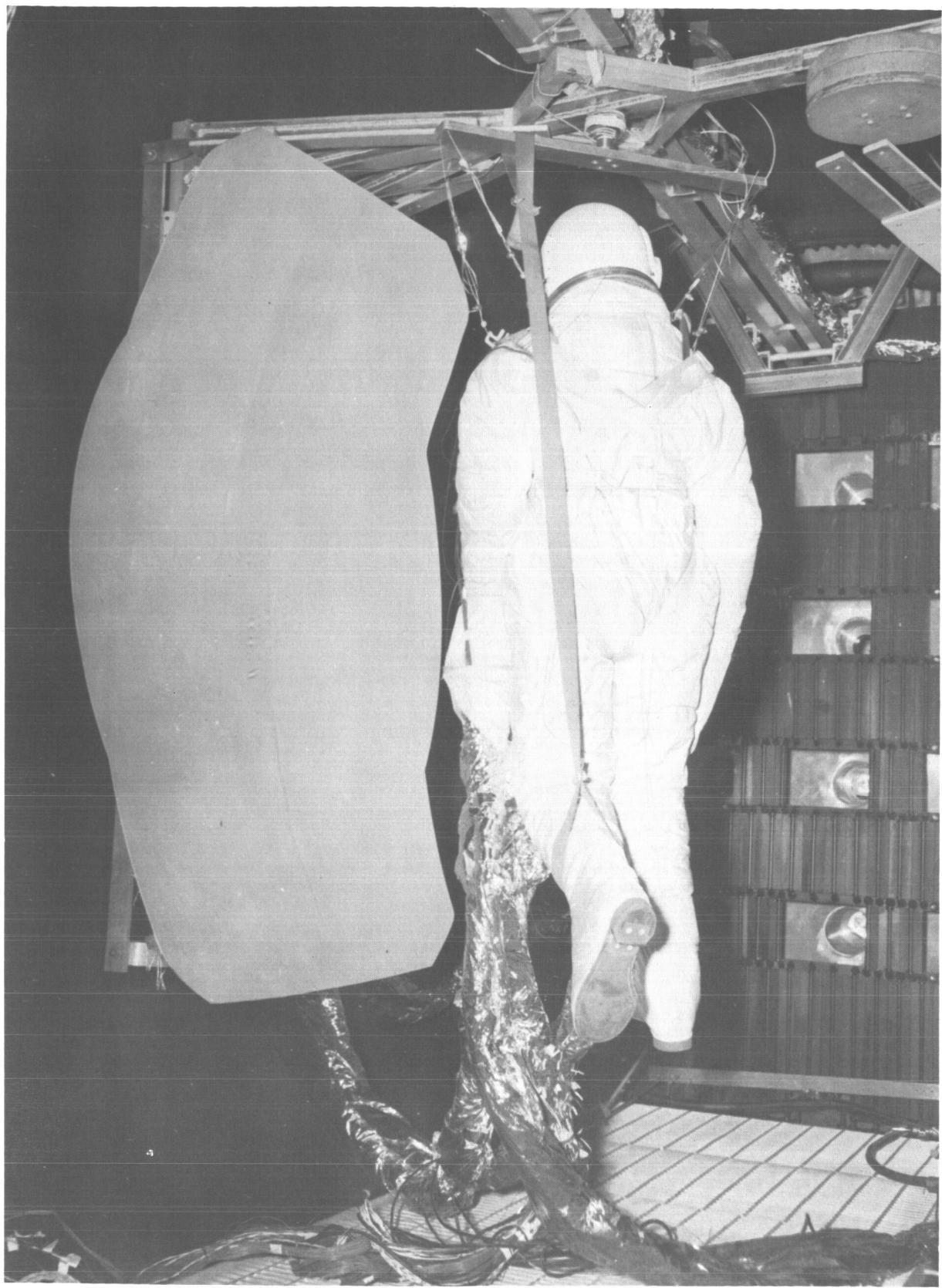


FIGURE 22 GEMINI SPACE SUIT ASSEMBLY INSTALLED IN LTV SPACE ENVIRONMENT SIMULATOR
SHOWING POSITION OF LEFT LEG (TEST DAY #2)

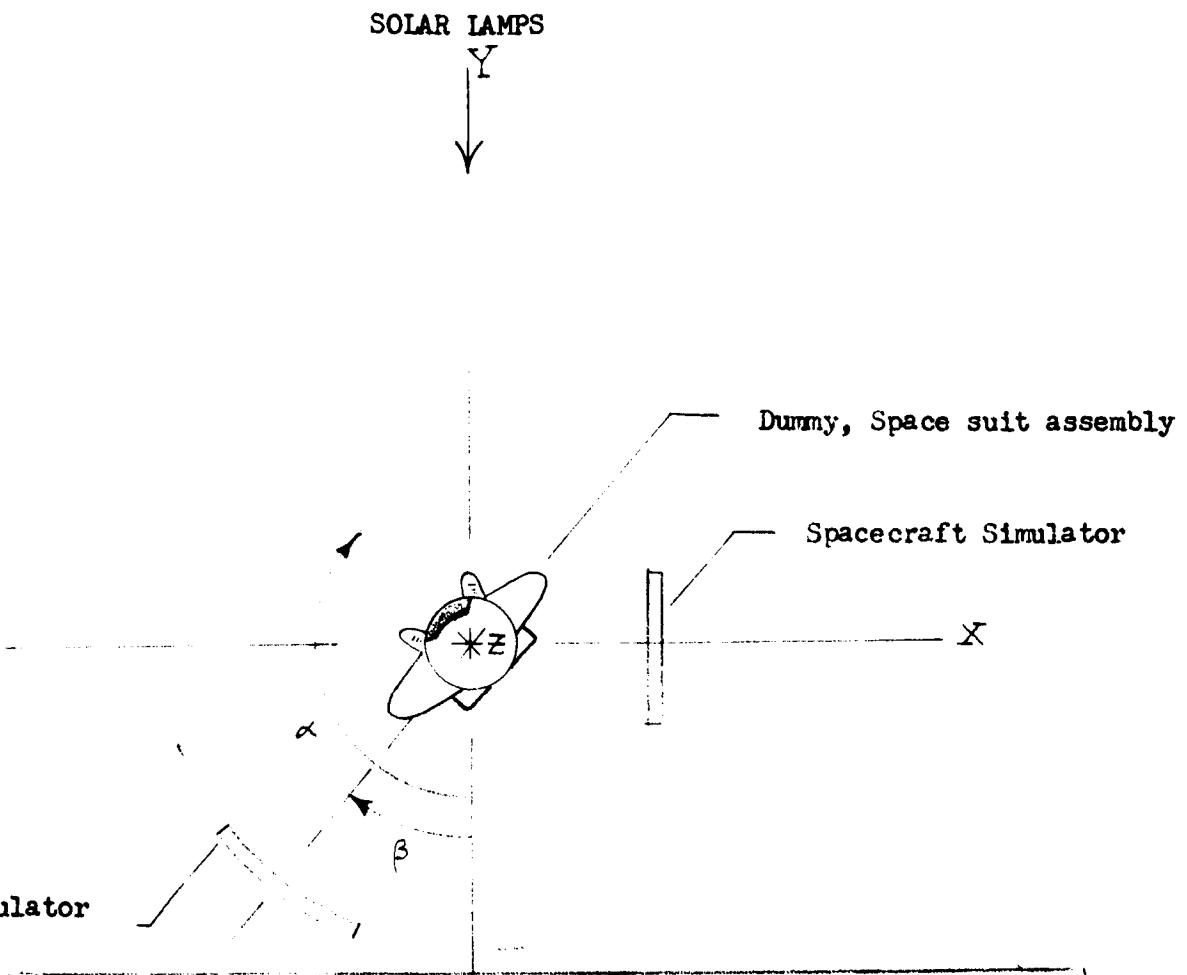


FIGURE 23

ORBITAL POSITIONS FOR SPACESUIT ASSEMBLY

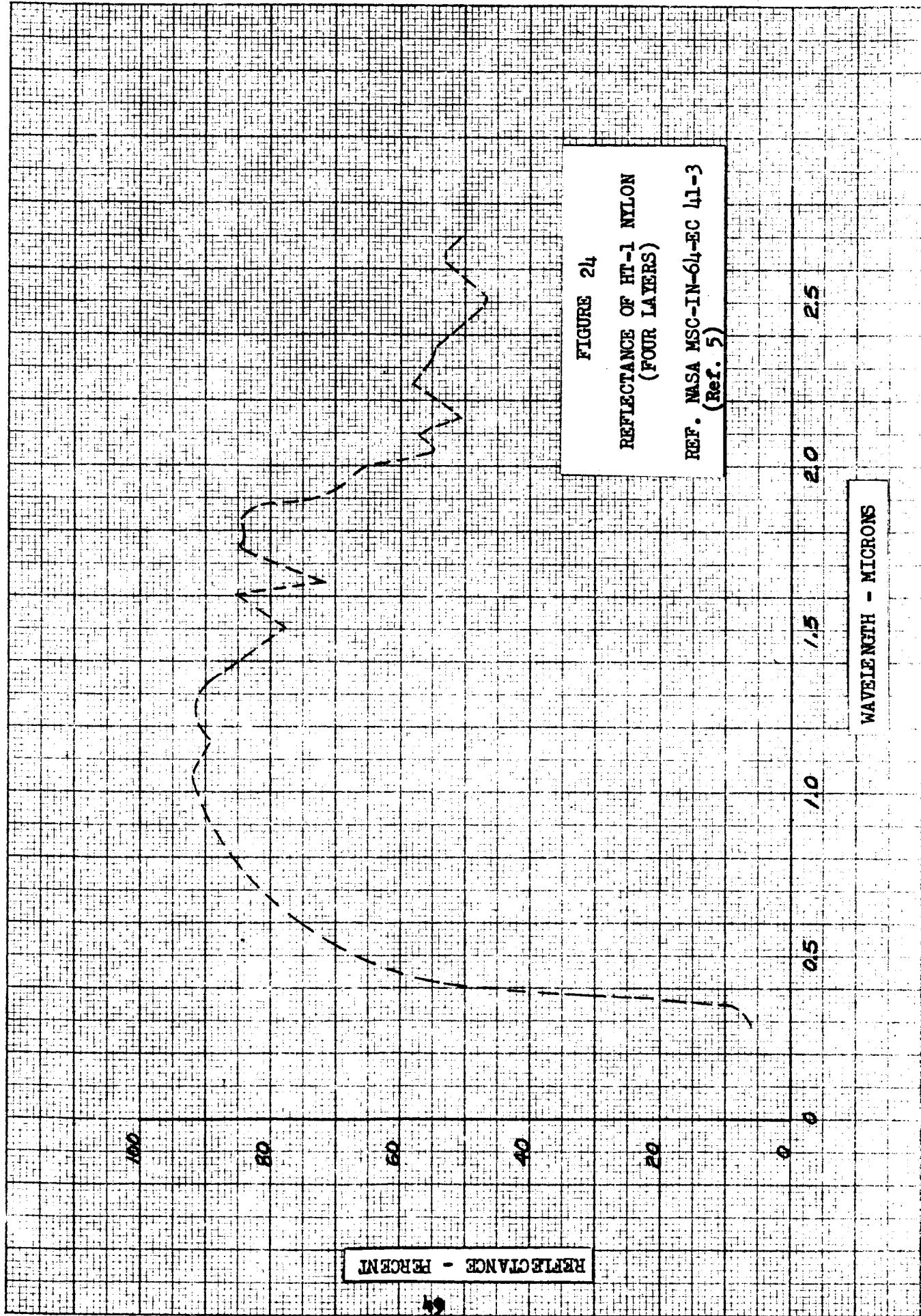
AND EARTH SIMULATOR

a. Solar Portion - 60 minutes

Time Minutes	E.S. Position, β Degrees	SSA Position, α Degrees
0-7½	0	180
7½-15	0	0
15-22½	30	0
22½-30	30	180
30-37½	60	180
37½-45	60	0
45-52½	90	0
52½-60	90	180

b. Dark Portion - 30 minutes

0-7½	90	180
7½-15	90	0
15-22½	45	0
22½-30	45	180



where the transmittance is assumed to be zero. The reflectance was calculated by a computer program which evaluates the following expression:

$$\rho = \frac{\int \rho_{\lambda} E_{\lambda} d\lambda}{\int E_{\lambda} d\lambda}$$

Where

ρ = reflectance at wavelength λ

E_{λ} = monochromatic emissive power

The limits of integration are chosen as appropriate to the spectrum being considered, i.e. SES or Solar. The computer program inputs include material reflectance data from Figure 23, the Johnson data for the solar spectrum (Reference 4) and the data shown in Table I for the SES lamp spectrum. The absorptances of the nylon outer cover to the SES and solar spectrums were computed to be as follows:

$$\alpha_{SES} = 0.273$$

$$\alpha_{Solar} = 0.497$$

In order for the suit to absorb approximately the same amount of energy, whether exposed to the SES lamps or true sunlight, the following relationship must be maintained:

$$\alpha_{SES} S_{SES} = \alpha_{Solar} S_{Solar}$$

Where

S_{SES} = flux at test plane of SES

S_{Solar} = solar constant (443 BTU/hr ft²)

The required flux at the test plane is than calculated to be

$$S_{SES} = S_{Solar} \frac{\alpha_{Solar}}{\alpha_{SES}}$$

$$S_{SES} = 443 \frac{(0.273)}{(0.497)} = 443 (0.55)$$

$$S_{SES} = 243 \text{ BTU/hr ft}^2$$

However, for stable operation, the SES lamps cannot be operated below a flux of 288 BTU/hr ft² (or 65% of the solar constant). This lamp power setting was employed during the tests resulting in a higher heat absorbed during the experiment than would actually occur in space.

Flux distribution at the test plane was measured before and after the test using the thermopile described in paragraph 3.3.1. The results of these measurements are shown in Figure 6.

Collimation of the SES lamps varies from 0 to 13° whereas rays from the sun are essentially parallel. However, the cones formed by rays from the different lamps intersect in front of the test plane. This helps to smooth out the flux distribution. Because of this overlapping, collimation variances are not considered to be significant.

3.6.2 THERMAL AND ALBEDO SIMULATION

Accurate simulation of earth thermal and albedo radiation depends on the configuration or view factor between the earth simulator and the test plane and the radiant heat transfer properties of the earth simulator. The variances in SES simulation of earth thermal and albedo radiation are discussed in this section.

The view factor from the test plane to the earth simulator has been calculated to be approximately 0.81 as shown by the analyses included in Appendix C. Reflectance measurements for the earth simulator paint, as measured by a Gier-Dunkle Integrating Sphere Reflectometer are shown in Figure 25. The reflectance of the paint for the SES lamp spectrum was then computed to be approximately 0.32 using the computer program described in paragraph 3.6.1.

The heat flux at the test plane due to the earth simulator albedo (reflected energy) can be shown to be

$$q'_a = F \rho S_{SES}$$

$$q'_a = .81 (.32) (288)$$

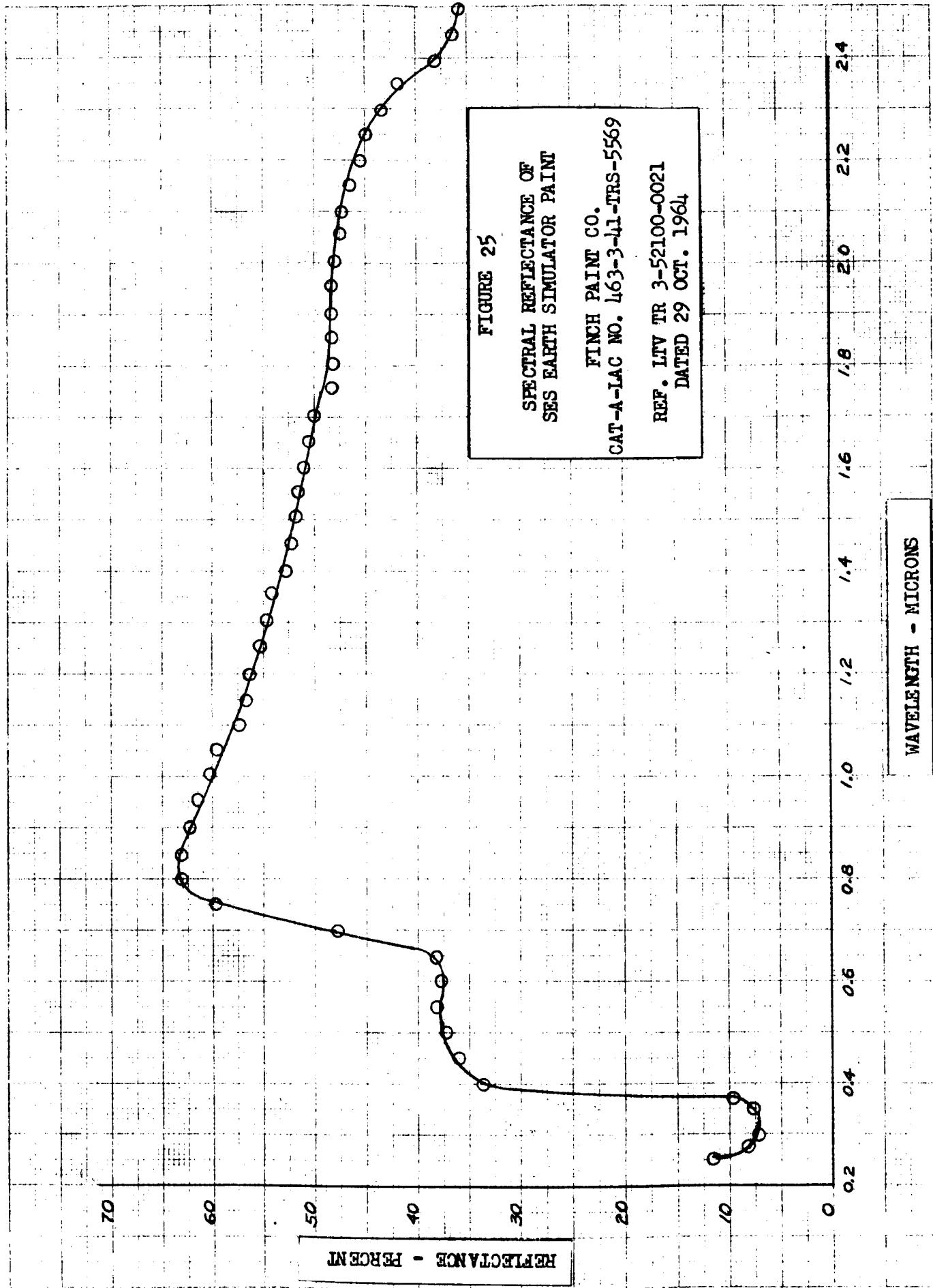
$$q'_a = 75 \frac{\text{BTU}}{\text{hr. ft}^2}$$

Where:

F = View factor from test plane to earth simulator.

ρ = Reflectance of earth simulator for SES lamp spectrum.

S_{SES} = Flux at test plane from SES lamps, BTU/hr. ft².



The distribution of reflected energy from the earth simulator at the test plane was measured using the thermopile described in 3.3.1. Figure 26 shows the distribution in flux for a horizontal traverse at different locations on the earth simulator vertical centerline. These data indicate the maximum flux measured was approximately 55 BTU/Hr. ft² with the earth simulator parallel to the test plane. The variation in flux as the earth simulator is rotated about the test plane is shown in Figure 27 for a traverse along the test plane vertical centerline. These flux measurements are believed to be somewhat lower than the actual flux due to the Fresnel reflection of the quartz lens in the thermopile.

The maximum heat flux incident on a flat plate in a 200 nautical mile earth orbit due to reflected solar energy from the earth is:

$$q_a = F a S$$

$$q_a = (0.9) (0.35) (443)$$

$$q_a = 139 \frac{\text{BTU}}{\text{hr. ft}^2}$$

Where:

a = earth albedo

S = Solar constant, $\frac{\text{BTU}}{\text{hr. ft.}^2}$

F = Flat plate view factor

Reflected solar energy from the earth is generally assumed, for calculation purposes, to be in the same spectrum as the sun. If the same assumption is made for the earth simulator; that is, reflected energy from the earth simulator is in the same spectrum as the solar lamps, then the required earth simulator reflected energy (at the test plane), is:

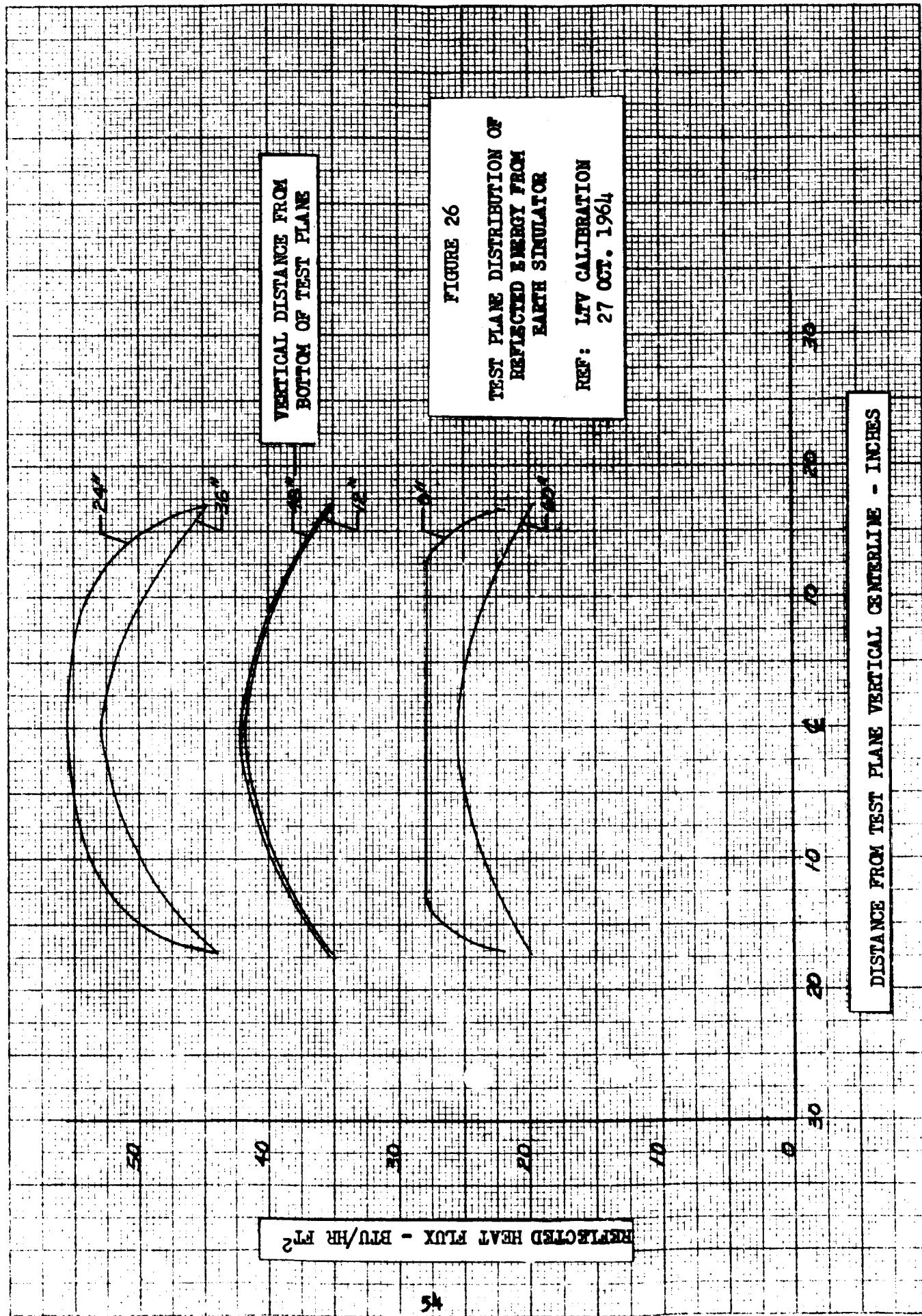
$$q'a = 139 \frac{\propto_{\text{solar}}}{\propto_{\text{SES}}}$$

$$q'a = 139 \frac{.273}{.497}$$

$$q'a = 139 (0.55)$$

$$q'a = 76 \frac{\text{BTU}}{\text{hr. ft}^2}$$

for accurate simulation of true space conditions. Therefore, the required flux at the test plane is calculated to be 76 BTU/(hr. ft.²) and the actual flux is calculated to be 75 BTU/(hr. ft.²) based on physical dimensions and measurements of SES lamp heat flux and earth simulator reflectance.



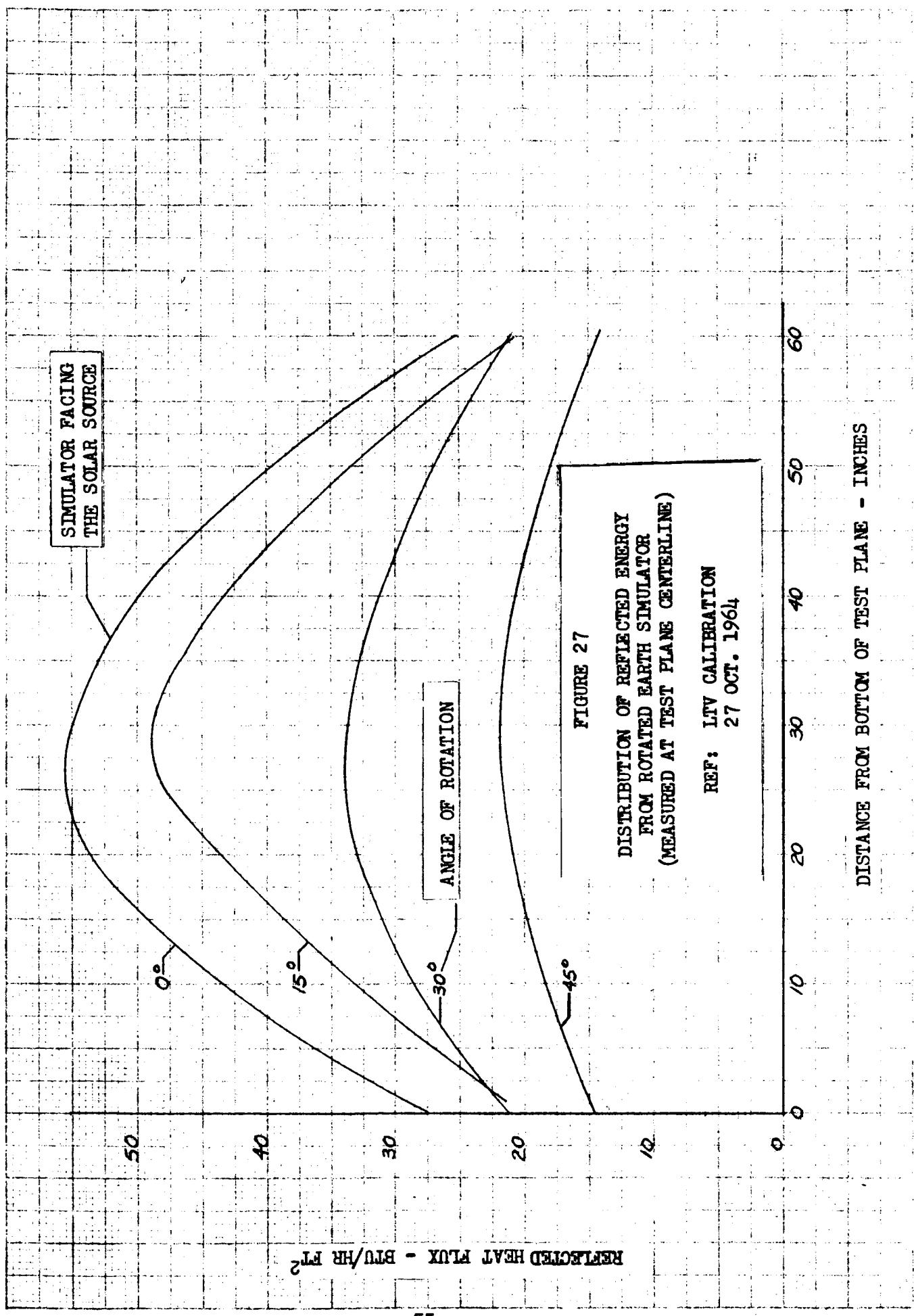


FIGURE 27

DISTRIBUTION OF REFLECTED ENERGY
FROM ROTATED EARTH SIMULATOR
(MEASURED AT TEST PLANE CENTERLINE)

REF: LTV CALIBRATION
27 OCT. 1964

Simulation of the earth's thermal radiation is accomplished by controlling the earth simulator temperature. The heat flux at the test plane due to thermal radiation from the earth simulator at a temperature of 70°F can be calculated as follows:

$$q'_e = F \epsilon \sigma T^4$$

$$q_e = (0.81) (0.60) (0.1713 \times 10^{-8}) (530)^4$$

$$q_e = 67 \frac{\text{BTU}}{\text{hr. ft.}^2}$$

Where:

F = View factor from test plane to earth simulator.

ϵ = Emittance of earth simulator

σ = Stefan-Boltzmann constant

T = Temperature °R

In a 200 nautical mile earth orbit the maximum heat flux incident on a flat plate due to the earth's thermal radiation is:

$$q_e = F \sigma T^4$$

$$q_e = (0.893) (0.1713 \times 10^{-8}) (454)^4$$

$$q_e = 64 \frac{\text{BTU}}{\text{hr. ft.}^2}$$

(This assumes the earth to emit as a black body at -6°F, Reference 2).

Therefore, the thermal radiation from the earth simulator is calculated to be 67 BTU/(hr. ft.²) at a temperature of 70°F and the thermal radiation from the earth incident on a flat plate in actual 200 nautical mile earth orbit is calculated to be 64 BTU/(hr. ft.²).

3.6.3 CHAMBER AND WALLS

The SES chamber and wall geometry as compared with actual earth orbit introduces relatively minor variances in the space simulation test program. The solar flux reflected by the rear wall of the SES to the test specimen will be approximately 8.0 BTU/hr. ft.². The fraction of this energy absorbed by the test specimen will be the product of the view factor and the absorptance of the specimen surface. The value of energy transported will be in the order of 0.18 BTU/hr. ft.² or less than 1% of the direct flux on the test specimen.

The chamber walls radiate some energy to the test specimen. The emitted radiation of the black walls at the liquid nitrogen temperature level is .36 BTU/ft.² hr or about 0.1% of the solar flux.

The openings in the liquid nitrogen cooled shroud for admitting the solar flux to the chamber interior present another item of variance when compared with actual earth orbital conductors. These twenty openings in the cold wall have a total area of 13 square feet and are located approximately 9 feet from the test plane. The view factor from these sources to the test specimen is approximately 0.024. The solar openings represent a source temperature of approximately 250°F during lamp operation and have an effective of about 0.8. The flux incident on the test specimen will be

$$Q/A = \sigma \epsilon F^4 = (.173 \times 10^{-8}) (0.8) (0.024) (710)^4 = 7.35 \frac{\text{BTU}}{\text{Hr. ft.}^2}$$

During periods of simulated darkness, these sources will be at room temperature and heat fluxes incident on the test specimen are less than 3 BTU/hr. ft². These fluxes do not result in a significant variance when compared to the test results.

3.6.4 PRESSURE

The primary potential variance attributable to the SES chamber pressure is the effect of pressure on the thermal protective characteristics of the space suit. The apparent thermal conductivity of superinsulations is minimized and becomes essentially independent of pressure below about 10⁻⁴ mm Hg, Figure 28. If the interlayer pressures of the suit exceed 10⁻⁴ mm Hg at any time, the thermal protective features of the suit become progressively ineffective. The interlayer pressures of the thermal protective layers while in space will be determined largely by the leakage rate of the suit through the pressure seals and joints. With chamber pressures remaining below 10⁻⁴ mm of Hg during the operational portions of this experiment, the variance due to chamber pressure is not believed to be significant. A plot of the chamber pressure during the second test day is shown in Figure 5.

FIGURE 28

EFFECT OF PRESSURE ON CONDUCTIVITY
OF TYPICAL SUPERINSULATIONS

NOTE: WARM SIDE TEMP. = 77°F
COLD SIDE TEMP. = -300°F

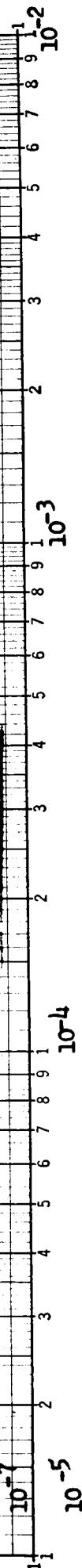
APPARENT THERMAL CONDUCTIVITY - WATTS/CM²·K

REFLECTIVE SHELLS
WITH FIBROUS SPACERS

NRC-2 SUPERINSULATION

REF: HNILICKA, M.P., "Engineering Aspects of Heat Transfer
in Multilayer Reflective Insulation and Performance of
NRC-2 Insulation." (Ref. 6)

PRESSURE - MM HG



4.0 RESULTS AND DISCUSSION

4.1 RESULTS

Tabulated data for all three test days are included in Appendix A. A brief description of each test day and test point is included with the data. Temperature data have been reduced at intervals ranging from every five minutes to every hour, depending on the length of the test point and the test objective. The test day number and test point number are noted on each page and the time of day is given above each data column. Immediately after the temperature data for each test day, thermal dummy heater power and suit flow system data are tabulated.

In Figures 29 through 37 selected temperatures have been plotted for each test point and test day. Significant events occurring during each test point, such as solar lamps on, are noted at the top of each figure.

4.2 DISCUSSION

4.2.1 SUIT TEMPERATURES AND PRESSURES

During this experiment, measured suit surface temperatures ranged from approximately -200°F to $+200^{\circ}\text{F}$. Table IV compares measured suit surface temperatures with calculated values for actual earth orbit. The higher measured temperature facing the sun resulted from the flux at the test plane being approximately 65% of one solar constant, (Figure 6), compared to the required 55% calculated from the ratio of solar and SES absorptances as outlined in Paragraph 3.6.1. During the simulated dark part of earth orbit (Test Point No. 2, Day No. 1) suit surface temperatures facing the earth simulator varied from -26°F to -40°F in locations other than the one (lower left back) given in Table IV. Therefore, the deviation from true space conditions is probably not as large as would appear (4°F compared to -20°) in the Table.

In general, reproducibility of suit surface temperatures from one test day to the next was good. For example, the suit surface temperature in the upper right chest area varied only 3°F (from 142 to 145°F) when facing the solar lamps on all three test days. Larger temperature variations were noted on the arms and legs. Temperatures in these locations were affected by peaks in the flux distribution at the test plane as shown in Figure 6, and by the location of the ventilation gas lines and thermocouple harnesses, Figure 1.

In Figs. 29 through 31 measured suit surface temperatures in the upper right chest and upper right back locations are plotted for each test point and test day. The variation in suit surface temperature in the lower left back area is shown in Figures 32 through 34. These figures show that the suit surface temperatures respond rapidly to a change in test conditions, such as solar lamps on, and reach steady state within approximately 30 minutes. When the lamps are turned off, suit surface temperatures drop rapidly at first but require two to three hours to reach essentially steady state conditions.

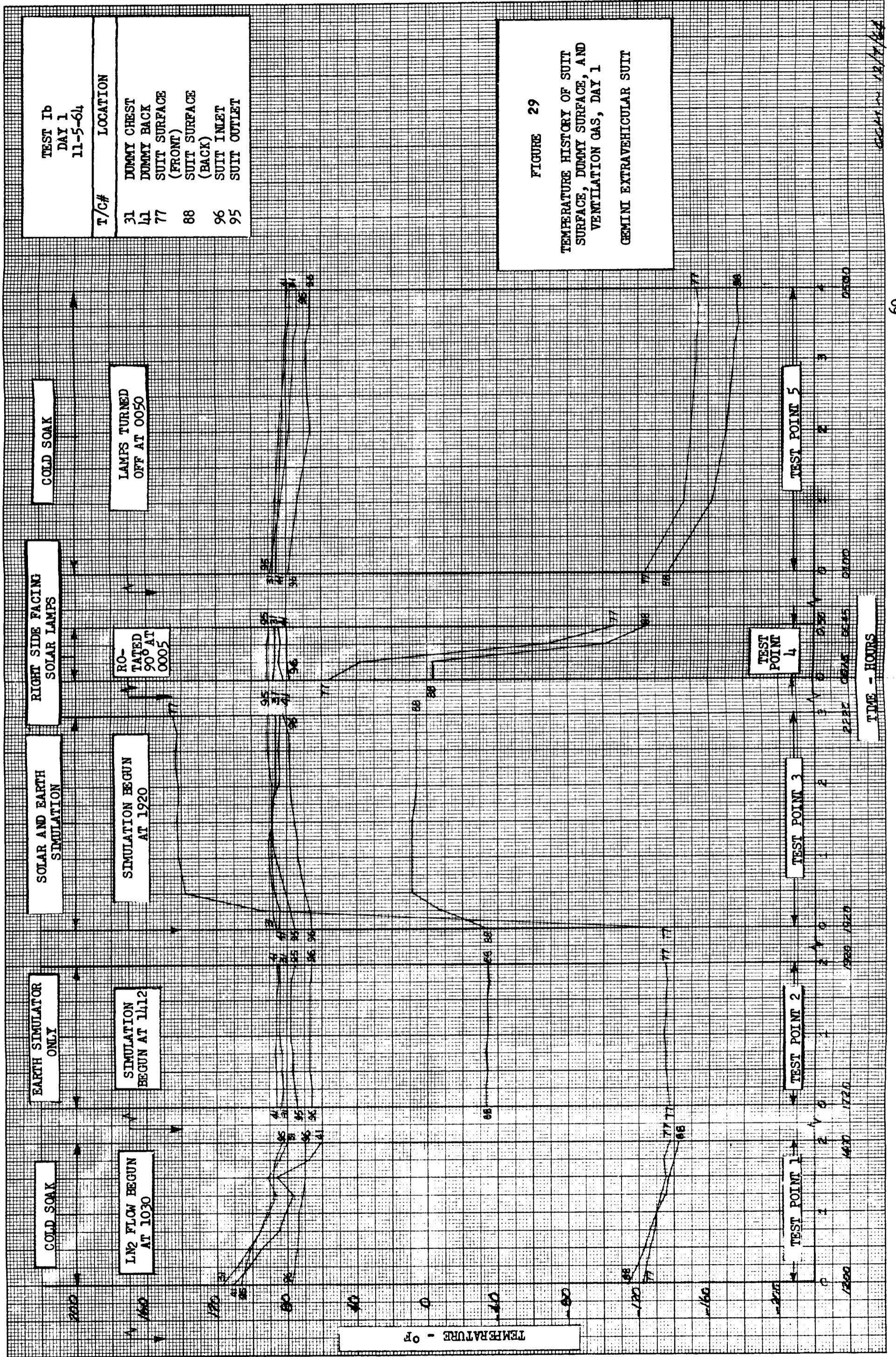


FIGURE 29

TEMPERATURE HISTORY OF SUIT SURFACE, DUMMY SURFACE, AND VENTILATION GAS, DAY 1

GEMINI EXTRAVEHICULAR SUIT

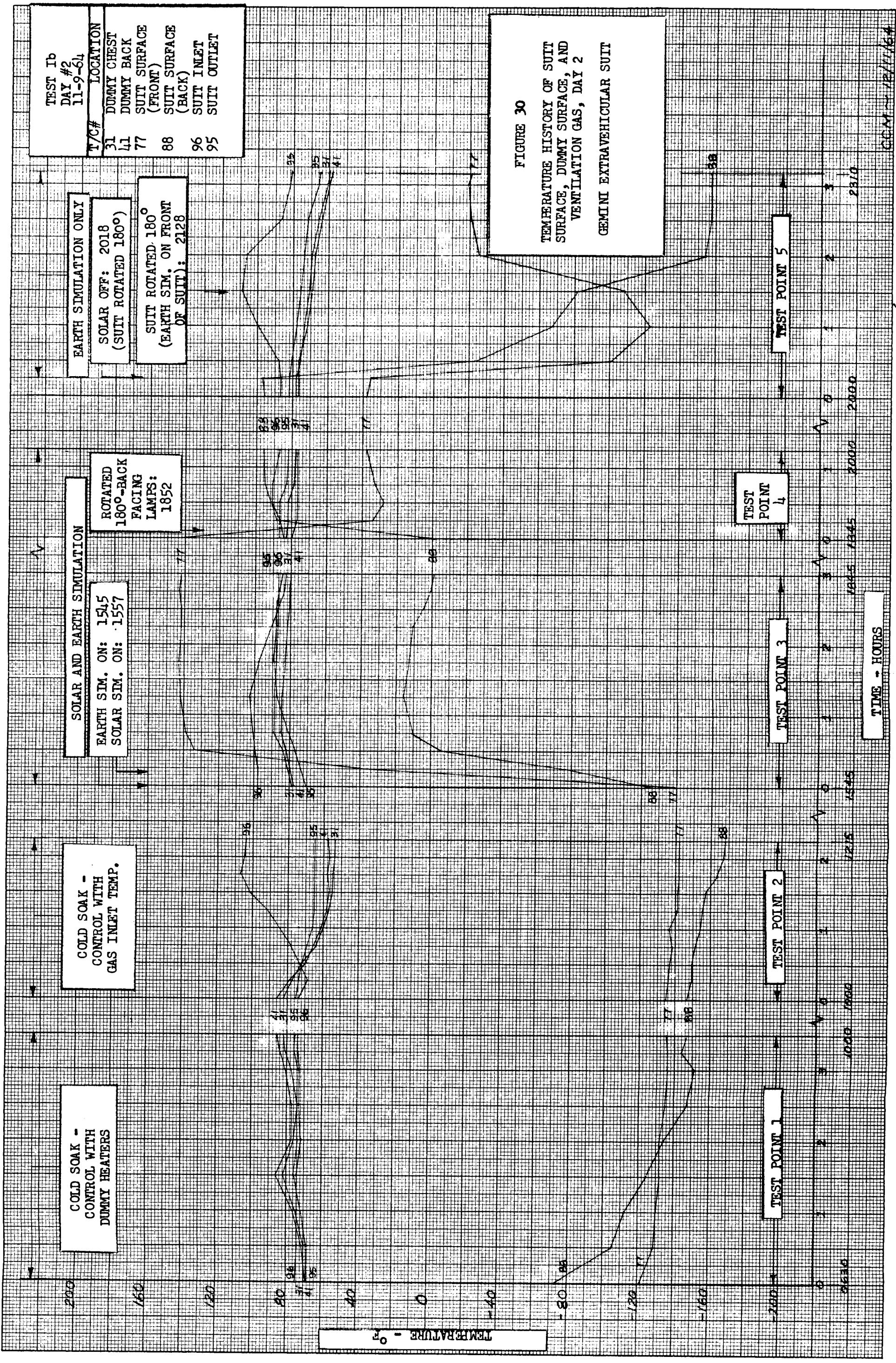
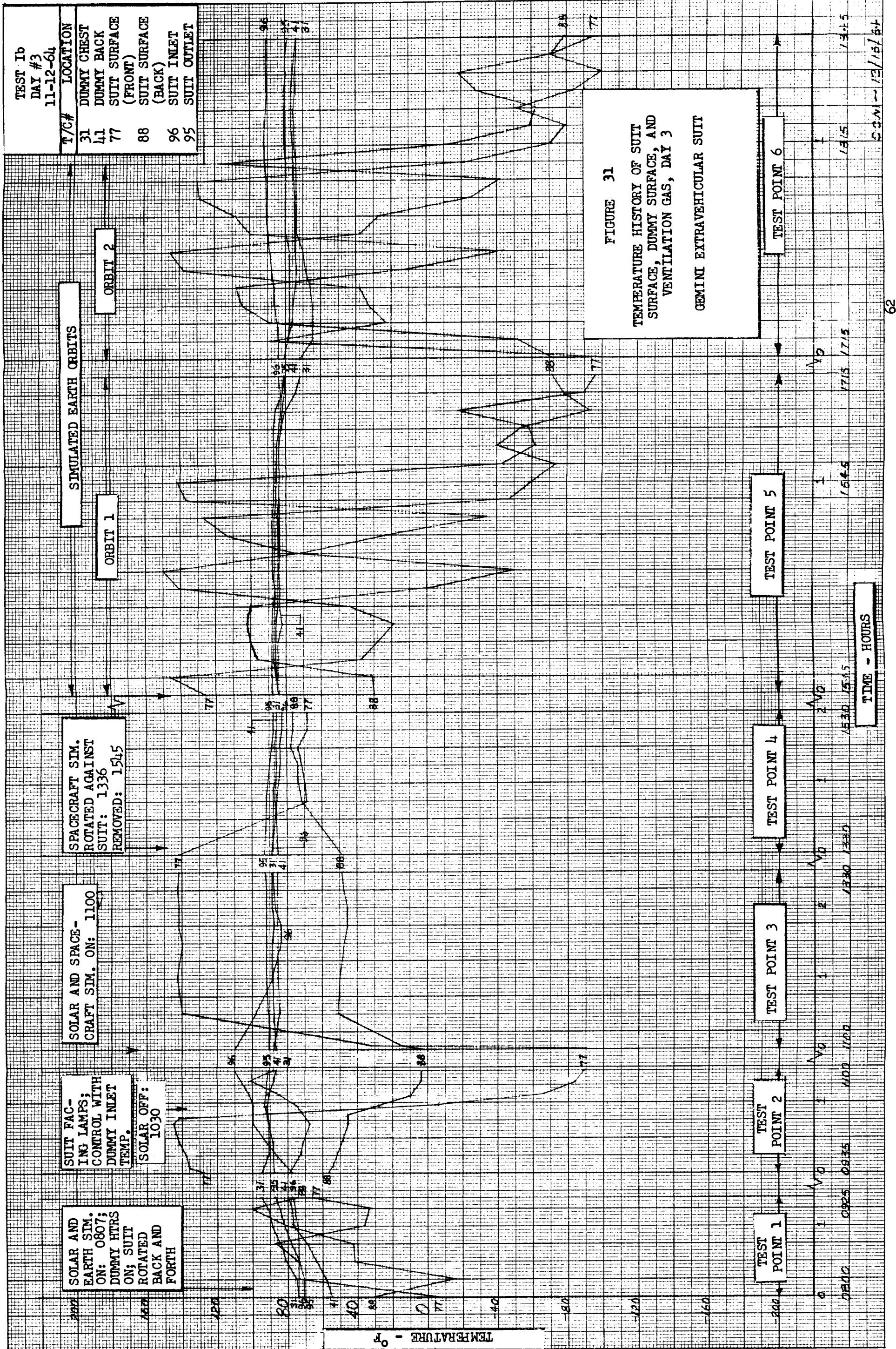


FIGURE 30
TEMPERATURE HISTORY OF SUIT
SURFACE, DUMMY SURFACE, AND
VENTILATION GAS, DAY 2
GEMINI EXTRAVEHICULAR SUIT



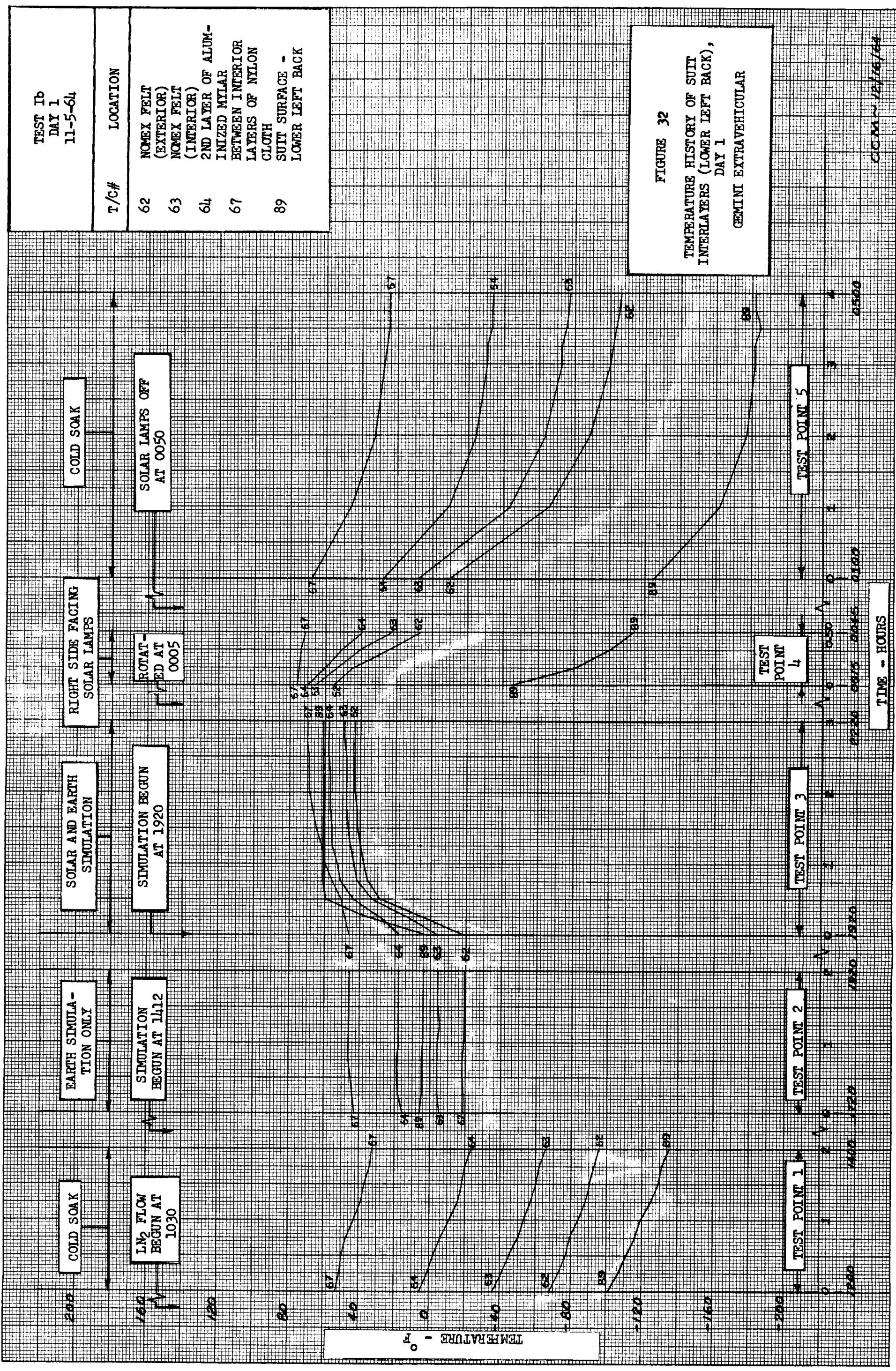


FIGURE 32
TEMPERATURE HISTORY OF SUIT
INTERLAYERS (LOWER LEFT BACK),
DAY 1
GEMINI EXTRAVEHICULAR

TEST 1b
DAY 2
11-9-64

T/C#	LOCATION
62	NOMEX FELT (EXTERIOR)
63	NOMEX FELT (INTERIOR)
64	2ND LAYER OF ALUMINIZED MYLAR
67	BETWEEN N INTERIOR LAYERS OF NYLON CLOTH
89	SUIT SURFACE - LOWER LEFT BACK

EARTH SIMULATION ONLY

SOLAR OFF: 2018 (SUIT ROTATED 180°)

ROTATED 180°-BACK
FACING LAMPS
1852

SOLAR AND EARTH SIMULATION

EARTH SIM. ON 1545

ROTATED 180°-BACK
FACING LAMPS
1852

COLD SOAK -
CONTROL WITH
GAS INLET TEMP.

COLD SOAK -
CONTROL WITH
DUMMY HEATERS

120

160

200

240

280

320

360

400

440

480

520

560

600

640

680

720

760

800

840

880

920

960

1000

1040

1080

1120

1160

1200

1240

1280

1320

1360

1400

1440

1480

1520

1560

1600

1640

1680

1720

1760

1800

1840

1880

1920

1960

2000

2040

2080

2120

2160

2200

2240

2280

2320

2360

2400

2440

2480

2520

2560

2600

2640

2680

2720

2760

2800

2840

2880

2920

2960

3000

3040

3080

3120

3160

3200

3240

3280

3320

3360

3400

3440

3480

3520

3560

3600

3640

3680

3720

3760

3800

3840

3880

3920

3960

4000

4040

4080

4120

4160

4200

4240

4280

4320

4360

4400

4440

4480

4520

4560

4600

4640

4680

4720

4760

4800

4840

4880

4920

4960

5000

5040

5080

5120

5160

5200

5240

5280

5320

5360

5400

5440

5480

5520

5560

5600

5640

5680

5720

5760

5800

5840

5880

5920

5960

6000

6040

6080

6120

6160

6200

6240

6280

6320

6360

6400

6440

6480

6520

6560

6600

6640

6680

6720

6760

6800

6840

6880

6920

6960

7000

7040

7080

7120

7160

7200

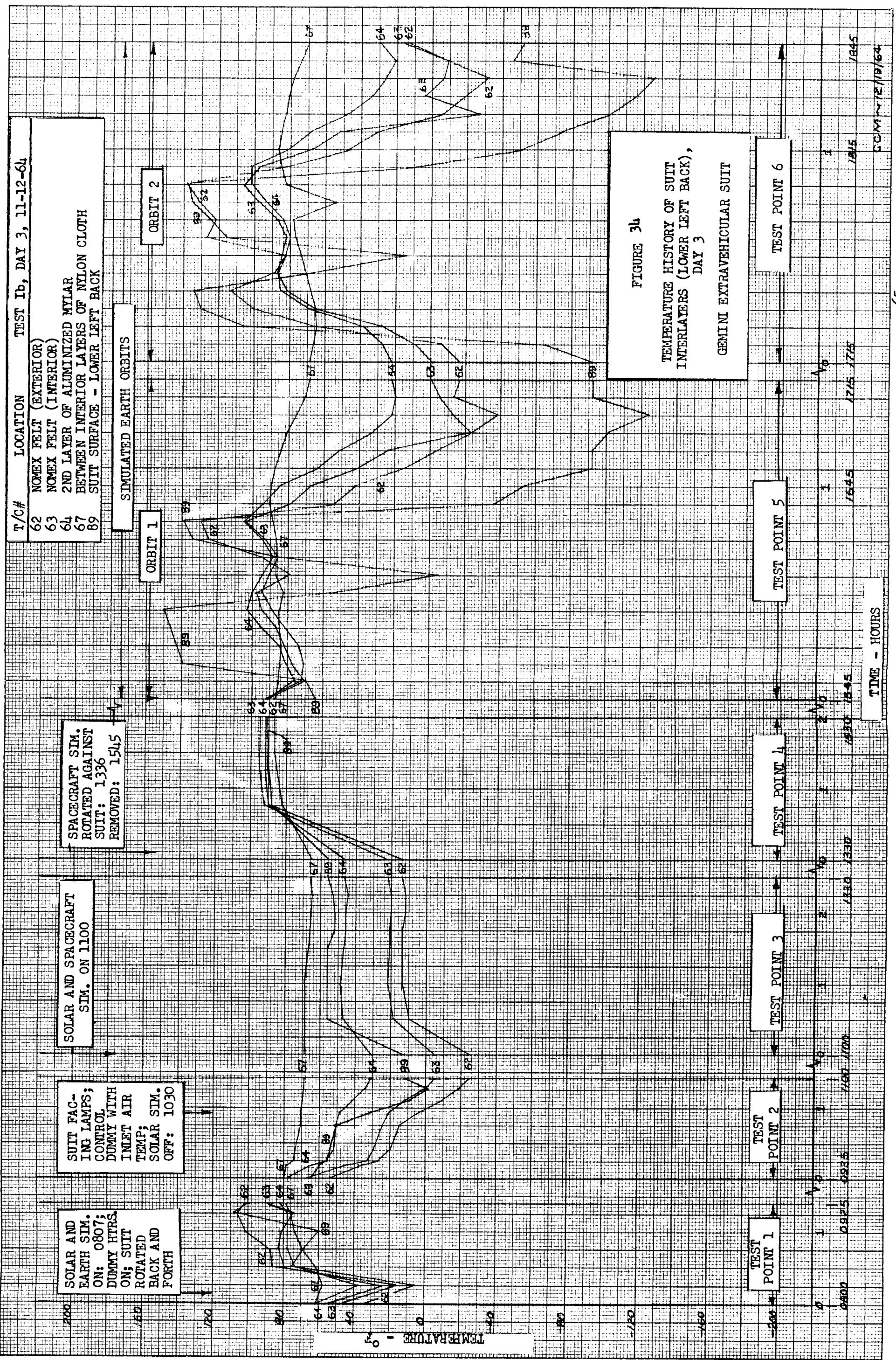
7240

7280

7320

7360

7400



TEST 1b
DAY 1
11-5-64

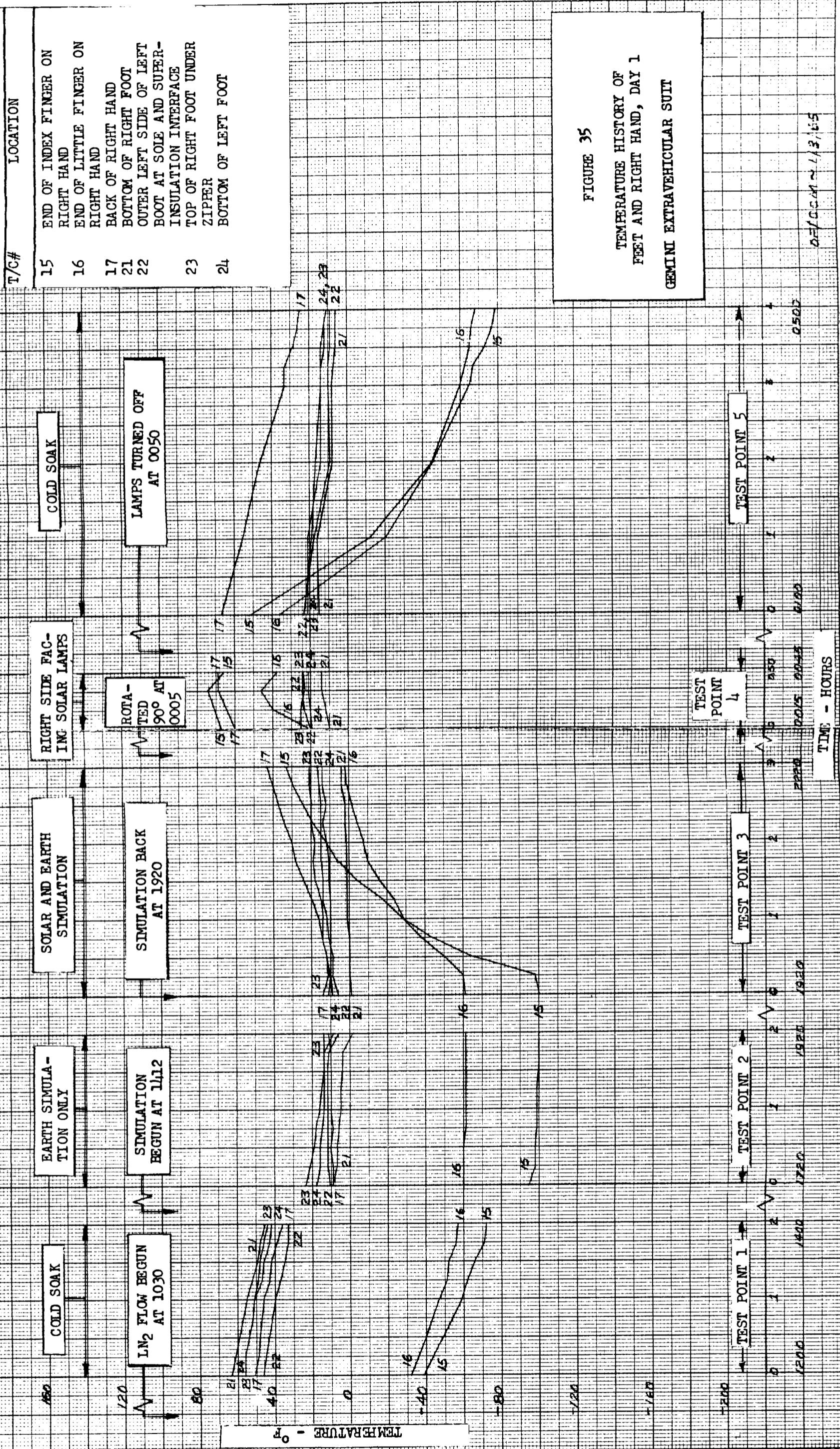


FIGURE 35

TEMPERATURE HISTORY OF
FEET AND RIGHT HAND, DAY 1

GEMINI EXTRAVEHICULAR SUIT

$\Delta T / \Delta t = 1/3.165$

TIME - HOURS

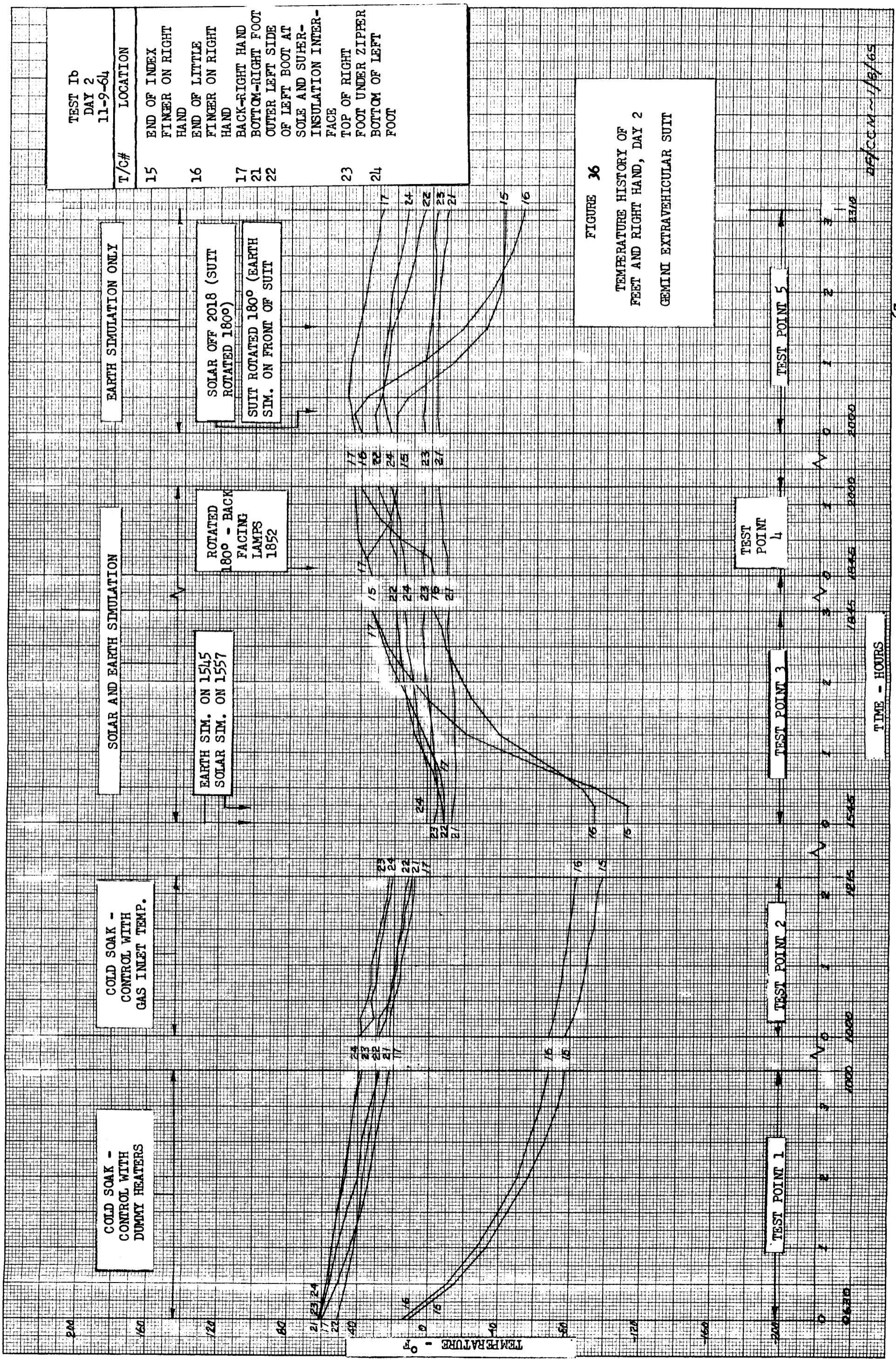


FIGURE 36

TEMPERATURE HISTORY OF FEET AND RIGHT HAND, DAY 2
GEMINI EXTRAVEHICULAR SUIT

DE/CCW ~ 1/9/65

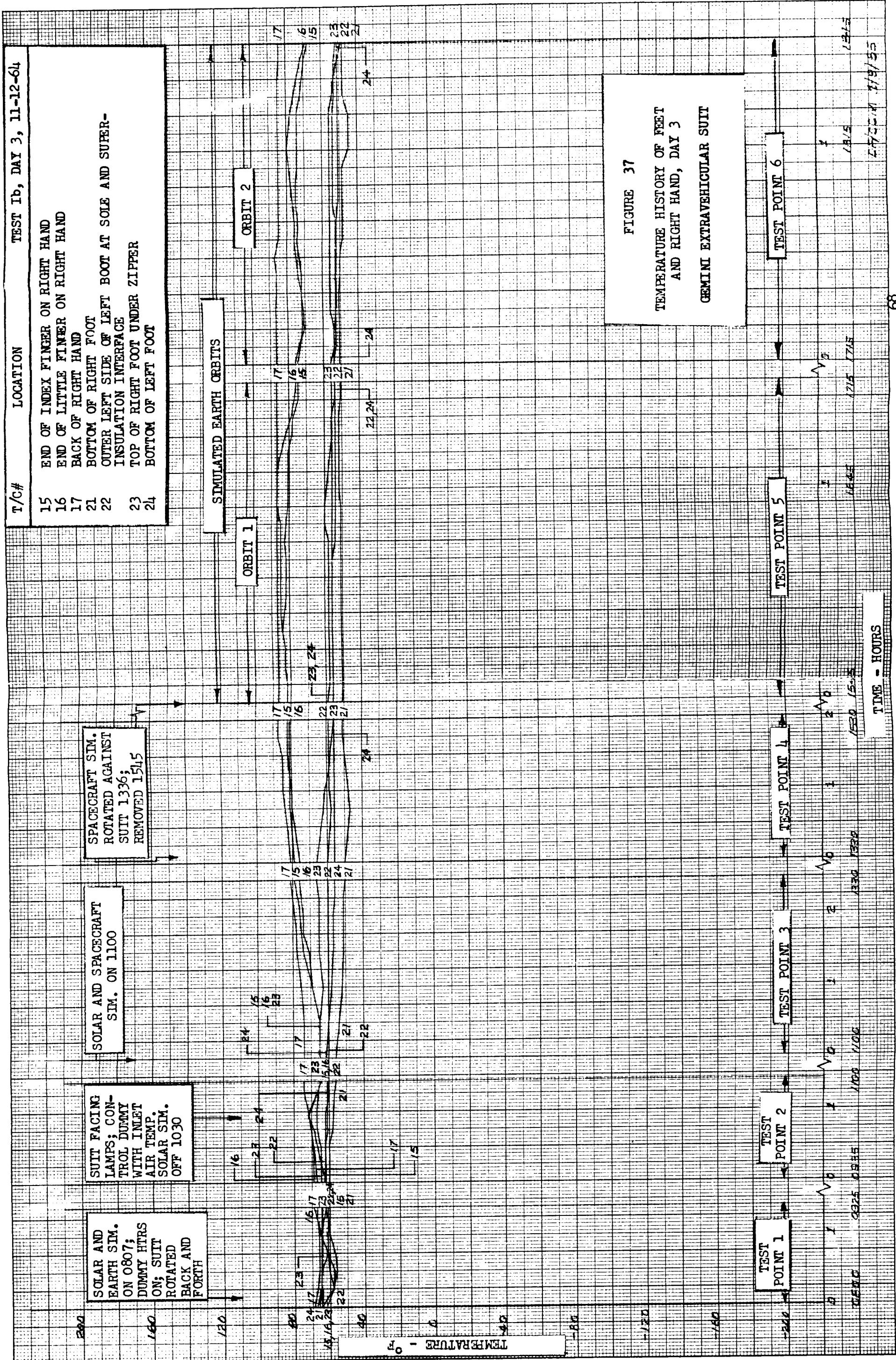


FIGURE 37
**TEMPERATURE HISTORY OF FEET
 AND RIGHT HAND, DAY 3**
GEMINI EXTRAVEHICULAR SUIT

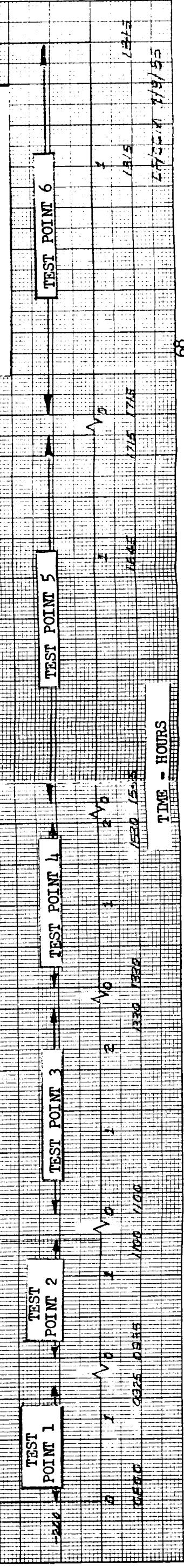


TABLE IV
COMPARISON OF MEASURED SUIT SURFACE TEMPERATURES AND CALCULATED
VALUES FOR A 200 NAUTICAL MILE EARTH ORBIT.

TEMPERATURE	(1) MEASURED °F	(2) CALCULATED °F
Suit surface temperature facing the sun	145	133**
Suit surface temperature facing the earth (sun side)	61	67**
Suit surface temperature facing the earth (dark side)	4	-20
Suit surface temperature facing deep space	-184	-180*

(1) Upper right chest and lower left back

(2) $\epsilon = 0.57$, $\alpha_{\text{solar}} = 0.273$ and flat plate view factors

* Based on a total heat loss of 150 BTU/Hr. and an area of 25 ft²

** Subsolar Point

Figures 32 through 34 show the temperature history of various suit layers in the lower left back area during the experiment. The effectiveness of the superinsulation is demonstrated in these figures. For example, on Day No. 1 from the end of test point No. 3 to the end of test point No. 5, the suit surface temperature decreased 243°F (from 61°F to -182°F) while the temperature of the interior mylon layers next to the pressure garment decreased by approximately 45°F from 70°F to 25°F . During the entire experiment the temperature of the interior nylon layers did not exceed $+100^{\circ}\text{F}$ or drop below 20°F . In general, the interlayer temperature variation shown in these figures is as would be expected; that is, during cold soak, the temperatures follow a steadily decreasing pattern from the interior nylon layers to the outer surface of the suit. However, with the solar lamps on, the suit surface temperature rapidly increases to a value higher than the nomex felt, Test Point No. 3, Day No. 1, Figure 32. The same situation holds true for Test Point No. 3, Day No. 2, Figure 33. In these test points it appears that the nomex felt serves as a heat sink for the warmer interior layers and outer surface.

The excellent duplication of conditions through simulated orbits 1 and 2 is shown in Figure 34. Also this figure shows the temperature of the interior nylon layers varied from only approximately 65 to 90°F during the two orbits while the suit outer surface varied from $+150^{\circ}\text{F}$ to -126°F .

Suit inlet pressure, pressure in the helmet area and pressure drop did not vary appreciably during the three test days. An analysis of the data shows the following variations in these parameters during the experiment:

Suit inlet pressure - $3.77 - 4.46 \text{ psia}$

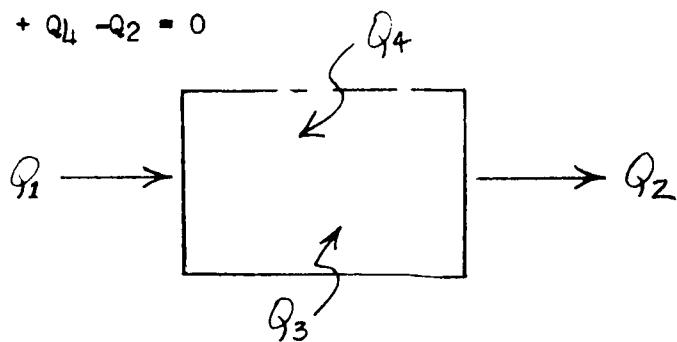
Suit pressure in - $3.80 - 4.40 \text{ psia}$
helmet area

Suit pressure drop - $.0812 - 0.115 \text{ psi}$

4.2.2 SUIT NET HEAT BALANCE

The heat loss out of the suit or heat leakage into the suit at steady state conditions can be determined by writing a heat balance for the suit as follows:

$$Q_1 + Q_3 + Q_4 - Q_2 = 0$$



Where

Q_1 = heat supplied by inlet gas, BTU/Hr.

Q_2 = heat removed by outlet gas, BTU/Hr.

Q_3 = heat transferred to ventilation gas from dummy,
BTU/Hr.

Q_4 = heat leakage into or out of suit, BTU/Hr.

Then

$$Q_1 + Q_3 + Q_4 = Q_2$$

$$WC_p t_i + 3.413 P + Q_4 = WC_p t_o$$

$$Q_4 = WC_p (t_o - t_i) - 3.413 P$$

Where

W = gas weight flow rate, lb/hr.

C_p = specific heat at constant pressure of gas,
BTU/lb °R.

t_o = outlet temperature of gas, °F.

t_i = inlet temperature of gas, °F.

P = dummy heater power, watts (1 watt = 3.413 BTU/hr.).

Using the above equation heat leakage into or out of the suit may be calculated.

The heat loss for Test Point No. 5, Day #1 (Figure 29) based on conditions at the end of the test point can be calculated as follows:

$$Q = 13.7 (.2485) (74-67) - 3.413 (50)$$

$$Q = 24 - 170$$

$$Q = - 146 \text{ BTU/Hr.}$$

The minus sign indicates a heat loss out of the suit. The heat balance was set up so that a minus sign always indicates a heat loss while a plus sign indicates a heat gain (heat leakage into the suit). This value is with the hood covering the helmet and visor.

With the hood off and the dummy surface temperature controlled with the dummy heaters (Test Point No. 1, Day No. 2) the calculated heat loss is as follows:

$$Q = 13.6 (2485) (76-74) - 3.413 (87.5)$$

$$Q = -291 \text{ BTU/Hr.}$$

Analysis of the data shows at least 50 BTU/Hr. of this total heat loss can probably be attributed to the heat capacity of the dummy. Also Figure 30 shows the suit surface temperatures are still decreasing, indicating steady state conditions have not been achieved. A difference of only 10°F (-155° compared to -165°F) in average suit surface temperature can mean a difference of 27 BTU/Hr. in the total heat transfer rate from the suit to its environment. Therefore a more realistic value for the net heat loss from the suit, in this case, would be approximately 200 BTU/Hr.

Test Point No. 2, Day No. 2, Figure 30 is a cold soak condition with the hood off where the dummy heater power was zero and the dummy surface temperature was maintained by controlling the inlet gas temperature. The heat loss for this condition is

$$Q = 14.2 (.2485) (65 - 104) - 3.413 (0)$$

$$Q = -138 \text{ BTU/Hr.}$$

This heat loss is believed to be low because the dummy face temperature could not be maintained at 85°F when the inlet gas temperature was used to control the dummy surface temperature. In the two previous heat loss calculations the dummy face temperature was approximately 83°F but at the end of the above test point the face temperature was 27°F .

In a similar manner the net heat leakage into or out of the suit at other test points can be determined. Calculated heat leakage data are presented in Table V. These calculations show that the maximum heat loss out of the suit is 291 BTU/Hr., while the maximum heat leakage into the suit is 18 BTU/Hr. under the conditions imposed during this experiment.

For a heat loss of 146 BTU/Hr. from the suit, the over-all heat transfer coefficient or conductance, U , is

$$Q = UA \Delta t$$

$$U = \frac{146}{25 (78 - (-165))}$$

$$U = 0.024 \frac{\text{BTU}}{\text{hr. ft}^2 \text{ }^{\circ}\text{F}}$$

based on a suit surface area of 25 square feet, an average inner surface temperature of 78°F and an average suit surface temperature of -165°F . If the visor and helmet are assumed to contribute approximately 50 BTU/Hr. to the total heat loss and have an area of 2 square feet, the conductance for the suit alone is

TABLE V
CALCULATED NET SUIT
HEAT LEAKAGE

Test Day No.	Test Point No.	Test Point Description	Heat Leakage BTU/Hr.
1	5	Cold soak. Hood covering helmet and visor. Dummy surface temperature controlled with dummy heaters.	-146
2	1	Cold Soak. Hood off and two 20% transmittance visors installed. Dummy surface temperature controlled with dummy heaters.	-291
2	2	Cold soak. Hood off and two 20% transmittance visors installed. Dummy surface temperature controlled with inlet gas.	-138
1	3	Full simulation: Solar lamps on; earth simulator on. Suit facing lamps with hood covering helmet and visor.	-25
2	3	Full simulation. Suit facing lamps with hood off and two 20% transmittance visors installed.	+7
2	4	Full simulation. Back facing lamps. Hood off; two 20% transmittance visors installed.	-18
3	3	Full simulation. Suit facing lamps with clear visor. Simulated spacecraft (180°F) surface on right side of suit.	+14
3	4	Full simulation. Suit facing lamps with clear visor. Spacecraft surface (180°F) in contact with suit.	+18

(+) Indicates a net heat gain

(-) Indicates a net heat loss

$$U = \frac{96}{23[78 - (-165)]}$$

$$U = 0.0172 \text{ BTU/Hr. ft}^2 \text{ }^{\circ}\text{F}$$

which agrees with previous test results, (Reference 6).

4.2.3 NET HEAT GAIN OR LOSS THROUGH VISOR

Comparing suit heat leakage values with the suit facing the lamps and the back facing the lamps, (Day No. 2, Table V) a change in heat leakage from +7 to -18 BTU/Hr. is observed. This variation would indicate the heat leakage through the two, 20% transmittance visors to be approximately 25 BTU/Hr. into the suit. Also Table V shows the suit net heat leakage with the hood "on" is -25 BTU/Hr. (Test Point No. 3, Day No. 1) while the suit net heat leakage with the hood "off" is +7 BTU/Hr. (Test Point No. 3, Day No. 2). This difference indicates a visor heat leakage of approximately 32 BTU/Hr. into the suit between the hood "on" and hood "off" conditions with the suit facing the lamps and full simulation (solar lamps on, earth simulator on) applied to the exterior of the suit.

Heat loss from the visor during the cold soak condition was impossible to determine from the over-all suit heat balance. However, the difference in power requirements for the heaters in the dummy head with the hood on and hood off gives an indication of the heat loss. The total power to the heaters in the dummy head at the end of Test Point No. 5, Day No. 1 (hood on), was 5 watts. At the end of Test Point No. 1, Day No. 2 (hood off, two 20% transmittance visors), the total power to the heaters in the head was 25 watts to maintain the same dummy face temperature. This 20 watt increase is equivalent to about 68 BTU/Hr. Part of this energy is transferred to the ventilation gas stream but the amount conducted through the visor and radiated from the outside surface can be calculated from the visor temperature. The temperature of the outside surface of the pressure visor at the end of Test Point No. 1, Day No. 2 was about 24°F . Assuming the outer surface of the outside tinted visor is 24°F (actually it would be less) and an emittance of 0.9 for the plexiglass, the heat loss from the 71 square inch visor surface would be

$$\begin{aligned} q &= \epsilon \sigma A T^4 \\ &= .9 (.1713 \times 10^{-8}) (.493)(484)^4 \end{aligned}$$

$$q = 42 \text{ BTU/Hr.}$$

This visor heat loss added to the -146 BTU/Hr. total heat loss calculated for test point No. 5, Day No. 1, (cold soak; hood on) would result in a total heat loss from the suit of

$$Q_{\text{total}} = -146 - (-42)$$

$$Q_{\text{total}} = -188 \text{ BTU/Hr.}$$

with the hood off and tinted visors installed. This value is in agreement with the -200 BTU/Hr. suggested in Paragraph 4.2.2 for Test Point No. 1, Day No. 2.

Therefore, these data indicate there is a net heat gain through visor of 30-40 BTU/Hr. when facing the sun and a net heat loss of 40-50 BTU/Hr. when facing deep space.

4.2.4 VISOR FROSTING

On Test Day No. 2 the humidity in the helmet was increased and a deflection in the oscillograph trace, indicating a decrease in light intensity to the photoelectric cell, was noted. The visor temperatures at this time were below 32°F and the deflection was possibly an indication of visor frosting. However, although the deflection occurs at approximately the same time as the increase in humidity, there is not always a good correlation between increases in humidity and deflections of the oscillograph trace. For a ventilation gas temperature of 85°F in the helmet area and a visor temperature below 32°F, the relative humidity in the helmet would have to be less than 14% for frosting not to occur. Relative humidity measurements as high as 95% in the helmet area were recorded during this phase of the test and although the data are not conclusive, visor frosting very likely did occur.

4.2.5 THERMAL ADEQUACY OF SUIT

Except for the hands and feet, the suit would appear to be thermally adequate. Figures 35 through 37 show the history of temperature measurements at various locations on the feet and right hand during the three test days. Temperatures near freezing or below were recorded for the feet and unheated hand on Days 1 and 2 with maximum thermal inputs to the suit from the solar lamps and earth simulator. Temperatures on the heated portions of both arms and legs were approximately the same as the torso temperatures at the various test points. Prior to Day No. 3 insulation was added to the bottom of the left foot and an insulated mitten was added to the right hand. The higher hand and feet temperatures recorded on the third test day were influenced by both the added insulation and the radiation from the simulated spacecraft surface. From the data it is not possible to determine the contribution of each. Temperatures on the right hand increased with an increase in temperature of the spacecraft surface, while temperatures on both feet remain relatively constant. The temperature on the bottom of the left foot is about 5-6°F higher than the bottom of the right foot; however, the bottom of the left foot was observed to be warmer than the right foot on previous days.

The 200-300 BTU/Hr. heat loss is larger than would be encountered in actual earth orbit since the suit will always be receiving the earth's thermal radiation. The slight heat leakage into the suit when facing the sun should not pose a severe problem for the environmental control system.

4.2.6 "HOT SPOTS" RESULTING FROM CONTACT WITH SPACECRAFT SURFACE

Contact with the 180° F simulated spacecraft surface did not produce a significant increase in dummy surface temperatures in the contact area. The total heat leakage into the suit may increase slightly (Table V, Test Point No. 4, Day No. 3) due to an increase in local suit surface temperatures but contact with the hot spacecraft surface did not create a "hot spot" in the sense of excessive temperatures on the interior of the suit.

Figure 38 shows the effect of mechanical loading on the apparent thermal conductivity of various numbers of aluminized layers in a vacuum. These data show that the apparent thermal conductivity of the layers increases abruptly (possibly by a factor of 100) with the initial application of load. However, after the load reaches about 2 psi the apparent thermal conductivity becomes practically independent of load and the maximum value attained is low indicating that radiation is still the predominant mode of heat transfer. Therefore, analysis of these data indicate that contact with a 180° F spacecraft surface should not produce a significant "hot spot" on the suit.

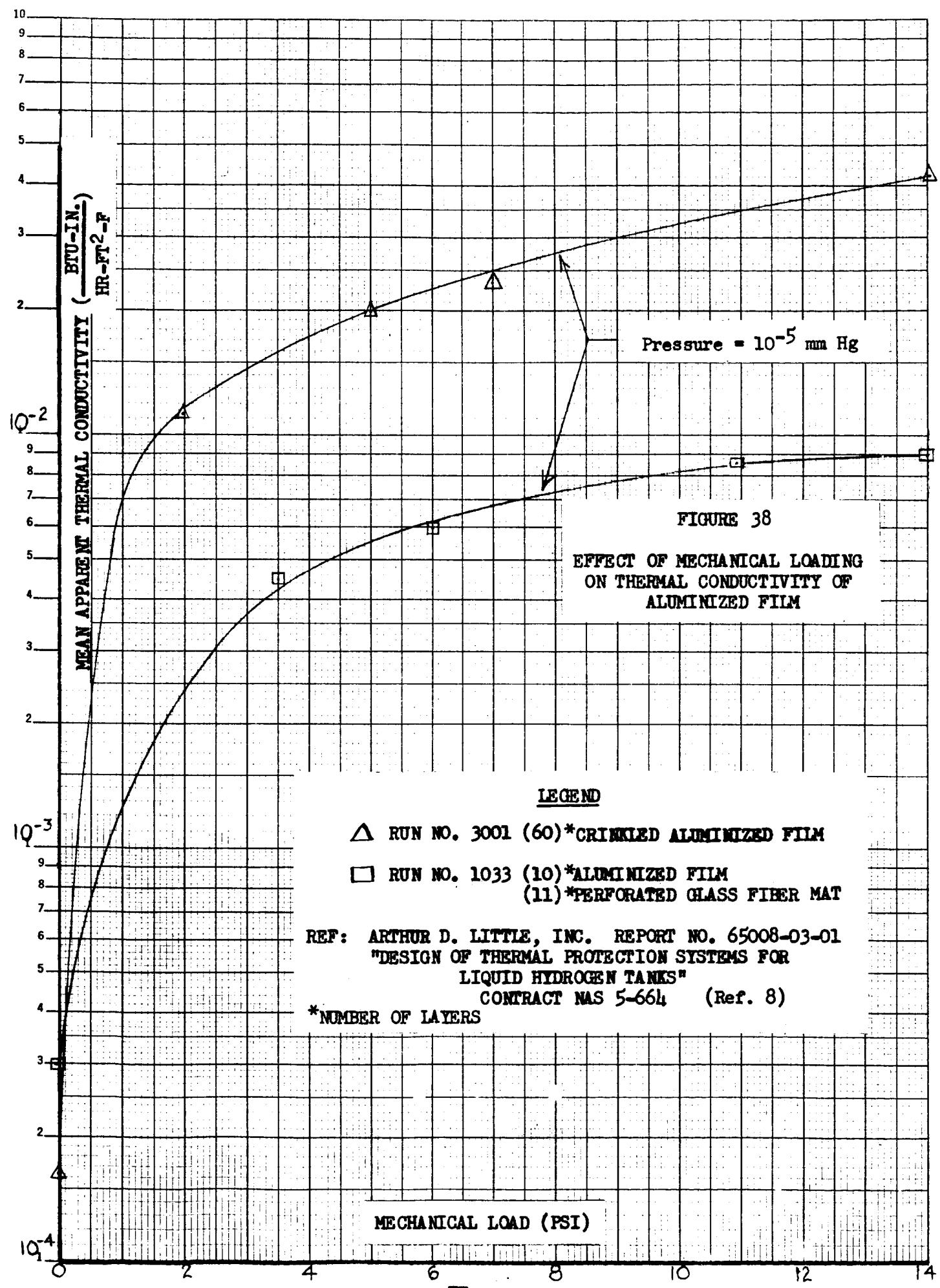
4.2.7 SUIT GAS LEAKAGE

Suit ventilation gas leakage was measured periodically during the three test days and varied between 140 and 190 cc/min. The Phillips gauges mounted external to the suit did not indicate the source of the leakage.

4.2.8 EFFECT OF COMPRESSION UNDER PARACHUTE HARNESS

During this series of tests the suit and dummy were partially supported by the parachute harness thereby imposing a greater compressive load under the harness straps than might ordinarily be experienced. Analysis of the data shows no significant difference in temperature between points on the dummy surface in the area of the straps and those on the underwear directly under the straps. The effect of harness compression on interlayer temperatures does not appear significant based on measurements in the upper left back area (under the harness) and the lower left back area (not under the harness). For example, Test Point No. 4, Day No. 2, with the back of the suit facing the solar lamps, the suit surface temperatures at the above locations are 132°F and 131°F respectively. The corresponding temperatures on the interior side of the nomex felt are 101°F and 100°F, while the temperatures on the exterior side of the second layer of aluminized mylar are 93°F and 106°F. Temperatures with the back of the suit facing the earth simulator do not agree as well because of the difference in view factor between the two locations and the earth simulator.

Suit surface temperatures under the harness are generally higher than adjacent surface temperatures based on an analysis of measurements made in the right chest and upper right back areas. During the cold soak condition the suit surface under the harness may be as much as 50-60°F warmer than the adjacent suit surface, due to the insulating effect of the harness. When facing the solar lamps the surface under the strap is only about 10°F higher than the bare suit surface. This slight difference could be due to a higher absorptance for the harness material.



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3 CYCLES X 140 DIVISIONS
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5.0 CONCLUSIONS & RECOMMENDATIONS

Based on the results of this experiment the following is concluded with regard to the performance of the Gemini Extravehicular Suit under the test conditions imposed:

1. Suit surface temperatures should not exceed +200°F or be colder than -200°F during a near-earth orbit. Pressure in the helmet area is about 0.06 psi less than the suit inlet pressure (3.7 psia nominal). Total suit pressure drop is approximately 0.1 psi at 11.5 ACFM (3.7 psia, 70°F).
2. Maximum heat loss from the suit should not exceed 250 BTU/Hr. Maximum heat leakage into the suit is approximately 20 BTU/Hr.
3. Heat leakage through the visor is approximately 30-40 BTU/Hr. into the suit when facing the sun and about 40-50 BTU/Hr. out of the suit when facing deep space.
4. Visor frosting is possible when the visor faces deep space as visor surface temperature drops below the freezing point. When facing the sun, visor surface temperatures are approximately 90-100°F and condensation is not likely to occur.
5. The suit is thermally adequate except for the gloves and boots. Insulation should be added to these locations.
6. Contact with the 180°F simulated spacecraft surface did not produce "hot spots" on the interior of the suit.
7. Suit ventilation gas leakage should not exceed 200 cc/min.
8. Compression under the parachute harness does not result in "hot spots" on the interior of the suit.

APPENDIX A

TABULATED TEST DATA

TEST DAY NO. 1
HOOD COVERING HELMET
AND VISOR. SUIT SUPPORTED
FROM TIEDOWN CABLE.
PROTECTIVE GLOVE ON RIGHT HAND

TEST DAY NO. 1

TEST POINT NO. 1

COLD SOAK. DUMMY

SURFACE TEMPERATURE

CONTROLLED WITH DUMMY HEATERS.

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT II

TEST DAY NO. 1

TEST POINT NO. 1

DATE 5 November 1964

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 1

TEST POINT NO. 1

DATE 5 November 1964

TEMPERATURE °F

Chan. No.	TIME OF DAY									
	1200	1215	1230	1245	1300	1315	1330	1345	1400	
027	119	113	104	98	92	87	92	87	82	
28	114	108	100	95	89	84	88	83	78	
29	88	89	84	82	78	75	74	74	70	
30	130	123	114	105	98		95	89	82	
31	117	109	102	96	91	87	91	85	80	
32	117	110	104	98	93	88	91	87	82	
33	123	117	108	100	92	87	91	84	78	
34	126	119	110	102	95	88	92	87	79	
35	117	109	101	94	87	81	85	78	74	
36	119	114	109	105	101	98	101	97	92	
37	118	113	108	104	100	97	100	96	91	
38	118	110	101	93	86	79	82	75	69	
39	118	110	99	91	85	81	85	72	64	
40	121	114	106	97	90	84	88	79	73	
41	111	102	95	85	81	77	86	68	61	
42	125	117	108	100	94	89	95	87	82	
43	117	110	101	94	87	80	84	78	70	
44	80	79	78	74	71	69	67	65	62	
45	122	114	106	100	94	89	95	88	82	
46	118	114	109	105	101	97	100	96	92	
47	118	114	109	104	100	97	100	96	91	
48	123	114	105	98	91	85	89	83	75	
49	121	113	104	96	89	84	87	81	74	
50										
51										
52										

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 1

TEST POINT NO. 1

DATE 5 November 1964

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 1

TEST POINT NO. 1

DATE 5 November 1964

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 1

TEST POINT NO. 1

DATE 5 November 1964

TEMPERATURE °F

Chan. No.	TIME OF DAY								
	1200	1215	1230	1245	1300	1315	1330	1345	1400
105									
106									
107									
108					-280	-280	-286	-287	
109					-294	-294	-297	-292	
110					-308	-308	-309	-310	
111					-317	-318	-318	-320	
112					-300	-302	-300	-302	
113					-308	-309	-307	-307	
114	114	107	100	94	89	86	89	82	78
115	121	114	108	101	96	92	96	91	84
116	108	105	102	97	93	89	88	87	83
117	107	104	101	96	93	89	88	87	82
118									
119	88	87	85	82	79	76	75	74	71
120	126	128	122	128	128	129	128	128	127
121	104	104	100	97	93	89	87	87	83
122	-88	-94	-98	-105	-111	-116	-117	-119	-124
123	-137	-141	-141	-147	-149	-153	-155	-156	-157
124	-150	-153	-154	-157	-161	-164	-168	-168	-170
125	-108	-113	-117	-122	-126	-132	-136	-138	-143
126									
127									
128									
129									
130									

TEST DAY NO. 1

TEST POINT NO. 2

EARTH SIMULATION

(ONLY) ON BACK OF SUIT.

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 1b

TEST DAY NO. 1

TEST POINT NO 2

DATE 11-5-64

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 1B

TEST DAY NO. 1

TEST POINT NO 2

DATE 11-5-64

TEMPERATURE °F

Chan. No.	TIME OF DAY									
	1720	1735	1750	1805	1820	1835	1850	1905	1920	
27	85	85	85	85	85	85	85	85	87	
28	82	82	83	82	82	83	83	82	84	
29	67	68	69	69	69	69	69	69	69	
30	97	95	91	90	88	87	87	85	85	
31	83	82	83	83	84		84	84	85	
32	83	84	84	85	85	85	85	85	85	
33	88	87	82	81	79	78	78	76	77	
34	93	91	88	86	85	84	83	82	82	
35	80	78	74	74	72	70	69	69	69	
36	87	85	84	84	84	84	84	84	85	
37	85	85	84	84	84	85	85	85	87	
38	81	81	82	83	85	82	84	86	86	
39	86	86	88	88	89	86	86	86	86	
40	87	86	82	80	79	77	76	75	76	
41	86	86	86	87	86	86	86	85	86	
42	87	87	88	88	88	88	88	88	89	
43	80	78	74	72	71	70	69	67	69	
44	59	60	60	60	60	60	60	60	61	
45	86	87	87	87	87	87	87	87	88	
46	87	85	85	85	85	85	85	85	87	
47	87	85	84	84	84	84	84	84	85	
48	87	88	88	88	88	87	87	88	88	
49	87	86	87	87	87	85	87	88	90	
50										
51										
52										

CEMING EXTRAVEHICULAR SUIT TEST

EXPERIMENT Th

TEST DAY NO. 1

WCR POINT NO 2

DATE 11-5-64

TEMPERATURE °F

Chan. No.	TIME OF DAY									
	1720	1735	1750	1805	1820	1835	1850	1905	1920	
53										
54										
55										
56										
57	21	24	24	24	25	24	24	24	24	
58										
59	54	56	56	56	56	56	56	56	56	
60										
61										
62	-19	-19	-18	-18	-19	-19	-19	-19	-19	
63	-5	-4	-4	-4	-4	-5	-4	-4	-4	
64	16	18	19	19	18	18	18	18	18	
65										
66										
67	43	44	45	46	46	46	46	46	46	
68	-116	-116	-116	-116	-116	-116	-117	-116	-116	
69	-24	-24	-23	-23	-23	-23	-23	-23	-23	
70	-82	-81	-81	-81	-81	-81	-81	-81	-81	
71	-30	-30	-30	-30	-31	-31	-31	-31	-31	
72	-94	-93	-93	-92	-92	-92	-92	-90	-90	
73	-28	-28	-26	-27	-27	-27	-27	-26	-27	
74	-156	-156	-156	-156	-156	-156	-156	-156	-156	
75	-174	-174	-173	-173	-174	-174	-174	-174	-174	
76	-170	-169	-168	-168	-168	-168	-168	-169	-168	
77	-137	-136	-135	-135	-134	-135	-135	-136	-135	
78	-149	-149	-149	-149	-147	-148	-149	-149	-149	

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Th

TEST DAY NO. 1

WEST POINT NO 2

DATE 11-5-64

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 1b

TEST DAY NO. 1

TEST POINT NO 2

DATE 11-5-64

TEMPERATURE °F

TEST DAY NO. 1
TEST POINT NO. 3
SOLAR SIMULATION ON
FRONT OF SUIT; EARTH
SIMULATION ON BACK.

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Tb

TEST DAY NO. 1

TEST POINT NO 3

DATE 5 Nov. 1964

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Tb

TEST DAY NO. 1

TEST POINT NO 3

DATE 5 Nov. 1964

TEMPERATURE °F

Chan. No.	TIME OF DAY		
	2205	2220	
1	118	118	
2	121	114	
3	80	81	
4	81	81	
5	88	88	
6	87	88	
7			
8	85	85	
9	91	91	
10	91	91	
11	79	79	
12	87	87	
13	81	81	
14	87	87	
15	29	33	
16	1	2	
17	40	43	
18	94	93	
19	92	92	
20	85	85	
21	4	4	
22	16	17	
23	21	21	
24	14	14	
25	88	88	
26	85	85	

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Tb

TEST DAY NO. 1

TEST POINT NO 3

DATE 5 Nov. 1964

TEMPERATURE °F

Chan. No.	TIME OF DAY										
	1920	1935	1950	2005	2020	2035	2050	2105	2120	2135	2150
027	87	87	88	90	91	92	91	89	89	89	89
28	84	83	83	85	87	87	87	85	85	85	84
29	69	69	74	77	78	80	82	81	82	81	82
30	85	85	84	87	87	88	88	87	87	87	87
31	85	84	87	88	89	89	89	88	87	87	87
32	85	85	87	88	88	89	88	87	87	87	87
33	77	76	75	77	78	78	78	78	77	78	78
34	82	81	81	83	84	85	85	85	85	85	85
35	69	69	69	70	72	73	73	74	74	74	74
36	85	85	87	89	91	92	92	93	93	93	93
37	87	85	86	89	91	91	91	91	91	91	91
38	86	87	85	86	89	91	90	89	88	86	86
39	86	86	86	88	89	91	89	86	84	83	84
40	76	75	75	76	76	77	77	75	74	74	74
41	86	88	88	89	90	90	88	88	85	84	85
42	89	89	89	90	91	91	89	87	87	87	87
43	69	67	67	69	70	71	71	70	70	70	71
44	61	62	69	74	74	78	78	78	78	78	78
45	88	88	88	89	90	91	88	87	87	86	87
46	87	87	87	88	89	91	91	90	90	90	90
47	85	85	85	87	88	89	91	90	90	90	90
48	88	87	87	88	88	89	88	84	84	82	81
49	90	90	89	91	92	92	91	88	88	87	87
50											
51											
52											

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Tb

TEST DAY NO. 1

TEST POINT NO 3

DATE 5 Nov. 1964

TEMPERATURE °F

Chan. No.	TIME OF DAY									
	2205	2220								
027	89	88								
28	85	84								
29	82	82								
30	87	87								
31	87	87								
32	87	87								
33	78	78								
34	85	85								
35	74	75								
36	93	93								
37	91	91								
38	86	85								
39	82	81								
40	74	75								
41	84	84								
42	87	87								
43	71	72								
44	78	78								
45	87	87								
46	90	90								
47	90	91								
48	81	80								
49	85	85								
50										
51										
52										

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Tb

TEST DAY NO. 1

TEST POINT NO 3

DATE 5 Nov. 1964

TEMPERATURE °F

Chan. No.	TIME OF DAY										
	1920	1935	1950	2005	2020	2035	2050	2105	2120	2135	2150
053											
54											
55											
56											
57	24	28	35	40	43	46	47	47	47	47	47
58											
59	56	56	60	62	65	66	67	67	67	67	67
60											
61											
62	-19	5	29	36	38	40	42	42	43	43	43
63	-4	14	34	42	44	46	47	48	48	48	48
64	18	29	44	51	53	56	56	57	57	57	58
65											
66											
67	46	49	51	56	60	62	65	67	69	69	69
68	-116	65	134	146	150	154	157	157	157	158	159
69	-23	-6	11	16	18	18	20	20	20	20	20
70	-81	53	135	146	148	150	152	152	152	153	153
71	-31	9	25	29	29	30	30	29	29	30	29
72	-90	-10	104	131	140	145	148	150	150	150	151
73	-27	-16	1	10	12	14	14	15	15	15	15
74	-156	-34	-8	-5	-5	-5	-5	-6	-6	-6	-6
75	-174	-95	-71	-66	-65	-65	-65	-65	-65	-65	-67
76	-168	34	80	84	85	85	85	83	82	83	83
77	-135	94	138	140	142	142	143	142	142	143	143
78	-149	115	180	184	185	186	186	184	184	185	184

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 1b

TEST DAY NO. 1

TEST POINT NO 3

DATE 5 Nov. 1964

TEMPERATURE °F

Chan. No.	TIME OF DAY		
	2205	2220	
053			
54			
55			
56			
57	48	47	
58			
59	67	67	
60			
61			
62	43	43	
63	49	49	
64	58	58	
65			
66			
67	70	70	
68	158	160	
69	20	20	
70	153	153	
71	29	29	
72	152	151	
73	15	15	
74	-7	-6	
75	-66	-66	
76	82	83	
77	142	145	
78	184	185	

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 1b

TEST DAY NO. 1

TEST POINT NO 3

DATE 5 Nov. 1964

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT I^b

TEST DAY NO. 1 TEST POINT NO 3 DATE 5 Nov. 1964

TEMPERATURE °F

Chan. No.	TIME OF DAY		
	2205	2220	
079	173	174	
80	114	117	
81	157	158	
82	139	140	
83	172	174	
84	166	168	
85	-25	-21	
86	28	28	
87	30	30	
88	6	6	
89	61	61	
90	28	28	
91	19	20	
92	29	29	
93	22	22	
94	79	79	
95	91	91	
96	79	82	
97	78	77	
98	71	70	
99			
100	66	66	
101	60	58	
102	92	91	
103			
104			

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT I^b

TEST DAY NO. 1

TEST POINT NO 3

DATE 5 Nov. 1964

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 1b

TEST DAY NO. 1

TEST POINT NO 3

DATE 5 Nov. 1964

TEMPERATURE °F

TEST DAY NO. 1

TEST POINT NO. 4

SOLAR SIMULATION ON

RIGHT SIDE OF SUIT; EARTH

SIMULATION ON LEFT SIDE.

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENTAL

TEST DAY NO. 1

TEST POINT NO. 4

DATE 5 November 1964

TEMPERATURE °F

Chan. No.	TIME OF DAY				
	0015	0025	0035	0045	
001	123		123	129	
2	111	122		108	
3	85	84	83	82	
4	85	84	83	83	
5	87	84	80	79	
6	87	85	84	85	
7					
8	85	85	84	85	
9	92	92		92	
10	91	91	91	92	
11	79		78	78	
12	87	86	85	87	
13	82	82	81	81	
14	87	87	85	87	
15	67		74	66	
16	20	40		48	
17	60		69	69	
18	95	94	93	93	
19	91	90	88	88	
20	85	81	75	74	
21	10	12	14	14	
22	20	23	24	24	
23	25	25	23	24	
24	19	20	21	21	
25	88	87	86	87	
26	85		83	85	

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT I^b

TEST DAY NO. 1

TEST POINT NO. 4

DATE 5 November 1964

TEMPERATURE °F

Chan. No.	TIME OF DAY				
	0015	0025	0035	0045	
027	89		87	88	
28	85	85	84	85	
29	82	81	80	80	
30	91	91	91	93	
31	88	87	87	87	
32	87	86	85	87	
33	80	81	80	82	
34	89	91	91	93	
35	78	78	77	80	
36	96	94	93	94	
37	91	91	89	91	
38	86	88	86	89	
39	79	81	77	80	
40	77	79	77	80	
41	82	85	84	85	
42	87	87	87	88	
43	76	76	75	78	
44	78	75	74	74	
45	87	87	85	87	
46	91	89	88	89	
47	91	91	91	92	
48	78	78	77	79	
49	85	85	87	88	
50					
51					
52					

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT No

TEST DAY NO. 1

TEST POINT NO. 4

DATE 5 November 1964

TEMPERATURE °F

Chan. No.	TIME OF DAY				
	0015	0025	0035	0045	
53					
54					
55					
56					
57	56	48	43	39	
58					
59	71	68	65	65	
60					
61					
62	57	45	24	7	
63	66	53	40	23	
64	70	60	51	39	
65					
66					
67	76	75	74	71	
68	60	-1	-28	-40	
69	31		4	-10	
70		131	77	18	
71	-39	-46	-118	-143	
72	36	102	77	37	
73	-7	1	-5	-28	
74	116	129	-52	-110	
75	121	140	-50	-109	
76	60	43	-75	-116	
77	57	39	-70	-106	
78	70	5	-57	-92	

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 1

TEST POINT NO. 4

DATE 5 November 1964

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 1b

TEST DAY NO. 1

TEST POINT NO. 4

DATE 5 November 1964

TEMPERATURE °F

Chan. No.	TIME OF DAY			
	0015	0025	0035	0045
105				
106				
107				
108				
109	-292	-282	-282	-282
110	-307	-296	-294	-290
111		-316		-312
112			-320	-320
113	-319	-309	-310	-311
114		318		
115	86	85	85	86
116	87	88	87	88
117	83	84	84	84
118	84	84	84	84
119				
120	83	81	80	80
121	126	129	129	129
122	94	94	94	94
123	-35	-59	-81	-94
124	111	97	-50	-105
125	113	101	-65	-108
126	-9	-24	-93	-116
127				
128				
129				
130				

TEST DAY NO. 1

TEST POINT NO. 5

COLD SOAK. DUMMY

SURFACE TEMPERATURE CONTROLLED

WITH DUMMY HEATERS.

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 1

TEST POINT NO. 5

DATE 12-4-64

TEMPERATURE °F

Chan. No.	TIME OF DAY										
	0100	0200	0300	0400	0415	0430	0445	0500			
1	118	113	110	114	109	110	110	114			
2	107	103	100	104		69		108			
3	80	69	61	60	59	57	56	56			
4	81	71	61	61	61	59	58	57			
5	76	63	56	54	54	53	52	52			
6	85	82	84	77	77	77	75	75			
7											
8	86	85	83	79	79	78	78	77			
9	92	90	87	85	85	83	83	82			
10	93	89	87	83	83	82	81	80			
11	79	80	78	75	75	74	74	74			
12	88	89	87	85	85	83	82	82			
13	80	74	69	66	66	65	65	65			
14	87	87	84	82	81	80	80	79			
15	51	-12	-46	-65	-67	-73	-77	-79			
16	36	-20	-46	-60		-65	-66	-68			
17	67	56	45	33	33	28	27	25			
18	94	89	85	82	82	81	80	79			
19	88	87	84	81	81	80	79	79			
20	72	63	56	53	53	51	51	49			
21	15	16	8	8	7	6	6	6			
22	23	18	9	10	10	9	9	9			
23	23	19	17	14	14	12	12	11			
24	21	21	14	14	14	14	12	11			
25	88	87	84	81	81	80	80	79			
26	85	83	82	78	78	76	76	75			
27	88	87	85	82	81	80	80	80			
28	85	83	82	78	77	76	75	74			
29	80	74	71	67	67	66	66	65			
30	95	92	88	84	83	81	80	80			

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 1

TEST POINT NO. 5

DATE 12-4-64

TEMPERATURE °F

Chan. No.	TIME OF DAY								
	0100	0200	0300	0400	0415	0430	0445	0500	
31	88	87	85	80	89	79	78	78	
32	87	87	85	81	81	80	79	78	
33	83	85	82	79	79	78	76	75	
34	94	91	85	81	80	78	78	76	
35	80	80	78	74	74	71	70	69	
36	94	90	87	84	83	82	82	81	
37	90	89	87	84	84	83	82	82	
38	89	84	81	77	77	75	74	73	
39	81	82	80	77	77	77	76	75	
40	82	84	82	78	77	76	75	74	
41	86	85	83	81	81	80	80	79	
42	89	88	87	83	82	81	81	80	
43	79	79	78	72	71	70	69	68	
44	74	68	62	60	60	58	58	57	
45	88	88	85	82	82	81	80	80	
46	90	89	87						
47	92	89	85	82	82	81	80	79	
48	80	81	80	77	76	75	74	74	
49	89	87	82	78	78	76	75	74	
50									
51									
52									
53									
54									
55									
56									
57	34	9	-4	210	-10	-13	-13	-14	
58									
59	62	51	42	39	39	38	35	35	
60									

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 1

TEST POINT NO. 5

DATE 12-4-64

TEMPERATURE °F

Chan. No.	TIME OF DAY								
	0100	0200	0300	0400	0415	0430	0445	0500	
61									
62	-9	-66	-89	-100	-101	-103	-105	-106	
63	8	-43	-63	-72	-72	-75	-76	-77	
64	28	-9	-24	-30	-30	-33	-33	-34	
65									
66									
67	68	46	33	28	26	25	25	25	
68	-51	-87	-101	-111	-111	-114	-115	-116	
69	-22	-70	-90	-102	-103	-106	-108	-108	
70	-20	-71	-76	-79	-81	-81	-81	-82	
71	-157	-188	-195	-198	-200	-201	-201	-203	
72	0	-74	-87	-93	-93	-94	-95	-95	
73	-51	-98	-112	-119	-119	-122	-123	-123	
74	-135	-164	-173	-177	-177	-180	-181	-181	
75	-138	-175	-183	-189	-189	-199	-191	-191	
76	-140	-177	-186	-190	-190	-191	-191	-191	
77	-124	-146	-150	-153	-153	-154	-154	-153	
78	-114	-150	-160	-164	-164	-166	-167	-167	
79	-108	-150	-166	-174	-174	-176	-177	-177	
80	-84	-132	-150	-159	-160	-162	-163	-164	
81	-67	-101	-114	-120	-119	-123	-124	-125	
82	-31	-73	-92	-101	-103	-106	-108	-109	
83	-134	-161	-168	-170	-170	-172	-173	-174	
84	-106	-147	-159	-164	-164	-166	-167	-168	
85	65	-10	-59	-87	-89	-96	-100	-104	
86	-47	-118	-148	-164	-166	-170	-172	-174	
87	-48	-105	-128	-140	-141	-144	-146	-147	
88	-137	-162	-170	-174	-175	-177	-176	-176	
89	-125	-162	-177	-181	-181	-185	-184	-184	
90	-124	-167	-183	-190	-191	-193	-194	-195	

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 1

TEST POINT NO. 5

DATE 12-4-64

TEMPERATURE °F

Chan. No.	TIME OF DAY								
	0100	0200	0300	0400	0415	0430	0445	0500	
91	-155	-167	-190	-193	-194	-196	-195	-196	
92	-114	-156	-173	-181	-181	-184	-186	-186	
93	-136	-163	-173	-177	-177	-179	-180	-181	
94	77	78	75	73	72	71	70	70	
95	89	84	79	76	76	74	74	74	
96	79	74	67	69	69	67	67	67	
97	21	-70	-110	-132	-133	-140	-144	-147	
98	23	-70	-111	-133	-135	-142	-144	-148	
99									
100	20	-65	-105	-128	-129	-137	-138	-143	
101	9	-76	-116	-136	-140	-144	-149	-151	
102	26	-61	-101	-125	-126		-137	-140	
103									
104									
105									
106									
107									
108									
109	-280	-281	-282	-277	-279	-281	-280	-279	
110	-292	-292	-292	-292	-290	-290	-290	-292	
111	-310	-308	-309	-305	-305	-307	-307	-307	
112	-319	-318	-316	-311	-312	-312	-316	-316	
113	-311	-308	-302	-298	-299	-300	-301	-297	
114		-318	-308	-307	-308	-309	-309	-302	
115	86	84	83	79	78	77	77	76	
116	88	88	87	83	83	82	81	81	
117	85	85	83	81	80	79	78	78	
118	85	85	83	80	80	79	78	78	
119									
120	79	75	71	68	68	67	66	65	

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Tb

TEST DAY NO. 1

TEST POINT NO. 5

DATE 12-4-64

TEMPERATURE °F

SUIT FLOW SYSTEM
GEMINI EXTRAVEHICULAR SUIT
EXPERIMENT Ib

TEST DAY NO. 1 DATE: 11-5-64 to 11-6-64

TIME	ROTAMETER		VOL/FLOW							
	PRESSURE PSIA	TEMP OF	FLOW SCFM*	SUIT OUTLET PRESS. PSIA	TEMP OF	FLOW ACFM	SUIT LEAKAGE CC/MIN			
1130	14.7	70	3.04	3.74	95	11.7				
1200	↑	↑	3.08	3.78	89	11.5				
1230			3.10	3.78	81	11.3				
1300			3.11	3.72	70	11.2				
1330			3.12	3.73	68	11.15				
1400			3.13	3.74	66	11.15	142			
1500			2.90	3.75	69	10.35				
1530			2.96	3.75	69	10.50				
1600			2.97	3.78	67	10.35				
1630			2.97	3.78	66	10.4				
1700			2.95	3.74	70	10.6				
1730			2.96	3.76	69	10.5				
1800			2.96	3.75	67	10.5				
1830			2.98	3.74	68	10.6				
1900			2.99	3.74	69	10.6				
1930			2.93	3.73	70	10.5	140			
2000	.	.	2.99	3.74	68	10.6				
2030	.	.	3.00	3.76	68	10.5				
2100	.	.	3.01	3.75	68	10.6				
2135										
2200			3.10	3.78	69	10.8				
2230			3.04	3.70	69	10.8	140			
2300			3.00	3.76	69	10.5				
2330			3.04	3.76	68	10.5				
0030	▼	▼	3.05	3.78	69	10.5				
0100	14.7	70	3.05	3.74	69	10.7				

* Air - 14.7 psia, 70°F

SUIT FLOW SYSTEM
GEMINI EXTRAVEHICULAR SUIT
EXPERIMENT I^b

TEST DAY NO. 1 DATE: 11-5-64 to 11-6-64

* Air - 14.7 psia, 70°F

THERMAL DUMMY HEATER POWER
GEMINI EXTRAVEHICULAR SUIT TEST
EXPERIMENT Ib

TEST DAY NO. 1 DATE: 11-5-64 to 11-6-64

POWER-WATTS

TIME	VOLTS	TORSO	HEAD	LEFT ARM	RIGHT ARM	LEFT THIGH	RIGHT THIGH	LEFT LEG	RIGHT LEG	TOTAL	
0945	60	60	20	20	20	25	25	12	12	194	
1015	60	55	18	19	19	25	25	12	10	183	
1050	60	58	19	19	19	24	24	11	11	185	
1115	60	58	19	20	19	24	24	11	11	186	
1130	60	58	20	20	20	23	23	11	10	185	
1145	40	30	10	10	10	10	10	5	5	90	
1210	0	0	0	0	0	0	0	0	0	0	
1245	0	0	0	0	0	0	0	0	0	0	
1318	40	30	10	10	10	10	10	5	5	90	
1332	0	0	0	0	0	0	0	0	0	0	
1540	36	20	15	15	15	15	15	5	5	105	
1550	36	20	10	10	5	5	5	5	5	65	
	36	25	15	10	5	5	5	5	5	75	
1620	36	23	13	12	12	8	10	10	10	98	
1640	36	25	15	15	15	9	10	10	10	109	
1700	36	25	15	12	12	8	8	5	5	90	
1710	36	20	8	6	6	6	6	6	6	64	
1800	37	20	8	6	6	6	6	6	6	64	
1820	37	20	8	6	6	6	6	4	4	60	
1900	37	20	8	6	6	6	6	4	4	60	
2025	37	15	5	5	5	5	5	4	4	48	
2040	37	15	5	5	5	6	5	4	4	49	
2040	20	6	2	2	2	2	2	2	2	20	
2115	20	6	2	2	2	0	0	2	2	16	
0045	37	15	5	5	5	5	5	4	4	48	
0500		15	5	5	5	5	5	5	5	50	

TEST DAY NO. 2
HOOD OFF. TWO 20%
TRANSMITTANCE VISORS
INSTALLED. SUIT SUPPORTED
FROM TIEDOWN CABLE. PROTECTIVE
GLOVE ON RIGHT HAND.

TEST DAY NO. 2

TEST POINT NO. 1

COLD SOAK. DUMMY SURFACE

TEMPERATURE CONTROLLED WITH

DUMMY HEATERS.

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 1b

TEST DAY NO. 2

TEST POINT NO 1

DATE 9 Nov. 1964

TEMPERATURE °F

Chan. No.	TIME OF DAY									
	0630	0700	0730	0800	0830	0900	0930	0945	1000	
001	96	93	-	87	18	85	88	85	88	
2	86	88	85	69	83	74	83	89	87	
3	60	56	58	65	63	60	57	57	57	
4	60	58	61	66	65	61	60	60	60	
5	65	57	57	58	58	57	57	58	59	
6	74	74	78	84	79	78	81	84	85	
7										
8	70	70	101	81	75	74	76	79	80	
9	69	69	72	77	77	77	76	76	76	
10	70	71	78	85	79	77	75	76	76	
11	4	-10	-12	-8	-14	-18	-18	-18	-15	
12	65	71	84	95	70	72	77	83	83	
13	43	34	33	33	30	30	29	29	30	
14	74	75	80	87	82	80	84	87	87	
15	10	-15	-33	-45	-57	-66	-73	-76	-77	
16	14	-11	-28	-40	-51	-57	-64	-66	-68	
17	60	51	44	38	33	30	26	24	23	
18	69	70	77	84	79	78	76	76	76	
19	69	70	76	84	81	79	78	78	78	
20	65	62	62	65	65	65	65	65	65	
21	61	56	51	46	40	38	33	30	28	
22	51	46	42	39	37	34	31	30	29	
23	61	56	54	51	47	45	42	40	38	
24	61	57	54	51	48	45	42	40	39	
25	74	76	81	88	82	81	85	88	89	
26	71	71	76	82	77	76	78	81	82	

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 1b

TEST DAY NO. 2

TEST POINT NO 1

DATE 9 Nov. 1964

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 2

TEST POINT NO 1

DATE 20 Nov. 1964

TEMPERATURE °F

Chan. No.	TIME OF DAY									
	0630	0700	0730	0800	0830	0900	0930	0945	1000	
053										
54										
55										
56										
57	28	11	4	2	-1	-4	-6	-6	-5	
58										
59	56	47	45	46	43	40	40	42	42	
60										
61										
62	-46	-68	-78	-82	-87	-84	-85	-70	-90	
63	-21	-40	--49	-52	-56	-55	-57	-59	-60	
64	10	-5	-11	-13	-16	-17	-19	-20	-20	
65										
66										
67	53	38	34	33	33	30	30	29	30	
68	-73	-87	-92	-95	-96	-105	-106	-105	-105	
69	-39	-63	-73	-79	-85	-87	-90	-93	-94	
70	-63	-76	-78	-76	-76	-76	-77	-77	-79	
71	-73	-102	-117	-131	-143	-164	-170	-161	-164	
72	-52	-68	-77	-79	-81	-82	-83	-84	-84	
73	-31	-57	-77	-83	-90	-99	-105	-104	-105	
74	-149	-162	-167	-170	-173	-171	-173	-180	-180	
75	-170	-183	-191	-195	-196	-195	-196	-203	-204	
76	-144	-155	-160	-161	-160	-164	-167	-167	-168	
77	-121	-129	-130	-132	-132	-135	-136	-136	-135	
78	-123	-131	-134	-137	-138	-147	-149	-143	-143	

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 2

TEST POINT NO 1

DATE 20 Nov. 1964

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 2

TEST POINT NO

1

DATE 20 Nov. 1964

TEMPERATURE °F

TEST DAY NO. 2

TEST POINT NO. 2

COLD SOAK. DUMMY SURFACE

TEMPERATURE CONTROLLED

WITH INLET GAS.

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT IV

TEST DAY NO. 2

TEST POINT NO 2

DATE 11-9-64

TEMPERATURE °F

Chan. No.	TIME OF DAY									
	1015	1030	1045	1100	1115	1130	1145	1200	1215	
1	81	79	80	83	81	85	83	88	94	
2	75	71	78	65	80		84	81	80	
3	54	52	49	46	44	42	42	40	40	
4	54	54	51	48	46	44	43	42	42	
5	56	54	51	51	56	58	62	65	66	
6	84	74	69	68	70	71	74	74	74	
7										
8	79	69	63	59	57	56	56	56	56	
9	75	74	74	72	70	69	66	65	64	
10	74	71	69	66	65	62	60	58	57	
11	-16	-21	-28	-34	-38	-40	-41	-44	-44	
12	67	52	42	36	32	29	28	27	27	
13	28	24	20	20	19	20	21	23	23	
14	82	75	70	66	65	65	65	65	65	
15	-82	-85	-87	-89	-90	-93	-94	-95	-98	
16	-71	-73	-75	-76	-78	-79	-81	-82	-83	
17	22	20	17	16	14	12	10	9	9	
18	74	71	69	67	65	63	61	60	58	
19	75	74	71	70	69	67	66	65	65	
20	63	62	61	60	60	58	58	57	57	
21	24	23	20	18	18	15	14	11	10	
22	28	22	21	19	18	16	15	14	12	
23	39	35	33	33	30	28	26	24	23	
24	31	33	30	29	28	26	25	24	21	
25	83	75	70	67	66	67	69	69	69	
26	78	69	66	63	6;	6;	65	65	65	

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT I^b

TEST DAY NO. 2

TEST POINT NO 2

DATE 11-9-64

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT II

TEST DAY NO. 2

TEST POINT NO 2

DATE 11-9-64

TEMPERATURE °F

Chan. No.	TIME OF DAY									
	1015	1030	1045	1100	1115	1130	1145	1200	1215	
53										
54										
55'										
56										
57	-8	-9	-13	-14	-16	-18	-18	-18	-18	
58										
59	40	38	34	33	31	31	33	33	33	
60										
61										
62	-93	-95	-95	-95	-96	-98	-95	-94	-94	
63	-63	-63	-64	-65	-66	-65	-63	-61	-61	
64	-21	-23	-24	-25	-25	-25	-23	-25	-22	
65										
66										
67	30	28	26	25	25	25	28	28	29	
68	-105	-106	-108	-107	-110	-108	-111	-111	-113	
69	-95	-96	-99	-101	-102	-104	-104	-105	-106	
70	-79	-79	-81	-82	-82	-82	-84	-83	-83	
71	-166	-168	-170	-173	-174	-177	-186	-189	-190	
72	-183	-85	-86	-86	-87	-87	-85	-85	-85	
73	-106	-108	-108	-111	-112	-114	-117	-120	-121	
74	-181	-182	-182	-183	-186	-187	-182	-181	-181	
75	-206	-206	-209	-210	-212	-212	-205	-205	-203	
76	-168	-169	-170	-167	-170	-170	-176	-177	-176	
77	-136	-137	-138	-137	-141	-141	-142	-142	-142	
78	-144	-144	-148	-144	-149	-148	-151	-153	-153	

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Tb

TEST DAY NO. 2

TEST POINT NO 2

DATE 11-9-64

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT I^b

TEST DAY NO. 2

TEST POINT NO 2

DATE 11-9-64

TEMPERATURE °F

TEST DAY NO. 2

TEST POINT NO. 3

SOLAR SIMULATION ON
FRONT OF SUIT; EARTH
SIMULATION ON BACK.

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 2

TEST POINT NO. 3

DATE 11-20-64

TEMPERATURE °F

Chan. No.	TIME OF DAY										
	1545	1600	1615	1630	1700	1730	1800	1815	1830	1845	
1											
2		87				115	119				
3	40	42	49	57	72	75	75	75	75		
4	42	45	51	60	74	75	76	76	75	75	
5	67	68	72	80	95	97	95	93	92	91	
6	88	89	91	95	95	92	89	88	87	87	
7											
8	78	80	82	86	86	85	84	84	82	80	
9	56	57	60	63	69	71	74	74	75	75	
10	57	61	65	70	73	73	74	74	74	74	
11	-25	-21	-8	6	25	23	21	19	18	18	
12	70	72	75	79	71	65	65	63	62	62	
13	31	35	51	61	79	84	84	83	83	82	
14	83	85	87	89	88	85	84	83	82	82	
15	-112	-112	-94	-67	-20	2	18	25	29	34	
16	-93	-93	-86	-71	-39	-23	-13	-8	-6	-1	
17	-8	-8	-7	-5	4	13	23		30	34	
18	54	57	62	70	74	74	74	75	75	75	
19	58	61	66	71	77	77	76	75	75	75	
20	63	65	68	74	88	95	97	98	98	98	
21	-12	-13	-14	-14	-13	-13	-11	-10	-9	-10	
22	-8	-7	-4	-1	9	14	17	18	19	20	
23	-2	-4	-4	-3	-1	2	4	4	5	4	
24	2	2	2	2	7	9	12	14	14	15	
25	89	90	93	96	93	91	89	87	87	85	
26	82	83	86	89	88	87	85	83	83	82	
27	88	90	93	96	94	91	89	87	87	87	
28	74	75	78	82	85	83	82	82	80	79	
29	24	21	51	74	92	94	94	93	93	93	
30	65	71	78	85	85	81	79	79	78	78	

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 1b

TEST DAY NO. 2

TEST POINT NO. 3

DATE 11-20-64

TEMPERATURE °F

Chan. No.	TIME OF DAY									
	1545	1600	1615	1630	1700	1730	1800	1815	1830	1845
31	79	81	84	89	89	88	87	87	84	83
32	84	85	88	92	91	88	87	87	84	84
33	90	94	95	96	95	92	91	91	89	88
34	58	65	72	79	79	77	76	76	76	76
35	87	90	91	93	92	91	90	91	89	88
36	58	61	66	74	75	75	75	76	76	76
37	61	65	71	76	77	76	76	76	76	75
38	36	46	58	69	67	59	55	53	52	50
39	44	53	63	79	66	57	51	49	46	45
40	86	89	90	91	92	90	88	86	86	85
41	78	80	82	85	85	83	82	81	81	80
42	83	84	85	90	86	84	83	83	82	80
43	85	89	89	91	90	88	88	87	87	87
44	22	25	46	68	89	92	92	92	92	92
45	85	87	88	91	87	85	84	82	82	82
46	56	60	64	69	71	70	71	71	71	71
47	54	58	62	69	71	70	71	71	71	74
48	50	60	71	81	71	60	53	51	49	47
49	40	50	62	74	67	58	54	52	51	51
50										
51										
52										
53										
54										
55										
56										
57	-8		-8	23	46	51	52	52	51	48
58										
59	43	45	49	55	68	71	71	70	69	69
60										

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 2

TEST POINT NO. 3

DATE 11-20-64

TEMPERATURE °F

Chan. No.	TIME OF DAY									
	1545	1600	1615	1630	1700	1730	1800	1815	1830	1845
61										
62	-94	-77	-41	-2	29	33	33	30	29	25
63	-61	-52	-24	5	37	40	39	38	37	33
64	-19	-14	4	25	52	56	56	52	51	48
65										
66										
67	30	31	34	41	60	67	69	69	57	66
68	-105	1	133	147	159	162	161	162	162	162
69	-93	-69	-24	11	33	34	33	30	28	24
70	-89	-74	1	43	71	74	74	74	74	74
71	-139	078	5	25	37	35	33	28	25	21
72	-83	-60	72	121	148	152				152
73	-103	-89	-43	-12	16	19	18	16	14	1
74	-189	-106	-54	-26	-18	-19	-20	-21	-20	-23
75	-213	-146	-89	-65	-56	-56	-57	-60	-60	-61
76	-176	-6	101	108	109	104	100	100	101	100
77	-139	40	134	139	142	143	142	142	143	142
78	-141	27	167	177	180	180	178	178	178	
79	-166	-2	165	173	180	181	179	181	182	181
80	-162	-64	116	108	110	111	109	110	110	109
81	-118	50	119	171	178	180	180	182	182	181
82	-92	56	157	160	164	166	166	169	169	168
83	-177	81	158	163	167	168	166	169	169	166
84	-174	-57	4	26	33	33	34	34	33	32
85	-85	-149	-260	-270	-210	-162				
86	-147	-90	-27	15	26	23	21	18	14	10
87	-123	-79	-25	11	25	24	24	19	15	14
88	-126	-77	-6	10	16	13	11	5	1	-1
89	-119	-83	1	42	62	59	57	52	48	44
90	-132	78	-6	24	40	38	37	33	28	25

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 2

TEST POINT NO. 3

DATE 11-20-64

TEMPERATURE °F

Chan. No.	TIME OF DAY										
	1545	1600	1615	1630	1700	1730	1800	1815	1830	1845	
91	-141	-83	-1	16	27	25	24	19	15	11	
92	-127	-76	-6	23	34	31	29	24	20	18	
93	-134	-80	-7	13	24	21	19	15	11	9	
94	-33	-22	1	21	41	40	38	37	33	29	
95	71	74	77	81	88	89	88	88	87	87	
96	98	98	100	101	103	98	91	87	87	85	
97	-82	-3	81	103	97	89	87	74	65	60	
98	-81	-6	74	97	89	81	78	65	56	51	
99	-24	50	105	103	91	87	85	65	56	56	
100	-105	-50	24	54	68	66	65	57	52	48	
101	-99	-40	34	62	73	70	69	60	52	48	
102	-93	-25	68	98	107	103	101	91	85	82	
103											
104											
105											
106											
107											
108											
109	-294	-290	-288	-288	-288	-286	-290	-290	-288	-289	
110		-286	-287	-292	-298	-294	-297	-299	-299	-294	
111	-317	-317	-314	-316	-316	-315	-318	-319	-317	-318	
112	-320	-319	-316	-318	-319	-319	-319	-318	-319	-320	
113	-309	-306	-302	-305	-315	-308	-306	-308	-305	-308	
114	-312	-310	-309	-309	-309	-309	-310	-310	-312	-312	
115	79	81	85	89	88	87	85	84	82	81	
116	83	85	87	89	87	85	84	82	82	81	
117	93	95	97	98	91	99	102	101	101	101	
118	96	97	97	99	103		101	101	101	108	
119											
120	22	24	58	81	96	100	100	100	100	100	

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT I^b

TEST DAY NO. 2

TEST POINT NO. 3

DATE 11-20-64

TEMPERATURE °F

TEST DAY NO. 2

TEST POINT NO. 4

SOLAR SIMULATION ON BACK

OF SUIT; EARTH SIMULATION

ON FRONT.

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 2

TEST POINT NO. 4

DATE 11-20-64

TEMPERATURE °F

Chan. No.	TIME OF DAY										
	1845	1855	1900	1905	1910	1915	1930	1940	1950	2000	
1	114	114		118			117	115	119	114	
2		126	104	108	119	108	108		122		
3		75	74	74	74	74	73	74	73	73	
4	75	75	75	75	75	75	74	75	75	74	
5	91	91	91	89	88	87	83	82	81	79	
6	87	87	85	85	84	84	83	83	83	82	
7											
8	80	79	79	80	80	80	80	81	81	80	
9	75	75	75	76	75	76	75	76	77	77	
10	74	74	74	74	74	75	75	78	78	78	
11	18	24	34	42	51	53	60	63	65	66	
12	62	62	62	63	65	65	65	65	65	65	
13	82	82	78	76	74	73	69	66	66	64	
14	82	82	80	80	80	82	82	82	82	82	
15	34	37	37	34	33	30	24	23	21	20	
16	-1	-1	1	6	14	18	28	32	37	40	
17	34	38	37	38	39	42	43	42	44	44	
18	75	75	75	75	75	74	74	74	74	74	
19	75	75	74	74	74	73	73	74	74	74	
20	98	98	97	97	95	95	91	89	89	87	
21	-9	-9	-9	-8	-6	-6	-6	-6	-5	-4	
22	20	20	20	23	23	24	23	23	29	31	
23	4	5	5	5	5	4	4	4	4	4	
24	15	16	16	16	18	18	18	20	23	23	
25	85	84	83	84	83	83	82	82	82	81	
26	82	82	81	82	82	82	82	83	83	83	
27	87	85	84	84	83	83	82	82	82	82	
28	79	79	78	79	79	79	79	80	80	80	
29	93	91	87	81	74	71	65	62	61	61	
30	78	78	78	79	78	78	78	77	76	76	

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 1b

TEST DAY NO. 2

TEST POINT NO. 4

DATE 11-20-64

TEMPERATURE °F

Chan. No.	TIME OF DAY									
	1845	1855	1900	1905	1910	1915	1930	1940	1950	2000
31	83	83	82	82	82	82	79	79	78	78
32	84	83	82	83	82	82	82	80	80	79
33	88	88	88	88	88	89	89	87	89	87
34	76	75	75	75	75	75	74	75	75	74
35	88	88	88	88	88	88	88	88	88	88
36	76	78	78	76	75	75	75	76	75	75
37	75	78	75	75	74	74	74	75	76	76
38	50	50	50	50	50	50	50	48	48	49
39	45	45	45	44	45	44	41	43	43	45
40	85	85	103	85	85	86	86	85	85	86
41	70	77	77	77	77	77	77	77	77	77
42	80	80	79	79	79	79	79	79	79	79
43	87	87	87	87	87	87	87	87	88	87
44	92	91	87	82	72	74	65	61	60	58
45	82	80	80	80	79	82	82	81	82	81
46	71	71	71	71	71	74	74	74	78	74
47	74	74	74	74	74	74	74	74	75	75
48	47	46	47	46	46	46	46	46	46	46
49	51	51	49	51	51	51	51	52	51	51
50										
51										
52										
53										
54										
55										
56										
57	48	51	57	66	74	79	91	95	98	101
58										
59	69	69	69	71	71	70	87	88	91	93
60										

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 2

TEST POINT NO. 4

DATE 11-20-64

TEMPERATURE °F

Chan. No.	TIME OF DAY										
	1845	1855	1900	1905	1910	1915	1930	1940	1950	2000	
61											
62	25	60	78	88	96	100	108	111	113	115	
63	33	42	56	69	80	87	92	96	98	100	
64	48	53	65	78	87	91	100	102	104	106	
65											
66											
67	66	66	66	69	71	74	82	87	91	93	
68	161	78	60	48	42	37	33	31	33	33	
69	24	76	97	109	117	121	126	129	131	132	
70	74	70	61	53	46	42	39	39	39	40	
71	21	91	100	101	104	104	104	105	106	107	
72	152	135	113	94	78	70	60	56	56	56	
73	1	33	57	75	87	93	101	104	106	108	
74	-23	-85	-95	-98		-100	-100	-98	-95	-95	
75	-61	-77	-82	-83	-85	-85	-84	-85	-84	-83	
76	100	49	39	35	33	33	37	37	39	42	
77	142	47	34	29	29	28	33	33	37	38	
78	146	78	51	42	37	37	37	39	42	44	
79	181	75	56	47	43	42	42	44	46	48	
80	109	11	-1		-10	-10	-11	-11	-9	-1	
81	181	74	60	54	51	51	47	47	48	49	
82	168	100	83	76	74	70	69	69	69	70	
83	166	28	9	1	-1	-1	0	1	4	5	
84	33	9	9	7	9	9	9	10	11	11	
85	-83	-204				-206	-197	-189	-183	-179	
86	10	27	29	32	33	34	37	39	40	41	
87	14	121	134	139	142	143	146	146	146	147	
88	-1	82	88	91	92	92	95	95	95	96	
89	44	88	113	121	125	126	129	131	131	131	
90	25	70	78	82	83	83	87	87	87	88	

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 2

TEST POINT NO. 4

DATE 11-20-64

TEMPERATURE °F

Chan. No.	TIME OF DAY									
	1845	1855	1900	1905	1910	1915	1930	1940	1950	2000
91	11	106	113	114	117	117	118	118	118	119
92	18	33	38	40	42	42	43	44	45	46
93	9	138	146	149	150	150	153	153	154	154
94	29	51	58	65	70	74	80	83	84	85
95	87	87	87	87	85	87	83	83	83	82
96	85	87	87	88	88	91	91	90	89	87
97	60	65	69	68	74	77	85	89	95	98
98	51	51	51	51	56	60	66	72	78	81
99	56	51	46	52	62	65	69	74	80	82
100	48	46	46	44	46	46	51	54	57	60
101	48	51	51	51	56	56	62	69	70	74
102	82	87	91	92	97	100	108	113	117	118
103										
104										
105										
106										
107										
108										
109	-299	-288	-290	-287	-289	-289	-289	-289	-287	-288
110	-294	-299	-300	-296	-292	-292	-296	-292	-295	-298
111	-318	-320	-317	-318	-317	-319	-319	-318	-317	-317
112	-320	-320	-320	-320	-318	-320	-320	-320	-320	-320
113	-308	-309	-305	-307	-302	-302	-307	-302	-307	-313
114	-310	-308	-308	-310	-305	-308	-308	-308	-308	-316
115	81	82	81	81	79	79	78	77	77	76
116	81	80	80	80	82	82	81	82	82	82
117	101	102	104	102	100	104	99	100	102	102
118	108	102	101	104	100	100	100	105	101	104
119										
120	100	95	88	82	78	74	69	65	62	62

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Tb

TEST DAY NO. 2

TEST POINT NO. 4

DATE 11-20-64

TEMPERATURE °F

TEST DAY NO. 2
TEST POINT NO. 5
EARTH SIMULATION (ONLY)
ON FRONT OF SUIT.

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 2

TEST POINT NO. 5

DATE 9 November 1964

TEMPERATURE °F

Chan. No.	TIME OF DAY										
	2015	2020	2030	2100	2128	2137	2200	2230	2240	2245	2300
001	117	110				108	97	74	87		
2	108	111	106	91	104	91	85	90	96		
3	74	74	71	63	58	58	56	52	51	50	48
4	75	74	74	65	60	60	57	54	53	51	49
5	79	78	76	71	72	74	76	74	74	70	67
6	82	82	81	80	82	83	83	78	76	74	71
7											
8	81	80	78	74	71	70	70	65	65	62	60
9	78	78	78	76	74	74	71	69	69	67	65
10	78	78	78	75	71	69	66	63	62	61	60
11	67	52	30	+1	-11	-19	-30	-36	-36	-36	-38
12	65	65	62	53	46	44	39	38	37	37	35
13	63	61	56	42	37	38	42	39	38	37	35
14	82	82	82	79	78	77	75	71	70	68	65
15	20	20	14	-13	-31	-36	-39	-40	-41	-41	-41
16	44	45	37	5	-17	-21	-24	-14	-16	-18	-51
17	46	47	47	46	42	42	37	34	33	31	30
18	74	74	74	71	69	67	65	61	61	60	57
19	74	75	74	74	70	70	69	65	65	62	61
20	85	84	83	68	74	71	70	70	70	70	69
21	-3	-3	-3	-3	-3	-3	-4	-6	-6	-8	-8
22	33	33	29	25	23	20	15	10	9	9	6
23	5	5	4	4	1	0	-1	-2	-1	-1	-2
24	26	26	28	28	25	24	23	18	18	16	15
25	81	80	80	78	79	79	79	75	74	71	69
26	83	83	82	79	78	78	76	71	69	66	65

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 1b

TEST DAY NO. 2

TEST POINT NO. 5

DATE 9 November 1964

Chan. No.	TIME OF DAY						
	2310						
001	87						
2	92						
3	47						
4	48						
5	66						
6	70						
7							
8	58						
9	65						
10	58						
11	-39						
12	34						
13	34						
14	65						
15	-41						
16	-52						
17	28						
18	56						
19	60						
20	69						
21	-9						
22	4						
23	-3						
24	14						
25	69						
26	65						

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT II

TEST DAY NO. 2

TEST POINT NO. 5

DATE 9 November 1964

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 1b

TEST DAY NO. 2

TEST POINT NO. 5

DATE 9 November 1964

TEMPERATURE °F

Chan. No.	TIME OF DAY											
	2310											
027	69											
28	56											
29	28											
30	58											
31	60											
32	65											
33	75											
34	56											
35	75											
36	58											
37	61											
38	19											
39	24											
40	73											
41	58											
42	60											
43	74											
44	28											
45	65											
46	56											
47	56											
48	25											
49	18											
50												
51												
52												

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 1b

TEST DAY NO. 2

TEST POINT NO. 5

DATE 9 November 1964

TEMPERATURE °F

Chan. No.	TIME OF DAY										
	2015	2020	2030	2100	2128	2137	2200	2230	2240	2250	2300
053											
54											
55											
56											
57	104	100	78	46	30	25	10	-1	-3	-5	-9
58											
59	95	95	89	70	61	58	52	43	42	38	35
60											
61											
62	117	57	21	-21	-36	-59	-81	-93	-95	-97	-99
63	101	79	39	-1	-18	-29	-51	-63	-65	-68	-70
64	108	93	62	25	14	6	-10	-21	-23	-26	-29
65											
66											
67	96	96	91	74	60	56	49	39	37	33	28
68	30	-11	-40	-68	-76	-33	-11	-5	-5	-4	-4
69	134	61	24	-15	-26	-61	-81	-90	-92		-85
70	42	18	-20	-60	-71	-60	-47	-43	-43	-41	-41
71	108	18	-12	-60	-68	-154	-164	-174	-175	-176	-177
72	56	46	9	-43	-60	-47	-19	-7	-6	-5	-4
73	110	76	36	-19	-39	-57	-147	-101	-101	-106	-108
74	-95	-111	-135	-160	-162	-170	-170	-170	-170	-170	-169
75	-83	-119	-151	-183	-183	-196	-196	-195	-196	-195	-195
76	39	-72	-113	-143	-134	-60	-41	-34		-31	-31
77	35	-67	-101	-123	-108	-42	-25	-20	-18	-18	-19
78	42	-36	-93	-126	-119	-36	-10	-2	-1	0	-1

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 2

TEST POINT NO. 5

DATE 9 November 1964

TEMPERATURE °F

Chan. No.	TIME OF DAY							
	2310							
053								
54								
55								
56								
57	-10							
58								
59	34							
60								
61								
62	-101							
63	-71							
64	-39							
65								
66								
67	26							
68	-5							
69	-96							
70	-43							
71	-176							
72	-4							
73	-108							
74	-168							
75	-194							
76	-35							
77	-21							
78	-3							

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT II

TEST DAY NO. 2

TEST POINT NO 5

DATE 23 Nov. 1964

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Tb

TEST DAY NO. 2

TEST POINT NO 5

DATE 23 Nov. 1964

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT I^b

TEST DAY NO. 2

TEST POINT NO 5

DATE 23 Nov. 1964

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Tb

TEST DAY NO. 2

TEST POINT NO 5

DATE 23 Nov. 1964

TEMPERATURE °F

SUIT FLOW SYSTEM
GEMINI EXTRAVEHICULAR SUIT
EXPERIMENT 1b

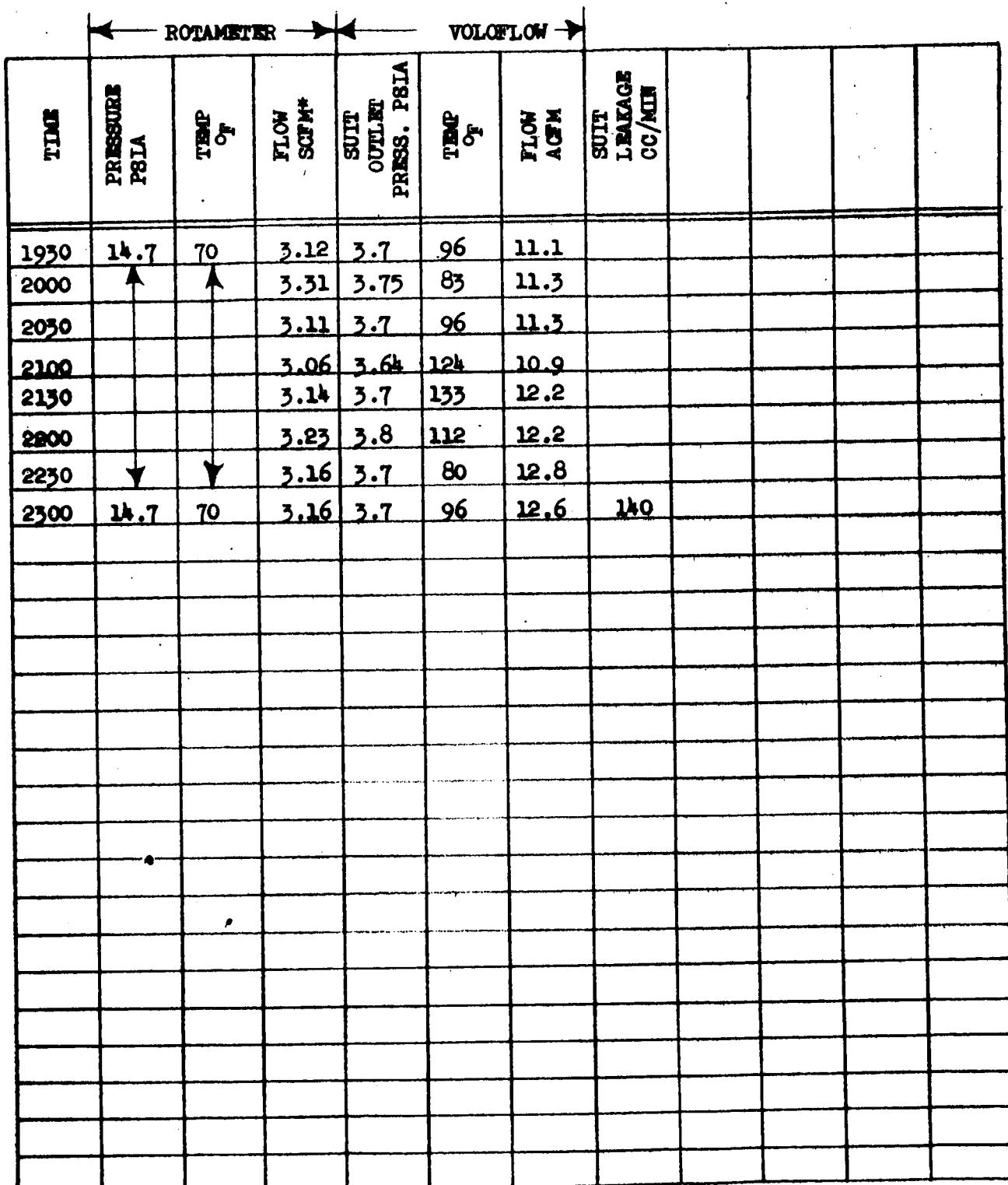
TEST DAY NO. 2 DATE: 11-9-64

TIME	ROTAMETER			VOLFLOW			SUIT LEAKAGE CC/MIN
	PRESSURE PSIA	TEMP OF	FLOW SCFM*	SUIT OUTLET PRESS. PSIA	TEMP OF	FLOW ACFM	
0630	14.7	70	3.21	3.7	75	11.7	
0700	↑	↑	-	3.8	75	11.75	
0730			-	3.7	75	11.6	
0800			-	3.7	75	11.5	
0830			-	3.65	77	11.45	
0900			-	3.7	77	11.45	
0930			-	3.7	77	11.4	
1000			-	3.7	77	11.4	160
1030		3.03	3.6	82		11.45	
1100		3.12	3.6	115		10.8	
1130		3.12	3.7	132		10.7	
1200		3.14	3.7	131		10.55	
1230		3.16	3.7	129		10.35	190
1300		3.21	3.7	129		10.75	
1330		3.03	3.7	130		10.75	
1400		3.03	3.7	131		10.75	
1430		2.98	3.7	131		10.75	
1500		3.03	3.7	131		10.75	
1530		3.02	3.7	130		10.75	
1600		3.02	3.7	131		10.75	
1630		3.02	3.7	130		10.75	
1700		3.07	3.7	115		11.0	
1730		3.07	3.7	92		11.2	
1800		3.03	3.7	79		11.45	
1830	▼	▼	3.02	3.7	78	11.45	
1900	14.7	70	3.06	3.7	100	11.10	

* Air - 14.7 psia, 70°^F

SUIT FLOW SYSTEM
GEMINI EXTRAVEHICULAR SUIT
EXPERIMENT Ib

TEST DAY NO. 2 DATE: 11-9-64



THERMAL DUMMY HEATER POWER
GEMINI EXTRAVEHICULAR SUIT TEST
EXPERIMENT Ib

TEST DAY NO. 2 DATE: 11-9-64

POWER-WATTS

TIME	VOLTS	TORSO	HEAD	LEFT ARM	RIGHT ARM	LEFT THIGH	RIGHT THIGH	LEFT LEG	RIGHT LEG	TOTAL	
0605	20	5	3.5	2	2	2	2	2	2	20.5	
0615	30	10	7	3	3	3	3	3	3	35	
0630	37	15	15	5	5	5	5	5	5	60	
0650	37	18	20	7	8	7	7	7	7	81	
0700	37	21	28	9	4	9	9	7	7	131	
0720	44	30	34	14	14	15	15	13	11	146	
0740	43	35	38	10	18	20	17	11	14	163	
0750	43	35	38	7	12	12	12	7	7	130	
0755	43	25	22	5	5	10	10	5	5	87	
0805	36	17.5	11	3	3	5	5	3	3	50.5	
0815	30	15	10	2	2	2	2	2	2	37	
0820	30	15	13	2	2	2	2	2	2	40	
0830	30	15	15	2	3	2	2	2	2	43	
0845	34	17	22	3.5	4	3	3	2.5	2.5	57.5	
0850	34	20	22	5	5	3	3	2.5	2.5	63	
0900	34	25	22	5	5	3	3	4	4	71	
0920	34	30	22	5	5	3	3	4	4	71	
0925	40	35	30	6	6	4	4	5.5	5	95.5	
0935	40	30	30	6	6	4	4	5.5	5	90.5	
0945	40	30	25	6	6	4	5	5.5	5	86.5	
1000	40	30	25	6	6	4	6	5.5	5	87.5	
1010	0	0	0	0	0	0	0	0	0	0	
1115	30	30	25	6	6	4	6	5.5	5	87.5	
1125	40	40	32.5	9	8.5	6	9	7.5	7	119.5	
1145	36	40	32.5	9	8.5	6	9	7.5	7	119.5	
1155											

**Thermal Dummy Heater Power
Gemini Extravehicular Suit Test
Experiment 1B**

TEST DAY NO. 2 DATE: 11-9-64

POWER-WATTS

TEST DAY NO. 3
SIMULATED SPACECRAFT
SURFACE INSTALLED. SUIT
SUPPORTED BY HELMET WITH
CLEAR VISOR EXPOSED. PROTECTIVE
GLOVE COVER (MITTEN) ON
RIGHT HAND. SUPER INSULATION
ADDED TO BOTTOM OF LEFT FOOT.

TEST DAY NO. 3

TEST POINT NO. 1

SOLAR SIMULATION ON;

EARTH SIMULATION ON.

SUIT ROTATED TO ACHIEVE

AN AVERAGE SUIT SURFACE TEMPERATURE

OF $75 \pm 15^{\circ}\text{F}$. DUMMY

SURFACE TEMPERATURE CONTROLLED

WITH DUMMY HEATERS.

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT IV

TEST DAY NO. 3

TEST POINT NO 1

DATE 11-12-64

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 3

TEST POINT NO 1

DATE 11-12-64

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT I^b

TEST DAY NO. 3

TEST POINT NO 1

DATE 11-12-64

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 3

TEST POINT NO 1

DATE 11-12-64

TEMPERATURE °F

Chan. No.	TIME OF DAY							
	0800	0815	0830	0845	0900	0915	0925	
79	-10	7	51	23	31	65	51	
80	-10	10	53	47	42	60	53	
81	-6	104	92	108	30	56		
82	20	43	87	78	74	67	91	
83	-52	113	105	110	28	38	69	
84	-4	100	98		56	65	100	
85	113	134	56	44	-4	-21	4	
86	28	-10	71	65	71	108	113	
87	19	-3	70	60	70	104	101	
88	31	-16	42	43	80	100	75	
89	34	5	76	69	60	108	101	
90	18	-13	47	47	56	98	80	
91	14	-14	56	51	77	115	88	
92	18	-13	70	60	82	158	127	
93	19	-6	74	60	74		130	
94	69	56	57	60	60	65	65	
95	71	71	74	78	82	84	87	
96	74	74	74	74	75	76	78	
97	56	23	80	117	117	113	113	
98	56	18	69	113	111	104	104	
99	37	12	104	121	113	110	109	
100	53	18	52	87	92	93	92	
101	56	20	49	84	87	87	85	
102	56	33		114	119	118	117	
103	46	41	41	44	46	46	48	
104	46	41	44	46	49	49	50	

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT I^b

TEST DAY NO. 3

TEST POINT NO 1

DATE 11-12-64

TEMPERATURE °F

TEST DAY NO. 3

TEST POINT NO. 2

SOLAR SIMULATION ON
FRONT OF SUIT; EARTH
SIMULATION ON BACK.

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 3

TEST POINT NO 2

DATE 28 Nov. 1964

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Th

TEST DAY NO. 3

TEST POINT NO 2

DATE 28 Nov. 1964

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT II

TEST DAY NO. 3

TEST POINT NO 2

DATE 28 Nov. 1964

TEMPERATURE °F

Chan. No.	TIME OF DAY									
	0935	0940	0950	1000	1015	1020	1030	1040	1050	1100
053										
54										
55	129	140	141	144	148	150		-60	-75	-79
56										
57	78		71	69	65	65	61	60	56	53
58										
59	84	83	82	79	78	76	75	74	74	72
60										
61										
62	54	38	25	20	16	15	5	-9	-19	-24
63	65	46	33	29	25	25	21	12	0	-5
64	78	66	56	52	51	51	49	42	34	31
65										
66										
67	80	79	75	74	71	71	71	70	69	69
68	108	129	145	148	142	140	121	62	28	9
69	62	56	48	43	38	37	33	24	16	14
70	65	51	45	51	61	63	44	15	-9	-21
71	65	60	56	52	49	49	28	9	-1	-1
72	92	106	120	127	47	135	35	65	19	-1
73	61	61	60	58	56	56	56	51	45	39
74	25	-30	34	-14	-10	-15	-51	-67	-73	-73
75	4	4	2	37	43	28	-25	-47	-57	-57
76	134	142	146	146		143	0	-62	-85	-96
77	128	136	138	142	144	142	-6	-66	-84	-89
78	140	146	139	136	134	134	42	-53	-90	-101

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 16

TEST DAY NO. 3

TEST POINT NO 2

DATE 28 Nov. 1964

TEMPERATURE °F

Chan. No.	TIME OF DAY										
	0935	0940	0950	1000	1015	1020	1030	1040	1050	1100	
079	144	131	125	121	119	119	29	-54	-87	-101	
80	136	143	146	147	148	148	-19	-95	-119	-129	
81	82	51	56	70	78	79	20	-29	-50	-57	
82	102	92	87	82	78	78	104	44	18	5	
83	125	117	117	118	117	118	-15	-90	-111	-118	
84	108	115	118	115	115	114	51	-16	-47	-57	
85	10	14	14	14	14	14	31	47	47	35	
86	1	-8	-11	-13	-15	-16	-35	-56	-67	-68	
87	16	9	4	-1	-1	-1	-21	9	-52	-54	
88	57	54	51	49	46	46	28	10	4	4	
89	65	60	56	54	52	51	-31	9	-1	12	
90	37	33	28	25	23	21	2	-18	-26	-28	
91	45	39	36	34	33	31	9	-11	-20	-19	
92	39	33	28	25	23	22	2	-18	-28	-26	
93	51	44	40	39	37	35	14	-6	-15	-15	
94	65	65	62	61	60	60	58	56	51	48	
95	88	88	88	89	91	92	93	93	91	91	
96	78	80	87	93	100	100	100	102	106	110	
97	108	105	101	98	95	95	84	63	67	76	
98	98	95	89	87	85	85	82	66	69	78	
99	104	100	98	97	85	96	85	65	91	78	
100	88	85	82	80	77	76	70	54	47	48	
101	82	80	76	74	70	69	65	51	51	53	
102	110	108	104	101	96	95	84	62	60	61	
103	49	50	50	53	55	56	55	74	73	77	
104	50	50	52	54	55	58	58	76	73	77	

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 3

TEST POINT NO 2

DATE 28 Nov. 1964

TEMPERATURE °F

Chan. No.	TIME OF DAY									
	0935	0940	0950	1000	1015	1020	1030	1040	1050	1100
105										
106										
107										
108										
109										
110										
111										
112										
113										
114										
115	92	91	89	89	89	90	90	89	86	84
116	93	91	89	88	88	88	89	89	93	89
117	93	93	93	93	93	93	93	93	93	93
118	93	93	93	93	93	93	93	93	93	92
119										
120	83	87	87	87	87	87	44	24	14	10
121	78	79	82	87	95	97	91	101	104	104
122	87	88	89	91	92	93	95	95	93	92
123	62	52	48	46	43	42	20	0	-10	-
124	166	174	176	174	177	174	-9	-78	-	-105
125	125	132	136	144	147	146	0	-55	-77	-85
126	85	80	-	74	70	71	43	22	14	14
127	73	73	77	86	91	95	97	101	105	108
128	82	82	82	82	85	90	90	92	91	90
129										
130										

TEST DAY NO. 3

TEST POINT NO. 3

SOLAR SIMULATION ON

FRONT OF SUIT; EARTH SIMULATION
ON BACK; SPACECRAFT SIMULATION

ON RIGHT SIDE.

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 3

TEST POINT NO. 3

DATE 11-12-64

TEMPERATURE °F

Chan. No.	TIME OF DAY										
	1100	1130	1200	1230	1245	1300	1315	1330			
1		87	-65					-5			
2	69	76	79	78	78	78	79	79			
3	87	85	87	87	87	87	88	88			
4	87	87	87	87	87	88	88	88			
5	87	91	95	95	95	95	95	91			
6	88	91	91	91	89	89	89	91			
7											
8	88	87	87	87	87	85	85	87			
9	83	83	83	84	85	85	85	87			
10	83	82	83	84	84	85	85	85			
11	69	81	82	82	81	81	82	83			
12	65	42	69	71	72	74	73	75			
13	65	89	93	95	94	95	95	95			
14	90	89	88	87	87	87	87	87			
15	65	65	69	74	75	76	77	79			
16	65	65	69	71	74	74	75	76			
17	74	74	75	78	78	79	80	81			
18	83	84	85	87	87	87	87	88			
19	83	83	84	85	85	85	85	85			
20	95	94	100	102	104	104	104	105			
21	56	54	52	51	51	51	51	50			
22	60	60	60	60	60	60	60	60			
23	65	65	63	65	65	63	65	66			
24	61	60	58	57	57	57	56	56			
25	88	90	91	89	89	89	89	90			
26	91	90	88	87	87	87	87	87			
27	89	91	91	91	89	89	90	90			
28	87	87	87	87	87	87	87	87			
29	33	83	87	86	88	89	89	90			
30	87	87	87	87	88	88	88	88			

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 3

TEST POINT NO. 3

DATE 11-12-64

TEMPERATURE °F

Chan. No.	TIME OF DAY							
	1100	1130	1200	1230	1245	1300	1315	1330
31	87	86	89	89	86	89	89	89
32	87	86	89	89	86	88	89	89
33	92	91	91	91	91	91	91	91
34	87	85	91	87	87	87	88	88
35	91	91	91	91	91	91	92	92
36	84	84	85	87	87	87	87	88
37	83	85	85	87	85	85	87	87
38	82	77	77	79	80	80	80	81
39	80	75	75	75	75	74	74	75
40	91	90	90		240	240	323	90
41	86	85	86	86	86	86	86	86
42	87	87	87	87	87	87	87	87
43	106	87	88	88	89	89	89	89
44	51	104	107	108	108	108	104	107
45								
46	79						82	81
47	83	80	81	82	82	83	83	84
48	78	74	74	74	74	74	74	73
49	80	76	75	76	76	77	76	76
50								
51								
52								
53								
54								
55	-6	150	153	151	152	152	152	
56								
57	52	51	51	52	52	52	52	52
58								
59	71	69	69	69	69	69	69	69
60								

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 1b

TEST DAY NO. 3

TEST POINT NO. 3

DATE 11-12-64

TEMPERATURE °F

Chan. No.	TIME OF DAY							
	1100	1130	1200	1230	1245	1300	1315	1330
61								
62	-21	10	14	14	14	12	12	14
63	-5	19	22	21	21	20	20	22
64	31	47	49	47	46	46	45	47
65								
66								
67	67	69	69	67				66
68	25	154	161	160	161	161	160	160
69	12	20	23	23	23	21	20	20
70	-20	44	51	51	51	51	62	56
71	9	53	54	52	51	50	51	53
72	-4	127	134	134	134	134	136	134
73	39	43	48	46	51	51	52	52
74	-66	-29	-29	-30	-31	-33	-5	-29
75	-46	7	9	5	4	4	44	7
76	36	153	156	154	154	154	158	154
77	33	140	143	140	142	142	143	142
78	4	162	166	165	165	165	165	165
79	31	178	182	180	181	181	181	181
80	21	146	150	147	148	148	148	148
81	-38	65	69	69	69	69	88	70
82	165	88	95	95	74	72	72	72
83	76	180	184	180	181	181	181	181
84		111	113	113	113	113	113	113
85	19	-46	-41	-34	-28	-25	-137	-25
86	-57	-15	-15	-16	-18	-18	-17	-16
87	-44	-3	-1	-3	-4	-4	-3	-1
88	15	51	50	48	46	46	48	49
89	12	56	56	56	52	52	53	56
90	-17	23	24	23	21	21	22	23

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 3

TEST POINT NO 3

DATE 11-12-64

TEMPERATURE °F

Chan. No.	TIME OF DAY									
	1100	1130	1200	1230	1245	1300	1315	1330		
91	-6	34	34	33	33	31	33	33		
92	-16	24	24	23	22	21	23	24		
93	-3	37	37	35	34	34	36	37		
94	48	51	53	56	56	57	57	58		
95	91	91	92	92	92	92	92	93		
96	110	98	89	84	84	87	88	89		
97	78	109	104	101	98	97	102	104		
98	76	98	91	89	87	85	91	92		
99	79	106	100	98	95	95	106	101		
100	48	79	79	78	76	75	78	79		
101	49	78	75	74	71	69	74	74		
102	66	108	106	104	101	100	103	104		
103	84	201			169			180		
104	83	203	190	175	168	163	184	181		
105										
106										
107										
108										
109	-99	-99	-99	-98	-99	-99	-96	-96		
110	-101	-106	-108	-106	-108	-106	-103	-104		
111	-111	-112	-112	-112	-114	-112	-111	-111		
112	-111	-112	-112	-112	-112	-111	-109	-109		
113	-110	-111	-111	-111	-111	-110	-107	-108		
114	-106	-108	-108	-109	-108	-109	-107	-108		
115	84	86	87	87	87	87	87	88		
116	89	88	88	87	87	87	87	87		
117	93	92	93	93	93	93	93	95		
118	93	92	93	93	93	93	94	95		
119										
120	48	82	87	87	87	87	88	88		

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Γβ

TEST DAY NO. 3

TEST POINT NO 3

DATE 11-12-64

TEMPERATURE °F

TEST DAY NO. 3
TEST POINT NO. 4
SOLAR SIMULATION
ON FRONT OF SUIT; EARTH
SIMULATION ON BACK.
ROTATED SIMULATED HOT
SPACECRAFT SURFACE AGAINST
RIGHT SIDE OF SUIT.

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT I^b

TEST DAY NO. 3

TEST POINT NO 4

DATE 11-12-64

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT I_b

TEST DAY NO. 3

TEST POINT NO 4

DATE 11-12-64

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 1b

TEST DAY NO. 3

TEST POINT NO 4

DATE 11-12-64

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 10

TEST DAY NO. 3

TEST POINT NO 4

DATE 11-12-64

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 3

TEST POINT NO 4

DATE 11-12-64

TEMPERATURE °F

Chan. No.	TIME OF DAY						
	1330	1415	1430	1445	1500	1515	1530
105							
106							
107							
108							
109	-292	-296	-297	-297	-298	-297	-299
110	-306	-309	-309	-309	-309	-309	-309
111	-320						
112	-315	-320	-320				
113	-313	-316	-316	-316	-316	-316	-316
114	-313	-316	-316	-315	-315	-313	-316
115	88	87	86	85	85	85	84
116	87	87	87	87	87	86	85
117	95	95	94	94	94	94	94
118	95	95	94	94	94	94	94
119							
120	88	37	37	37	37	37	36
121	94	92	90	88	86	85	85
122	95	95	92	91	90	89	88
123	42	42	42	42	42	42	41
124	60	140	140	142	148	139	139
125	146	95	95	98	97	94	93
126	75	161	161	161	163	162	161
127	91	86	85	84	84	83	83
128	92	91	89	88	87	86	86
129							
130							

TEST DAY NO. 3

TEST POINT NO. 5

SIMULATED ORBIT. SOLAR

SIMULATION ON FOR 60

MINUTES; OFF FOR 30 MINUTES.

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT I_b

TEST DAY NO. 3

TEST POINT NO 5

DATE 11-12-64

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 3

TEST POINT NO 5

DATE 11-12-64

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 1b

TEST DAY NO. 3

TEST POINT NO 5

DATE 11-12-64

TEMPERATURE °F

Chan. No.	TIME OF DAY										
	1530	1545	1550	1555	1600	1605	1610	1615	1620	1625	1630
27	85	85	85	85	87	87	85	85	85	86	87
28	87	87	87	87	87	87	87	87	87	87	87
29	63	63	81	76	74	70	66	75	80	80	58
30		93	92	92	92	92	92	92	92	91	91
31	86	85	86	87	87	87	85	85	85	85	85
32	84	84	85	85	85	85	84	84	85	85	85
33	85	93	85	85	85	85	85	85	85	85	85
34	93	93	92	92	92	92	92	92	92	91	91
35	85	85	85	85	85	85	85	85	85	85	87
36	87	86	87	87	87	87	87	87	87	87	87
37	82	81	81	82	82	81	82	82	82	82	87
38	79	79	79	79	78	77	79	78	77	77	79
39	71	70	61	70	69	70	70	70	73	71	71
40	85	84	84	84	83	84	84	84	84	84	85
41	86	85	85	85	85	82	84	84	85	84	84
42	87	85	85	85	85	85	85	85	85	85	85
43	85	84	84	84	84	84	84	84	85	85	85
44	65	69	74	75	75	76	65	75	88	91	69
45											
46	80						80				
47	85	85	85	85	85	85	85	87	87	85	85
48	70	70	69	69	70	70	70	71	71	71	71
49	78	78	78	78	78	78	78	79	78	78	78
50											
51											
52											

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 16

TEST DAY NO. 3

TEST POINT NO 5

DATE 11-12-64

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 3

TEST POINT NO5

DATE 11-12-64

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 10

TEST DAY NO. 3

TEST POINT NO 5

DATE 11-12-64

TEMPERATURE °F

Chan. No.	TIME OF DAY									
	1635	1640	1656	1650	1655	1700	1705	1710	1715	
53										
54										
55	24	143	147	26	24	22	95	51	134	
56										
57	86	88	87	83	79	74	68	63	62	
58										
59	84	87	87	87	85	83	80	77	75	
60										
61										
62	129	54	43	14	-3	-23	-38	-13	-16	
63	104	78	68	40	24	-23	-13	-5	-1	
64	105	94	85	63	51	33	22	20	22	
65										
66										
67	89	91	-95	83	85	88	76	72	69	
68	38	53	110	78	56	38	29	12	22	
69	106	85	78	58	52	38	29	26	27	
70	51	100	105	92	40	10	29	-6	-5	
71	142	-72	-70	-94	-59	-69	-120	-77	-65	
72	69	79	99	77	58	25	18	7	1	
73	80	85	83	74	68	61	51	42	39	
74	31	-15	-25	-59	-15	-10	-30	-76	-86	
75	68	-15	-19	-56	-5	-1	-38	-77	-90	
76	-31	139	144	-35	-53	-53	-26	-95	-99	
77	-54	137	142	-43	-51	-53	-32	-99	-95	
78	-54	144	158	11	-29	-59	-60	-79	-77	

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Tb

TEST DAY NO. 3

TEST POINT NO 5

DATE 11-12-64

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT I^b

TEST DAY NO. 3

TEST POINT NO 5

DATE 11-12-64

TEMPERATURE °F

Chan. No.	TIME OF DAY									
	1635	1640	1645	1650	1655	1700	1705	1710	1715	
79	-55	165	175	11	-22	-52	-52	-70	-62	
80	-69		156	9	-33	-57	-51	-59	-44	
81	7	123	134	-5	-28	-31	5	-51		
82	38	175	180	60	37	20	17	0	4	
83	-61	172	176	-59	-90	-93	-54	-122		
84	-33	91	100	15	-33	-71	-72	-61	-37	
85	-203	45	60	80	44	55	91	63		
86	137	-7	-18	-56	-90	-111	-119	-40	-48	
87	136	-1	-13	-48	-76	-95	-106	-47	-52	
88	127	-47	-59	-73	-40	-53	-93	-77	-71	
89	139	-36	-53	-92	-92	-101	-124	-92	-92	
90	128	-49	-63	-96	-88	-103	-137	-93	-93	
91	156	-56	-72	-97	-59	-75	-127	-76	-71	
92	181	49	-66	-101	-90	-105	-137	-87	-87	
93	176	-47	-65	-94	-68	-81	-124	-71	-67	
94	84	75	73	67	64	59	54	50	49	
95	88	87	87	87	87	87	86	82	81	
96	86	85	85	85	85	84	83	83	84	
97	74	72	72	67	67	64	65	66	68	
98	69	69	69	67	66	65	67	67	69	
99	75	62	83	71	79	71	73	70	71	
100	56	52	52	47	44	41	39		38	
101	63	57	56	51	48	46	46	45	47	
102	77	71	69	62	59	56	56	55	58	
103	314		165	159	155	150	144	143	147	
104	160	161	160	155	151	145	139	138	131	

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 16

TEST DAY NO. 3

TEST POINT NO 5

DATE 11-12-64

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT I^b

TEST DAY NO. 3

TEST POINT NO 5

DATE 11-12-64

TEMPERATURE °F

TEST DAY NO. 3

TEST POINT NO. 6

SIMULATED ORBIT. SOLAR

SIMULATION ON FOR 60

MINUTES; OFF FOR 30 MINUTES.

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT II

TEST DAY NO. 3

TEST POINT NO 6

DATE 30 Nov. 1964

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Tb

TEST DAY NO. 3

TEST POINT NO 6

DATE 30 Nov. 1964

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 3

TEST POINT NO 6

DATE 30 Nov. 1964

TEMPERATURE °F

Chan. No.	TIME OF DAY										
	1715	1720	1725	1730	1735	1740	1745	1750	1755	1800	1805
027	78	75	74	74	74	74	74	77	78	78	78
28	84	82	81	78	78	77	77	77	78	77	78
29	36	56	56	54	51	67	73	60	53	46	40
30	88	88	87	87	68	85	85	85	84	84	84
31	72	65	65	65	66	69	70	74	74	74	74
32	68	65	62	61	61	65	66	71	72	74	74
33	85	85	85	84	84	84	84	84	84	85	85
34	89	88	88	87	87	87	85	85	85	85	84
35	87	85	85	85	85	85	85	85	85	85	87
36	85	83	82	82	82	82	82	82	82	83	82
37	78	77	76	74	74	74	75	77	78	78	78
38	75	73	73	72	72	71	72	73	73	73	73
39	69	67	66	64	63	62	62	61	61	61	60
40	85	84	84	84	83	83	83	84	84	84	84
41	81	79	77	76	75	74	75	75	75	75	76
42	83	82	80	79	78	77	76	76	76	76	76
43	85	84	84	84	84	84	84	85	85	85	85
44	58	70	67	65	60	76	86	79	72	65	60
45											
46		79	79	78	78	78	78			78	78
47	82	81	81	81	81	81	81	80	80	80	81
48	69	69	67	66	65	65	65	62	62	61	61
49	74	73	72	72	73	73	73	71	71	70	72
50											
51											
52											

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 3

TEST POINT NO 6

DATE 30 Nov. 1964

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 1b

TEST DAY NO. 3

TEST POINT NO 6

DATE 30 Nov. 1964

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 3 TEST POINT NO 6

DATE 30 Nov. 1964

TEMPERATURE °F

Chan. No.	TIME OF DAY								
	1810	1815	1820	1825	1830	1835	1840	1845	
053									
54									
55	118	64	110	122	100	90	62	44	
56									
57	82	81	79	74	70	66	63	60	
58									
59	78	81	81	80	79	78	76	73	
60									
61									
62	82	47	31	-6		-31	-261*	14	
63	97	67	52	-22	4	-7	-9	15	
64	102	81	68	48	36	26	21	29	
65									
66									
67	85	87	85	83	81	78	74	70	
68	72	79	56	34	25	19	-228*	-1	
69	91	70	60	42	33	25	30	33	
70	55	39	22	7	10	19	7	-13	
71	-17	-82	-94	-67	-109	-132	-84	-73	
72	56	78	56	29	18	16	12	-6	
73	66	65	60	52	47	41	34	26	
74	-65	-70	0	-29	-35	-68	-72		
75	-17	-55	-64	9	-26	-35	-53	-62	
76	123	-14	-57	-72	-36	-26	-78	-106	
77	117	-13	-58	-62	-28	-19	-71	-95	
78	102	31	-23	-61	-62	-62	-85	-105	

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Ib

TEST DAY NO. 3

TEST POINT NO 6

DATE 30 Nov. 1964

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT 1b

TEST DAY NO. 3

TEST POINT NO 6

DATE 30 Nov. 1964

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT I^b

TEST DAY NO. 3

TEST POINT NO 6

DATE 30 Nov. 1964

TEMPERATURE °F

GEMINI EXTRAVEHICULAR SUIT TEST

EXPERIMENT Tb

TEST DAY NO. 3

TEST POINT NO 6

DATE 30 Nov. 1964

TEMPERATURE °F

SUIT FLOW SYSTEM
GEMINI EXTRAVEHICULAR SUIT
EXPERIMENT I^b

TEST DAY NO. 3 DATE: 11-12-64

**THERMAL DUMMY HEATER POWER
GEMINI EXTRAVEHICULAR SUIT TEST
EXPERIMENT 1b**

TEST DAY NO. 3 DATE: 11-12-64

POWER-WATTS

APPENDIX B

INSTRUMENTATION ACCURACIES

APPENDIX B
INSTRUMENTATION MEASUREMENT ACCURACIES

I. Thermocouple Temperature Measurements.

Experiment I-b specimen temperatures were measured by forty gauge copper-constantan thermocouples. Paragraph 3.4.1 describes the thermocouple attachments and signal recording methods.

Sources of error in temperature measurements on Experiment I-b arise from:

- (a) Thermocouple errors due to copper and constantan wire impurities.
- (b) Reference junction temperature errors.
- (c) Recorder errors.
- (d) Millivolt-temperature conversion errors.
- (e) Differences in junction temperatures and the temperature of the materials to which the thermocouples were attached.

The accuracy of the thermocouple wire (used for this test) is stated by the manufacturer to be $\pm 1\frac{1}{2}^{\circ}\text{F}$ in the temperature range between -75°F and $+200^{\circ}\text{F}$. At $+200^{\circ}\text{F}$, a copper-constantan thermocouple has a thermo-electric power of 26 microvolts/ $^{\circ}\text{F}$. Since the thermoelectric power decreases with temperature, the maximum error in this range will be at $+200^{\circ}\text{F}$ and is equal to 39 microvolts. This is the voltage error contributed by the thermocouple wire in this temperature range.

The manufacturer of the 150°F reference junction used (Pace model ERJRL3A-48TP) specifies the following tolerances for the junction: $\pm 0.1^{\circ}\text{F}$ accuracy, $\pm 0.1^{\circ}\text{F}$ stability, $\pm 0.1^{\circ}\text{F}$ uniformity (between multipoint junctions), and $\pm 0.25^{\circ}\text{F}$ stability in ambient temperatures of -30°F to $+120^{\circ}\text{F}$. On the basis of 26 microvolts/ $^{\circ}\text{F}$ for thermoelectric power, the total RMS error of the reference junction can be calculated to be:

$$\sqrt{(2.6)^2 + (2.6)^2 + (2.6)^2 + (6.5)^2} = 7.9 \text{ microvolts}$$

The Cubic Corporation specifies the following accuracies for the model A-85 A-C pre-amplifier used in the recording system:

- Gain accuracy can be set to $\pm 0.01\%$
- Gain stability is $\pm 0.1\%$.
- Noise level: ± 2 microvolts referred to input.

- Drift: ± 2 microvolts per 500 hours of operation at constant ambient temperature, referred to input.

The voltage error of the pre-amplifier due to the noise level and drift voltages is $\sqrt{8}$ microvolts. The voltage error contributed by the gain accuracy and stability and the basic digital voltmeter accuracy of .01% can be shown to be negligible in the RMS summing procedure. These errors are made further insignificant due to the digital voltmeter resolution of ± 1 digit. Since the last digit read on the meter was in units of 0.01 volts, this results in an error at least 10 times larger than the instrument basic accuracy. Thus the instrument resolution error is 0.01 volts divided by the gain factor of 1,000 which results in an error of 10 microvolts.

An additional error of approximately $\pm 0.5^{\circ}\text{F}$ or 13 microvolts was incurred as a result of reading the standard temperature conversion charts to the nearest degree.

It can be seen that the significant errors of the thermocouple wire and recording system and their magnitudes are as follows:

Thermocouple Wire	± 39 microvolts
Reference Junction	± 7.9 microvolts
Voltmeter Pre-amplifier	$\pm \sqrt{8}$ microvolts
Digital Voltmeter	± 10 microvolts
Millivolt-temperature Conversion Table Interpolation	± 13 microvolts

The total RMS sum of these errors is 43.2 microvolts which corresponds to the following temperature errors (exclusive of thermocouple attachment errors):

$\pm 1.7^{\circ}\text{F}$ in range of -75° to $+200^{\circ}\text{F}$

$\pm 3.1^{\circ}\text{F}$ in range of -150° to -75°F

Thermocouple attachment techniques are a potential source of error. The thermocouples must be attached such that the junction temperature is the same as the temperature of the material to which they are attached. Thus, it is heat transfer considerations that result in thermocouple junction temperature errors, and therefore, signal errors. Forty gauge thermocouple wire (0.003 in. diameter) and the attachment precautions described in paragraph 3.6.1 were used during Experiment I-b to reduce temperature measurement errors attributable to thermocouple mounting techniques.

The thermocouples on the HT-1 outside surface of the suit and those on the NRC-2 insulation are most subject to attachment errors. The thermocouples on the HT-1 fabric are subject to error for the following reasons:

- (a) The emissive properties of the painted thermocouple do not match those of the HT-1. Because the thermocouple absorbs and emits at a different rate, there is a tendency for the junction temperature to be higher or lower than that of the HT-1.
- (b) The lateral conductance of the HT-1 fabric is relatively low. The low thermal conductance of the HT-1 aids in permitting incident radiation (e.g. simulated solar radiation) to perturb the junction temperature as discussed above.

While tests were not performed to evaluate the accuracy of suit surface thermocouples during Experiment I-b, it is believed that no gross errors were incurred by the effects discussed above. The discussion of paragraph 4.2.1 shows that measured suit surface temperatures were approximately as expected (on the basis of test solar and albedo flux calibration). Also, undocumented results of a comparative evaluation of similar thermocouple attachments performed during contract NAS 9-1163 indicated that the attachment techniques employed during Experiment I-b do not result in large errors under simulated solar irradiation. The same comparative evaluation also revealed that attachment errors were probably nil during suit cold soak tests.

II. Suit Pressure Measurement Accuracies.

The suit inlet gas pressure, helmet pressure, and the pressure drop across the suit (inlet to outlet gas pressure) were measured by a system of pressure sensors described in paragraph 3.6.1. The following error analysis of these measurements is based on data from the manufacturer of the sensors.

The suit helmet pressure and the suit inlet pressure accuracies are the same since the sensors and method of readout are identical. A root-mean-square sum of the performance characteristics of the sensors is given as an example. The manufacturer specified the following:

Maximum combined non-linearity and hysteresis	.75% FS (Full Scale)
Repeatability	0.10% FS
Temperature Drift	2% FS/100°F
Temperature effect on sensitivity	1% FS/100°F

When the temperature is within 10°F of the calibration temperature, a value for the errors is 0.79% of full scale or .079 psi for the 10 psi full scale gauge.

The resolution of the recording oscilloscope (Figure 20) is approximately 0.235 MV (.05 in) with a non-linearity of 1%. The oscilloscope gives an error of .235 MV (resolution) and .24 MV (non-linearity). In this case, the .235 MV is equal to .09 psi and the RMS sum of the three figures is:

$$\sqrt{[(7.9)^2 + 9^2 + 9^2]} \times 10^{-2} \text{ PSI}^2 = 0.15 \text{ PSI}$$

The probable accuracy is then ± 0.15 PSI (1.5% of full scale).

A similar method was used on the suit pressure drop sensor and the resultant probable accuracy is $\pm .01$ psi (2% of full scale).

III. Suit Gas Flow Accuracy.

The flowmeter used to measure suit gas flow rate was calibrated against a Brooks flowmeter which was accurate to 1% of indicated flow. The flowmeter used during the test was mounted in the flow system where the inlet pressure was ambient pressure. Thus, no pressure corrections were required.

The accuracy of the flowmeter measurements is $\pm 3\%$ for the conditions of use.

IV. Suit Leakage Accuracy.

Suit leakage rate measurements are described in paragraph 3.4.1. On the basis of data supplied by the flowmeter, the accuracy of the instrument as used is 2%. The readability of the instrument is approximately 0.5% resulting in an overall accuracy of $+0.1\%$ to -4.1% . When a standard flowmeter gas correction (for N₂) is applied, the accuracy is $\pm 2.1\%$.

The ionization gauges described in paragraph 3.6.1 were utilized during Experiment I-b to indicate the general area of the origin of suit leaks. The manufacturers calibrations were used for the gauges since a qualitative indication was sufficient to indicate the area of the leaks. The accuracy of the gauges is estimated to be on the order of $\pm 15\%$ of the indicated reading.

V. Relative Humidity and Visor Frosting.

The humidity measuring system (paragraph 3.6.1) was calibrated with a Blue M. Electric Co. Model VP100 relative humidity chamber whose accuracy is 2%. The probable accuracy of the measurements made in this test are $\pm 10\%$, based upon linearity, calibration accuracy, and the method of indication.

The lamp-photo-cell visor frosting indicating system served only to give a qualitative indication so it was not quantitatively calibrated against any standard.

VI. Energy Into Visor.

The thermopile utilized for this measurement (paragraph 3.6.1) was calibrated by the Eppley Laboratories against a U.S. Bureau of Standards Class A standard. The Eppley Laboratory calibration for this instrument was used for test I-b.

APPENDIX C

VIEW FACTOR CALCULATIONS

CALCULATION OF VIEW FACTOR BETWEEN TEST PLANE
AND EARTH SIMULATOR

Diagram of approximate geometric configurations existing within the SES:

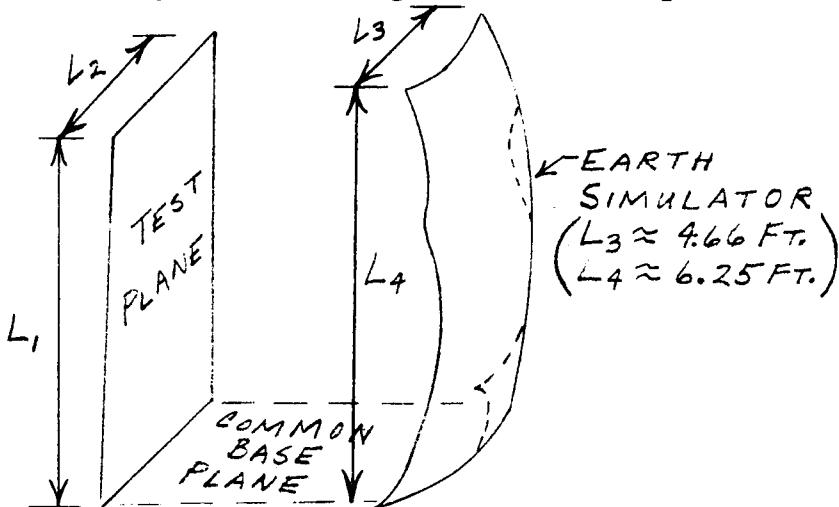


Figure C-1

Diagram of Geometric Configuration in SES

Assuming the simplest geometrical configuration available, that of an ellipse (See WADD TN 60-145), to represent the thermal dummy, the following relationships were utilized:

- (a) major diameter: 15.5 in. (1.29 Ft)
- (b) minor diameter: 8.9 in. (0.74 Ft)
- (c) height: 60.1 in. (5.75 Ft)
- (d) total surface area: 20.6 Ft^2
- (e) total projected area: 10.3 Ft^2
- (f) dimensions of test plane rectangle representing thermal dummy: height: 5.75 Ft (L_1); width: 1.79 Ft (L_2)

Assuming that the thermal dummy and the earth simulator can be replaced by their respective projected areas, it is now necessary to find the resulting view factor between them. The method used herein may be found in ASD Technical Report 60-119, Part I. For two parallel planes in the most general position, the following dimensions are defined with respect to Figure C-2:

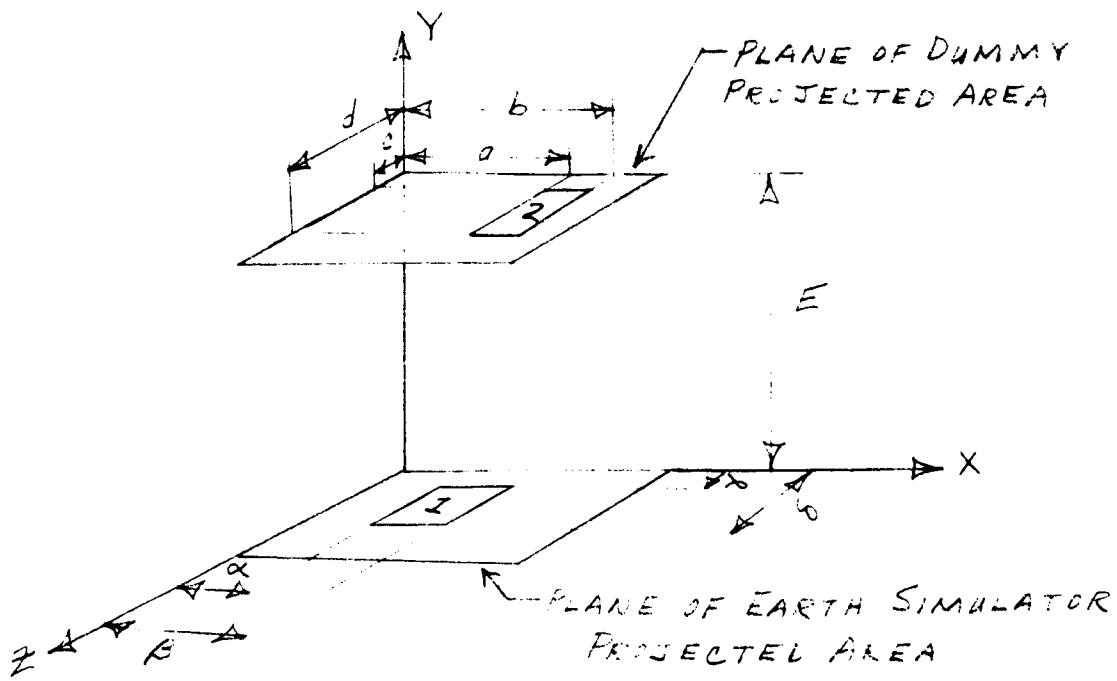


Figure 3-2

Definition of Dimensions for Two Parallel Planes

For the particular case in question, the following relationships exist:

$$(1) \quad \begin{cases} \alpha = 0 \\ y = 0 \\ c = 0 \end{cases}$$

$$(2) \quad \begin{cases} \beta = 4.66 \text{ Ft} \\ \delta = 6.25 \text{ Ft} \\ d = 5.75 \text{ Ft} \\ b = 3.73 \text{ Ft} \\ a = 1.94 \text{ Ft} \end{cases}$$

In general the following relationship exists (See Figure C-2):

$$(3) \quad F_{12} = \frac{1}{\pi A_1} f_1 (\beta-b, \delta-c) - f_1 (\beta-a, \delta-c) + f_1 (\alpha-a, \delta-c)$$

$$- f_1 (\alpha-b, \delta-c) + f_1 (\alpha-b, \gamma-c)$$

$$- f_1 (\alpha-a, \gamma-c) + f_1 (\beta-a, \gamma-c) - f_1 (\beta-b, \gamma-c)$$

$$+ f_1 (\beta-b, \gamma-d) - f_1 (\beta-a, \gamma-d) + f_1 (\alpha-a, \gamma-d)$$

$$- f_1 (\alpha-b, \gamma-d) + f_1 (\alpha-b, \delta-d) - f_1 (\alpha-a, \delta-d)$$

$$+ f_1 (\beta-a, \delta-d) - f_1 (\beta-b, \delta-d) ,$$

Where

$$(4) \quad f_1 (\nu, \xi) = \frac{1}{2} \left[E \nu \tan^{-1} \left(\frac{\nu}{E} \right) - \xi \sqrt{E^2 + \nu^2} \tan^{-1} \left(\frac{\xi}{\sqrt{E^2 + \nu^2}} \right) \right.$$

$$\left. - \nu \sqrt{E^2 + \xi^2} \tan^{-1} \left(\frac{\nu}{\sqrt{E^2 + \xi^2}} \right) + \frac{E^2}{2} \ln \left(\frac{E^2 + \nu^2 + \xi^2}{E^2 + \xi^2} \right) \right]$$

The following definitions are now in order:

$$(5) \quad \begin{cases} f_1 (\beta-b, \delta-c) = f (\nu_1, \xi_1) \\ f_1 (\beta-a, \delta-c) = f (\nu_2, \xi_2) \\ f_1 (\alpha-a, \delta-c) = f (\nu_3, \xi_3) \\ f_1 (\alpha-b, \delta-c) = f (\nu_4, \xi_4) \\ f_1 (\alpha-b, \gamma-c) = f (\nu_5, \xi_5) \\ f_1 (\alpha-a, \gamma-c) = f (\nu_6, \xi_6) \\ f_1 (\beta-a, \gamma-c) = f (\nu_7, \xi_7) \\ f_1 (\beta-b, \gamma-c) = f (\nu_8, \xi_8) \end{cases}$$

$$\begin{cases} f_1(\beta-b, \gamma-d) = f(v_9, \xi_9) \\ f_1(\beta-a, \gamma-d) = f(v_{10}, \xi_{10}) \\ f_1(\alpha-a, \gamma-d) = f(v_{11}, \xi_{11}) \\ f_1(\alpha-b, \gamma-d) = f(v_{12}, \xi_{12}) \\ f_1(\alpha-b, \delta-d) = f(v_{13}, \xi_{13}) \\ f_1(\alpha-a, \delta-d) = f(v_{14}, \xi_{14}) \\ f_1(\beta-a, \delta-d) = f(v_{15}, \xi_{15}) \\ f_1(\beta-b, \delta-d) = f(v_{16}, \xi_{16}) \end{cases}$$

$$(6) \begin{cases} f(v_1, \xi_1) = f[(4.66 - 3.73), (6.25 - 0)] = f(0.93, 6.25) \\ f(v_2, \xi_2) = f[(4.66 - 1.94), (6.25 - 0)] = f(2.72, 6.25) \\ f(v_3, \xi_3) = f[(0 - 1.94), (6.25 - 0)] = f(-1.94, 6.25) \\ f(v_4, \xi_4) = f[(0 - 3.73), (6.25 - 0)] = f(-3.73, 6.25) \\ f(v_5, \xi_5) = f[(0 - 3.73), (0 - 0)] = f(-3.73, 0) \\ f(v_6, \xi_6) = f[(0 - 1.94), (0 - 0)] = f(-1.94, 0) \\ f(v_7, \xi_7) = f[(4.66 - 1.94), (0 - 0)] = f(2.72, 0) \\ f(v_8, \xi_8) = f[(4.66 - 3.73), (0 - 0)] = f(0.83, 0) \\ f(v_9, \xi_9) = f[(4.66 - 3.73), (0 - 5.75)] = f(0.93, -5.75) \\ f(v_{10}, \xi_{10}) = f[(4.66 - 1.94), (0 - 5.75)] = f(2.72, -5.75) \\ f(v_{11}, \xi_{11}) = f[(0 - 1.94), (0 - 5.75)] = f(-1.94, -5.75) \\ f(v_{12}, \xi_{12}) = f[(0 - 3.73), (0 - 5.75)] = f(-3.73, -5.75) \\ f(v_{13}, \xi_{13}) = f[(0 - 3.73), (6.25 - 5.75)] = f(-3.73, 0.50) \\ f(v_{14}, \xi_{14}) = f[(0 - 1.94), (6.24 - 5.75)] = f(-1.94, 0.50) \\ f(v_{15}, \xi_{15}) = f[(4.66 - 1.94), (6.25 - 5.75)] = f(2.72, 0.50) \\ f(v_{16}, \xi_{16}) = f[(4.66 - 3.73), (6.25 - 5.75)] = f(0.93, 0.50) \end{cases}$$

Each of the terms given in equation (6) is evaluated by substituting the respective numbers into equation (3). Due to the fact that all the calculations are not only similar in nature, but also very tedious, only the first will be spelled out in detail. The others are omitted, with only the results called out. Thus,

$$(7) \quad f(\nu_1, \xi_1) = f(0.93, 6.25)$$

$$\begin{aligned} &= \frac{1}{2} \left[(3)(0.93) \tan^{-1} \left(\frac{0.93}{3} \right) - (6.25) \sqrt{(3)^2 + (0.93)^2} \tan^{-1} \left(\frac{6.25}{\sqrt{(3)^2 + (0.93)^2}} \right) \right. \\ &\quad \left. - (0.93) \sqrt{(3)^2 + (6.25)^2} \tan^{-1} \left(\frac{0.93}{\sqrt{(3)^2 + (6.25)^2}} \right) + \frac{(3)^2}{2 \ln} \left(\frac{(3)^2 + (0.93)^2 + (6.25)^2}{(3)^2 + (6.25)^2} \right) \right] \\ &= \frac{1}{2} \left[(2.79) \tan^{-1} (0.31) - (6.25) \sqrt{9.865} \tan^{-1} \left(\frac{6.25}{\sqrt{9.865}} \right) \right. \\ &\quad \left. - (0.93) \sqrt{48.0} \tan^{-1} \left(\frac{0.93}{\sqrt{48.0}} \right) + (4.5) \ln \left(\frac{48.865}{48.0} \right) \right] \\ &= \frac{1}{2} \left[(2.79)(0.292) - (19.6)(1.09) - 6.45(0.0194) + (4.5)(0.0188) \right] \\ &= \frac{1}{2} [0.815 - 21.7 - 0.125 + 0.0845] \\ &= \frac{1}{2} (-20.9) \end{aligned}$$

$$(8) \quad f_1(\nu_1, \xi_1) = -10.45$$

Similarly,

$$f_1(\nu_2, \xi_2) = -12.88$$

$$f_1(\nu_3, \xi_3) = -11.69$$

$$f_1(\nu_4, \xi_4) = -28.96$$

$$f_1(\nu_5, \xi_5) = +2.10$$

$$f_1(\nu_6, \xi_6) = +0.86$$

$$f_1(\nu_7, \xi_7) = +1.46$$

$$(9) \quad f_1(\nu_8, \xi_8) = +0.1347$$

$$f_1(\nu_9, \xi_9) = -0.988$$

$$f_1(\nu_{10}, \xi_{10}) = -10.98$$

$$f_1(\nu_{11}, \xi_{11}) = -10.12$$

$$f_1(\nu_{12}, \xi_{12}) = -12.84$$

$$f_1(\nu_{13}, \xi_{13}) = +1.94$$

$$f_1(\nu_{14}, \xi_{14}) = +0.643$$

$$f_1(\nu_{15}, \xi_{15}) = +0.055$$

$$f_1(\nu_{16}, \xi_{16}) = +0.065$$

To arrive at the form factor between the earth simulator and the thermal dummy, it is necessary to substitute the values of $f_1(\nu_n, \xi_n)$ obtained in equations (8) and (9) into equation (4).

Thus:

$$(10) \quad F_{12} = \frac{1}{\pi A_1} \left[(-10.45) - (-12.78) + (-11.74) - (-28.96) + (2.10) \right. \\ \left. - (0.86) + (1.46) - (0.1347) + -9.88) - (-10.98) \right. \\ \left. + (-10.12) - (-12.84) + (1.94) - (0.643) + (0.055) \right. \\ \left. - (0.065) \right] \\ = \frac{1}{\pi A_1} (71.215 - 44.4277) \\ = \frac{(26.79)}{\pi (6.25) (4.66)}$$

$$(11) \quad F_{12} = 0.286,$$

Where F_{12} is the view factor from the earth simulator to the thermal dummy. By the reciprocity theorem ($A_1 F_{12} = A_2 F_{21}$) the reciprocal view factor can be obtained; that is, the view factor from the thermal dummy to the earth simulator. Hence,

$$(12) \quad F_{21} = \frac{(6.25) (4.66) (0.286)}{(10.3)} = 0.809$$

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